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LONGITUDINAL AERODYNAMIC CHARACTERISTICS
OF A WING-WINGLET MODEL DESIGNED AT $M = 0.8$,
 $C_L = 0.4$ USING LINEAR AERODYNAMIC THEORY

FOR REFERENCE

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ABSTRACT

Wind tunnel test results have been presented herein for a subsonic transport type wing fitted with winglets. Wing planform was chosen to be representative of wings used on current jet transport aircraft, while wing and winglet camber surfaces were designed using two different linear aerodynamic design methods. The purpose of the wind tunnel investigation was to determine the effectiveness of these linear aerodynamic design computer codes in designing a non-planar transport configuration which would cruise efficiently. The design lift coefficient was chosen to be 0.4, at a design Mach number of 0.8. Force and limited pressure data were obtained for the basic wing, and for the wing fitted with the two different winglet designs, at Mach numbers of 0.60, 0.70, 0.75 and 0.80 over an angle of attack range of -2 to +6 degrees, at zero sideslip. The data have been presented without analysis to expedite publication.

INTRODUCTION

Recently, two different subcritical aerodynamic design computer programs have been developed which determine camber surfaces for one-or two-planform configurations for minimum induced drag at a chosen design lift coefficient and Mach number (refs. 1-3). Both of these computer programs used a vortex lattice model in the near field to obtain the minimum induced drag camber surfaces. The original program developed by Lamar (ref. 1) also used a discrete vortex far field wake model to determine the required optimum spanload, while the second program developed by Kuhlman (refs. 2,3) used a higher order panel wake model to determine the required spanload. For planar configurations the two programs have been found to yield identical camber surface results, but the camber surface results differ appreciably for non-planar configurations (refs. 2,3) such as a wing-winglet or wing-strut.

The present wind tunnel study of a transport wing fitted with winglets was undertaken to determine the effectiveness of these two subcritical aerodynamic design programs in determining efficient non-planar camber surfaces

with relatively little computer cost, due to the simplicity of the methods. Design results obtained from the two programs for the chosen wing-winglet planform yielded essentially identical wing camber surfaces, but widely differing winglet camber surfaces. As a result, a single wing model was built, along with winglet pairs which matched the camber surface results from the two design programs. Details of the design methodology used, and the camber surfaces which resulted from each program, have been documented by Kuhlman (ref. 4). The concept of use of a winglet surface to reduce the induced drag component for a transport-type wing, thereby reducing fuel consumption, was developed by Whitcomb (ref. 5).

The wing-winglet configuration was chosen for the present study to determine the accuracy of the theoretical design methods used (refs. 1-3) for a non-planar configuration. The design lift coefficient of 0.4 was chosen as being representative of a cruise condition. The design Mach number of 0.8 was chosen to provide a stringent test of both subcritical theoretical methods. It was hoped that subcritical flow might be maintained on the configuration at the design point (ref. 4). The model described in ref. 4 was tested in the NASA/Langley Research Center 7-by 10-foot high speed wind tunnel at Mach numbers of 0.60, 0.70, 0.75 and 0.80 over an angle of attack range of -2 to +6 degrees at zero sideslip. Both force and some limited wing pressure distribution data, as well as wing surface oil flow visualization results, have been obtained. The data have been presented without analysis to expedite publication.

SYMBOLS

The International System of Units has been used for displaying dimensional quantities in this report (see ref. 6). United States Customary units have been presented in parenthesis. All measurements and calculations have been made using the U.S. Customary Unit System. Data presented in this report have been referred to the stability axis system. The reference center for moments has been defined in figure 1. Symbols shown in parenthesis are used in tables II and III.

A	wing aspect ratio, b^2/S
b(B)	wing reference span, 1.387 m (54.60 in.)

(BETA)	angle of sideslip of the model, degrees
\bar{c}	wing reference chord, 0.2304 m (9.071 in.)
c_t	wing tip chord, m (in.)
(C)	local wing chord, m (in.)
(CA)	axial force coefficient, $\frac{\text{Axial Force}}{q S}$
$C_D, (CD)$	drag coefficient, $\frac{\text{Drag}}{q S}$
$C_L, (CL)$	lift coefficient, $\frac{\text{Lift}}{q S}$
$C_m, (CMS)$	stability axis pitching moment coefficient, $\frac{\text{Pitching Moment}}{q S \bar{c}}$
(CN)	normal force coefficient, $\frac{\text{Normal Force}}{q S}$
$C_p (CP)$	pressure coefficient
(CRMS)	stability axis rolling moment coefficient, $\frac{\text{Rolling Moment}}{q S b}$
(CYMS)	stability axis yawing moment coefficient, $\frac{\text{Yawing Moment}}{q S b}$
(CYS)	stability axis side force coefficient, $\frac{\text{Side Force}}{q S}$
$M, (MACH)$	free stream Mach number
(P1)	free stream static pressure, Pa (lb/ft ²)

(PT1)	stagnation pressure, Pa (lb/ft ²)
q,(Q)	free stream dynamic pressure, Pa (lb/ft ²)
S	wing reference area, 0.2848 m ² (3.066 ft ²)
X	streamwise body axis coordinate, m (in.)
Y	spanwise coordinate, m (in.)
Z	vertical coordinate, m (in.)
α , (ALPHA,ALPW)	angle of attack of the model, degrees
η	nondimensional spanwise coordinate, Y/B/2
Λ	leading edge sweep angle of the wing, degrees
ϕ	dihedral angle, degrees

DESCRIPTION OF MODEL

The geometry of the model tested has been presented in figure 1, while photographs of the model as installed in the NASA/Langley Research Center 7-by 10-foot high speed tunnel have been presented in figure 2. The baseline configuration tested consisted of the cambered, twisted wing shown in plan-view in figure 1a, mounted to an existing generalized transport-type aircraft fuselage which was used previously by Jacobs (ref. 7). The fuselage was mounted with a positive incidence with respect to the wing of 1.5 degrees. Also tested were two winglet designs, each having the planform shown in figure 1b. Design of the wing and winglet planforms was performed as described in reference 4 using two different subcritical aerodynamic design programs (refs. 1-3).

The baseline wing had a leading edge sweep angle of 38.2° , 6 degrees of dihedral, and an aspect ratio of 6.75. Trapezoidal wing reference area was 0.2848 m^2 , and wing reference span was 1.387 m. The wing had a break in trailing edge sweep at the 40 percent span station (fig. 1a). The winglet planform was based on criteria developed by Whitcomb (ref. 5), with a winglet root chord equal to 0.65 times the wing tip chord, 77.5° of dihedral, a leading edge sweep of 35.3° , and a height equal to 14 percent of the projected wing semispan. Winglet tip chord was 33 percent of the winglet reference root chord. A highly swept ($\Lambda = 61.6^\circ$) leading edge extension was added to the lower 25 percent of the winglet (see fig. 1b.). As described in detail in ref. 4, the wing and winglet camber surfaces were obtained using linearized aerodynamic theory (refs. 1-3) to obtain a rectangular chord loading at all span stations and minimum induced drag. An NACA 64A008 thickness distribution was used on both the wing and winglets.

The model was sting mounted on a six-component strain gage balance, which was used to measure the total forces and moments on the configuration. The wing was fitted with chordwise rows of surface static pressure taps at the 31.4 and 74.3 percent span stations. The winglets were fitted with chordwise rows of pressure taps at the 12.5 and 42.5 percent winglet span stations, corresponding to $\eta = 1.003$ and 1.011 , respectively. Pressure taps were connected via tubing to four mechanically-scanned electronic pressure transducers mounted to the fuselage strongback in the nose of the model. Also mounted to the fuselage strongback was an electrical accelerometer transducer which was used to determine model angle of attack.

APPARATUS, TESTS, AND CORRECTIONS

The investigation was conducted in the NASA/Langley 7- by 10-foot high speed wind tunnel. The capabilities of this tunnel and calibration results have been documented by Fox and Huffman in reference 8. Tests were conducted at Mach numbers ranging between 0.60 and 0.80, corresponding to Reynolds numbers of 2.2×10^6 to 2.6×10^6 , respectively, based on wing reference chord (ref. 8). The baseline wing, and the wing fitted with the two winglet models, were tested over an angle of attack range of -2 to $+6$ degrees, at zero sideslip.

Data acquisition and data reduction capabilities for the Langley 7-by 10-foot high speed tunnel have been described by Fox (ref. 9).

The balance chamber pressure and fuselage base pressure were measured, and total drag measurements were adjusted to a condition of freestream static pressure acting over the base of the model. Jet boundary corrections (ref. 10) and blockage corrections (ref. 11) have been applied to all force and moment data. Boundary transition strips 0.0016 m (.0625 in.) wide were placed on the model as shown in figure 3, where the sizing of the carborundum grit particles was determined using the method of Braslow and Knox (ref. 12), and the chordwise locations of the transition strips were determined as described by Blackwell (ref. 13). The fluorescent-oil film flow visualization technique described in reference 14 was used, both to verify that flow ahead of the transition strips was laminar, and to investigate surface shear patterns on the wing and winglet upper surfaces near the design point.

PRESENTATION OF RESULTS

The results have been presented herein without analysis, in order to expedite publication. The data have been presented in the following figures:

	<u>Figure</u>
Performance data at $M = 0.60$	4
Performance data at $M = 0.70$	5
Performance data at $M = 0.75$	6
Performance data at $M = 0.80$	7
Oil flow photographs of wing-winglet model	8

The run schedule has been presented in table I. Tabulated force and pressure data has been presented in coefficient form in tables II and III. Upper surface pressure coefficients have been presented first, followed by lower surface pressure coefficients.

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Table I Run schedule.

Run	M	α Range	Transition	Winglet	Data Type	Comments			
1	0.80	-4° to +4°	Free	None	Force	To determine α for oil flow photos			
2	0.80	-4° to +4°	Free	None	Force				
3	0.75	-4° to +4°	Free	None	Force				
4	0.80	-4° to +4°	Free	None	Force				
5	0.80	-2° to +3°	Free	None	Force	Force data for baseline wing, free transition			
6	0.75	-2° to +3°	Free	None	Force				
7	0.70	-2° to +3°	Free	None	Force				
8	0.60	-2° to +3°	Free	None	Force				
9	0.80	0.5°, 1.5°, 2.5°, 3.5°	Free	None	Oil flow	Oil flow to locate transitions trips			
9	0.60	3.5°	Free	None	Oil flow				
10	0.80	-2° to +6°	Fixed	None	Force and Pressure	Baseline wing performance data			
11	0.75	-2° to +6°	Fixed	None	Force and Pressure				
12	0.70	-2° to +6°	Fixed	None	Force and Pressure				
13	0.60	-2° to +6°	Fixed	None	Force and Pressure				
14	0.82	0° to +2.5°	Fixed	None	Force and Pressure				
15	0.80	-2° to +6°	Fixed	High-order Panel-wake	Force and Pressure	Performance data for wing with high-order-panel-wake winglet			
16	0.75	-2° to +6°	Fixed	High-order Panel-wake	Force and Pressure				
17	0.70	-2° to +6°	Fixed	High-order Panel-wake	Force and Pressure				
18	0.60	-2° to +6°	Fixed	High-order Panel-wake	Force and Pressure				
19	0.80	-2° to +6°	Fixed	Discrete-vortex-wake	Force and Pressure	Performance data for wing with discrete-vortex-wake winglet			
20	0.75	-2° to +6°	Fixed	Discrete-vortex-wake	Force and Pressure				
21	0.70	-2° to +6°	Fixed	Discrete-vortex-wake	Force and Pressure				
22	0.60	-2° to +6°	Fixed	Discrete-vortex-wake	Force and Pressure				
23	0.70	+2°, 3°	Fixed	Discrete-vortex-wake	Force and Pressure				
24	0.80	1.5°, 2°, 2.5°	Fixed	Discrete-vortex-wake	Oil Flow	Oil flow photos for wing with discrete-vortex-wake winglet			

1

1

Table II. Force data.

NASA LANGLEY						7 X 10 HIGH SPEED TUNNEL					
TEST 107						RUN 1					
POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16720	.804	30033.7	1.23	.3540	.0181	-.1370	-.0007	.0000	-.0004	.3543	.0105
16722	.807	30193.3	-5.91	-.3997	.0617	-.0734	-.0030	.0008	-.0029	-.4040	.0202
16723	.807	30183.6	-2.81	-.1037	.0218	-.0792	.0012	.0005	-.0006	-.1046	.0167
16724	.806	30113.2	-.73	.1303	.0145	-.1060	.0005	.0000	-.0002	.1301	.0162
16725	.806	30107.8	1.19	.3461	.0178	-.1342	-.0006	-.0000	-.0006	.3464	.0106
16726	.804	30045.2	2.97	.5418	.0290	-.1558	-.0026	.0000	-.0007	.5426	.0009
16727	.805	30076.9	4.55	.6988	.0463	-.1653	-.0026	.0001	-.0006	.7003	-.0093
16728	.805	30081.5	6.05	.8139	.0674	-.1594	-.0044	.0002	-.0008	.8165	-.0187
16729	.807	30175.5	7.45	.9039	.0947	-.1442	-.0040	.0003	-.0005	.9086	-.0233
16730	.805	30102.7	.33	.2496	.0154	-.1211	-.0002	-.0000	-.0001	.2496	.0140
16731	.804	30029.6	2.20	.4592	.0231	-.1469	-.0013	.0000	-.0005	.4598	.0055
16732	.807	30161.1	3.95	.6473	.0399	-.1631	-.0031	.0001	-.0006	.6485	-.0048
16733	.806	30121.2	1.29	.3615	.0184	-.1372	-.0011	-.0000	-.0003	.3618	.0103

NASA LANGLEY						7 X 10 HIGH SPEED TUNNEL					
TEST 107						RUN 2					
POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16747	.807	30170.2	1.36	.3671	.0182	-.1386	-.0012	-.0001	-.0005	.3675	.0095
16748	.806	30129.2	-2.70	-.0909	.0212	-.0796	.0011	.0005	-.0006	-.0918	.0169
16749	.805	30108.3	-.67	.1364	.0140	-.1075	-.0003	-.0000	-.0002	.1362	.0156
16750	.805	30106.9	.37	.2575	.0151	-.1226	-.0008	-.0001	-.0004	.2575	.0134
16751	.805	30113.7	1.36	.3693	.0183	-.1384	-.0010	-.0001	-.0005	.3696	.0095
16752	.805	30094.1	2.24	.4684	.0230	-.1494	-.0017	-.0000	-.0005	.4689	.0047
16753	.805	30090.3	3.11	.5650	.0302	-.1591	-.0025	.0000	-.0006	.5658	-.0005
16754	.807	30177.2	3.97	.6468	.0398	-.1635	-.0028	.0001	-.0008	.6480	-.0051
16755	.806	30167.1	4.68	.7147	.0485	-.1663	-.0037	.0002	-.0008	.7162	-.0100
16756	.809	30288.1	6.11	.8176	.0693	-.1581	-.0022	.0000	.0001	.8203	-.0181
16757	.807	30199.4	7.54	.9086	.0953	-.1393	-.0020	.0000	.0005	.9133	-.0247
16758	.807	30208.5	1.37	.3765	.0186	-.1401	-.0013	-.0001	-.0003	.3768	.0096

NASA LANGLEY						7 X 10 HIGH SPEED TUNNEL					
TEST 107						RUN 3					
POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16759	.755	27782.6	1.16	.3287	.0164	-.1221	-.0007	-.0000	-.0003	.3290	.0097
16760	.755	27790.8	-2.54	-.0609	.0184	-.0797	.0014	.0004	-.0001	-.0617	.0157
16761	.755	27790.0	-.70	.1316	.0135	-.1011	.0008	.0000	.0002	.1314	.0151
16762	.753	27699.1	.18	.2261	.0141	-.1111	-.0004	-.0000	-.0001	.2261	.0134

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7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 4

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16838	.805	30016.8	1.40	.3919	.0185	-.1431	-.0009	-.0000	-.0005	.3922	.0089
16839	.806	30077.9	-2.70	-.0770	.0209	-.0813	.0012	.0004	-.0011	-.0779	.0172
16840	.808	30160.7	-.55	.1669	.0142	-.1141	.0002	.0000	-.0004	.1668	.0158
16841	.804	30006.2	.42	.2781	.0151	-.1278	-.0006	.0000	-.0006	.2782	.0130
16842	.806	30066.5	1.39	.3891	.0186	-.1438	-.0011	.0000	-.0006	.3894	.0092
16843	.806	30057.0	2.32	.4977	.0243	-.1562	-.0020	.0000	-.0008	.4983	.0042
16844	.807	30127.8	3.18	.5892	.0319	-.1625	-.0033	.0001	-.0010	.5901	-.0009
16845	.804	29982.4	3.96	.6655	.0398	-.1665	-.0045	.0003	-.0012	.6666	-.0062
16846	.805	30043.9	4.71	.7345	.0495	-.1688	-.0045	.0004	-.0014	.7361	-.0110
16847	.807	30124.1	6.12	.8300	.0701	-.1555	-.0039	.0002	-.0007	.8327	-.0188
16848	.807	30127.4	6.12	.8276	.0696	-.1556	-.0036	.0002	-.0007	.8303	-.0190
16849	.807	30092.0	1.44	.3980	.0189	-.1439	-.0016	.0000	-.0006	.3984	.0089
16850	.808	30160.7	-5.71	-.3630	.0564	-.0772	-.0034	.0008	-.0036	-.3668	.0201
16851	.807	30126.5	-4.36	-.2437	.0364	-.0745	-.0004	.0007	-.0023	-.2458	.0177
16852	.806	30069.7	-2.66	-.0702	.0210	-.0817	.0014	.0005	-.0009	-.0711	.0177
16853	.806	30058.0	-1.69	.0385	.0159	-.0959	.0007	.0003	-.0006	.0380	.0170
16854	.806	30067.6	-.96	.1205	.0146	-.1058	.0005	.0001	-.0005	.1202	.0166
16855	.806	30049.0	-.43	.1847	.0144	-.1141	-.0003	.0000	-.0007	.1845	.0158
16856	.806	30047.5	-.08	.2218	.0147	-.1199	-.0001	.0001	-.0006	.2218	.0150
16857	.806	30051.4	.59	.3022	.0161	-.1317	-.0006	.0001	-.0006	.3024	.0129
16858	.805	30013.4	1.09	.3575	.0177	-.1386	-.0008	.0001	-.0006	.3577	.0108
16859	.807	30093.9	4.72	.7386	.0530	-.1693	-.0036	.0004	-.0011	.7405	-.0079
16860	.806	30045.7	1.61	.4166	.0201	-.1460	-.0017	.0001	-.0007	.4170	.0084

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7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 5

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16881	.809	30448.5	-.03	.2274	.0138	-.1219	-.0002	-.0001	-.0001	.2274	.0139
16882	.806	30317.8	-2.02	-.0019	.0163	-.0909	.0011	.0002	-.0000	-.0025	.0162
16883	.806	30318.1	-1.58	.0500	.0147	-.0978	.0010	.0001	.0001	.0495	.0160
16884	.804	30214.7	-1.03	.1132	.0137	-.1048	.0003	-.0000	-.0000	.1129	.0157
16885	.805	30294.9	-.57	.1670	.0135	-.1128	.0002	-.0001	.0001	.1669	.0151
16886	.806	30323.0	-.04	.2285	.0141	-.1219	-.0006	-.0001	-.0000	.2285	.0143
16887	.808	30395.2	.49	.2903	.0150	-.1290	-.0004	-.0001	.0000	.2904	.0125
16888	.807	30348.6	1.02	.3506	.0166	-.1363	-.0013	-.0001	-.0000	.3508	.0104
16889	.805	30275.9	1.51	.4066	.0190	-.1442	-.0014	-.0001	-.0000	.4070	.0083
16890	.806	30302.7	2.00	.4562	.0217	-.1503	-.0017	.0000	.0001	.4566	.0058
16891	.805	30276.4	2.47	.5164	.0254	-.1560	-.0025	-.0000	-.0002	.5170	.0032
16892	.806	30327.7	2.97	.5630	.0291	-.1584	-.0028	.0001	-.0003	.5637	-.0002
16893	.806	30329.0	4.04	.6670	.0410	-.1642	-.0035	.0002	-.0004	.6682	-.0061
16894	.805	30271.1	6.08	.8293	.0682	-.1579	-.0026	.0001	.0005	.8318	-.0200
16895	.807	30372.3	.03	.2394	.0144	-.1225	-.0006	-.0001	.0000	.2394	.0143

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 6

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16896	.755	27952.8	-.12	.2112	.0135	-.1102	-.0006	-.0001	-.0001	.2112	.0140
16897	.754	27901.3	-1.87	.0222	.0150	-.0891	.0010	.0002	.0002	.0217	.0157
16898	.755	27973.6	-1.56	.0569	.0140	-.0922	.0008	.0001	.0003	.0565	.0156
16899	.754	27906.3	-1.08	.1066	.0133	-.0986	.0003	-.0000	.0001	.1063	.0153
16900	.754	27904.2	-.67	.1501	.0133	-.1039	.0001	-.0000	.0002	.1500	.0151
16901	.753	27865.6	-.13	.2100	.0136	-.1096	-.0004	-.0001	-.0000	.2100	.0140
16902	.754	27908.7	.24	.2452	.0140	-.1142	-.0004	-.0000	.0001	.2452	.0129
16903	.755	27938.5	.73	.2972	.0150	-.1190	-.0011	.0000	-.0001	.2973	.0112
16904	.754	27932.3	1.16	.3386	.0163	-.1241	-.0006	.0000	-.0002	.3389	.0095
16905	.753	27845.0	1.53	.3777	.0176	-.1278	-.0009	.0001	-.0002	.3780	.0075
16906	.752	27796.8	2.00	.4270	.0194	-.1304	-.0016	.0001	-.0004	.4274	.0045
16907	.753	27882.2	2.57	.4859	.0222	-.1367	-.0010	.0002	-.0005	.4864	.0004
16908	.754	27897.5	3.61	.5962	.0281	-.1458	-.0022	.0002	-.0005	.5968	-.0095
16909	.753	27860.6	5.67	.7795	.0452	-.1440	-.0030	.0003	-.0000	.7802	-.0321
16910	.754	27913.7	-.11	.2107	.0136	-.1100	-.0004	-.0001	-.0001	.2107	.0140

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 7

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16926	.702	25360.6	.90	.3079	.0141	-.1134	-.0005	-.0000	-.0003	.3081	.0092
16927	.704	25416.1	-1.95	.0218	.0137	-.0848	.0011	.0001	.0002	.0213	.0144
16928	.704	25414.0	-1.57	.0600	.0128	-.0903	.0005	.0000	.0002	.0596	.0144
16929	.705	25468.2	-1.06	.1108	.0123	-.0951	.0008	-.0000	.0003	.1106	.0143
16930	.703	25398.7	-.55	.1659	.0120	-.0998	.0005	-.0001	.0002	.1658	.0136
16931	.702	25342.9	-.03	.2195	.0123	-.1053	.0002	-.0000	.0001	.2195	.0124
16932	.704	25424.7	.52	.2718	.0132	-.1101	.0000	-.0000	.0001	.2719	.0107
16933	.703	25379.0	.97	.3161	.0142	-.1146	-.0005	-.0000	-.0001	.3163	.0088
16934	.702	25342.4	1.60	.3761	.0161	-.1189	-.0005	.0000	-.0001	.3764	.0056
16935	.703	25390.9	2.00	.4140	.0176	-.1216	-.0005	.0001	-.0001	.4144	.0031
16936	.703	25375.9	2.46	.4601	.0194	-.1252	-.0008	.0001	-.0003	.4605	-.0004
16937	.702	25338.4	3.05	.5159	.0223	-.1288	-.0008	.0002	-.0003	.5163	-.0052
16938	.702	25358.9	4.08	.6049	.0282	-.1289	-.0024	.0003	-.0006	.6054	-.0148
16939	.702	25322.6	5.94	.7509	.0420	-.1164	-.0011	.0004	-.0003	.7512	-.0360
16940	.704	25414.6	-.09	.2117	.0125	-.1048	.0000	-.0000	.0002	.2117	.0128

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 8

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16946	.603	20317.3	-.04	.1997	.0121	-.0946	.0003	.0000	-.0001	.1996	.0123
16947	.602	20281.2	-2.09	.0137	.0128	-.0790	.0013	.0001	.0000	.0132	.0133
16948	.603	20283.6	-1.56	.0632	.0120	-.0837	.0009	.0000	.0002	.0628	.0137
16949	.602	20259.8	-1.08	.1066	.0118	-.0878	.0007	.0000	.0000	.1063	.0138
16950	.603	20282.7	-.54	.1563	.0118	-.0904	.0003	-.0000	-.0003	.1562	.0133
16951	.602	20250.2	.05	.2095	.0122	-.0960	.0004	.0000	-.0003	.2096	.0120
16952	.602	20250.9	.47	.2477	.0127	-.0990	.0001	.0000	-.0003	.2478	.0107
16953	.602	20242.2	.92	.2876	.0135	-.1015	.0002	.0000	-.0005	.2878	.0089
16954	.603	20285.8	1.46	.3360	.0149	-.1042	.0002	.0000	-.0007	.3363	.0064
16955	.602	20239.2	1.95	.3801	.0164	-.1067	-.0004	.0001	-.0006	.3804	.0035
16956	.601	20221.7	2.55	.4341	.0185	-.1096	-.0001	.0002	-.0007	.4345	-.0008
16957	.603	20314.6	3.06	.4788	.0206	-.1132	-.0003	.0002	-.0008	.4792	-.0049
16958	.603	20307.9	4.00	.5524	.0257	-.1112	-.0013	.0002	-.0011	.5529	-.0129
16959	.605	20416.8	5.97	.6992	.0384	-.1025	-.0009	.0003	-.0010	.6995	-.0345
16960	.604	20333.2	.00	.2043	.0121	-.0954	.0002	.0000	-.0003	.2043	.0121

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16981	.807	30401.2	-2.07	-.0086	.0173	-.0875	.0011	.0002	-.0002	-.0092	.0170
16983	.806	30366.2	-1.54	.0497	.0155	-.0945	.0005	.0000	-.0002	.0493	.0168
16984	.806	30376.0	-.93	.1161	.0146	-.1013	.0002	-.0000	-.0000	.1158	.0165
16985	.805	30325.0	-.51	.1620	.0147	-.1059	.0000	-.0001	.0000	.1619	.0162
16986	.806	30374.0	.02	.2200	.0153	-.1132	-.0002	-.0001	.0001	.2200	.0153
16987	.808	30435.4	.49	.2720	.0162	-.1197	-.0003	-.0001	.0001	.2721	.0139
16988	.806	30349.3	1.05	.3344	.0179	-.1269	-.0007	-.0001	-.0000	.3347	.0117
16989	.806	30365.6	1.48	.3835	.0196	-.1328	-.0012	-.0001	-.0001	.3839	.0097
16990	.806	30362.9	1.47	.3827	.0197	-.1334	-.0013	-.0001	-.0001	.3831	.0098
16991	.806	30358.9	1.92	.4341	.0220	-.1399	-.0018	-.0001	-.0001	.4346	.0075
16992	.806	30355.2	2.50	.4995	.0259	-.1488	-.0025	-.0000	-.0002	.5002	.0041
16993	.807	30385.2	3.07	.5635	.0307	-.1581	-.0031	.0000	-.0005	.5644	.0005
16994	.807	30420.1	4.06	.6647	.0411	-.1657	-.0044	.0001	-.0008	.6659	-.0060
16995	.808	30434.3	5.88	.8081	.0657	-.1545	-.0041	.0002	-.0006	.8105	-.0174
16996	.807	30395.5	-.01	.2177	.0156	-.1139	-.0005	-.0001	.0000	.2177	.0156

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
16999	.754	27951.6	-.02	.2017	.0146	-.1026	-.0000	-.0001	-.0003	.2017	.0147
17000	.754	27980.0	-2.06	-.0044	.0163	-.0829	.0010	.0001	-.0003	-.0049	.0161
17001	.755	28009.5	-1.57	.0468	.0148	-.0877	.0005	.0000	-.0003	.0463	.0161
17002	.755	27988.8	-1.04	.1002	.0142	-.0926	.0003	-.0001	-.0002	.1000	.0160
17003	.754	27959.6	-.59	.1446	.0142	-.0973	.0001	-.0001	-.0002	.1445	.0157
17004	.755	27994.7	-.02	.2025	.0147	-.1034	-.0001	-.0001	-.0002	.2025	.0147
17005	.754	27984.4	.48	.2536	.0154	-.1086	-.0003	-.0001	-.0003	.2537	.0133
17006	.754	27975.7	.95	.3024	.0165	-.1130	-.0008	-.0001	-.0004	.3026	.0114
17007	.754	27957.6	1.46	.3537	.0181	-.1175	-.0009	-.0000	-.0005	.3540	.0091
17008	.755	27993.4	1.91	.4001	.0197	-.1217	-.0012	-.0000	-.0005	.4006	.0064
17009	.754	27974.9	2.48	.4583	.0222	-.1271	-.0015	.0001	-.0007	.4589	.0023
17010	.754	27967.1	2.95	.5058	.0245	-.1311	-.0018	.0001	-.0007	.5064	-.0016
17011	.755	28030.1	4.00	.6180	.0307	-.1411	-.0027	.0002	-.0009	.6186	-.0125
17012	.755	28018.1	6.02	.8099	.0498	-.1431	-.0035	.0001	-.0005	.8106	-.0355
17013	.755	28011.7	-.01	.2046	.0147	-.1032	-.0003	-.0001	-.0001	.2046	.0148

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17016	.703	25488.9	-2.04	.0013	.0155	-.0790	.0009	.0001	.0000	.0008	.0155
17017	.703	25513.7	-1.51	.0524	.0143	-.0837	.0006	.0000	-.0000	.0520	.0157
17018	.704	25532.9	-.94	.1078	.0139	-.0885	.0004	-.0001	-.0001	.1075	.0157
17019	.703	25515.8	-.56	.1432	.0140	-.0917	.0002	-.0001	-.0001	.1430	.0154
17020	.703	25506.3	-.02	.1952	.0144	-.0965	.0000	-.0001	-.0002	.1952	.0144
17021	.703	25512.8	.51	.2462	.0151	-.1013	-.0001	-.0001	-.0004	.2463	.0129
17022	.704	25557.9	1.02	.2955	.0162	-.1057	-.0004	-.0001	-.0006	.2958	.0110
17023	.703	25513.0	1.58	.3494	.0178	-.1099	-.0005	-.0000	-.0006	.3498	.0082
17024	.704	25528.0	1.94	.3842	.0191	-.1124	-.0008	.0000	-.0007	.3846	.0061
17025	.703	25511.8	2.48	.4368	.0211	-.1163	-.0011	.0001	-.0008	.4373	.0022
17026	.704	25542.4	3.01	.4885	.0234	-.1204	-.0013	.0001	-.0009	.4890	-.0022
17027	.704	25538.1	4.03	.5863	.0289	-.1259	-.0023	.0002	-.0010	.5869	-.0124
17028	.703	25520.9	6.05	.7522	.0434	-.1166	-.0021	.0003	-.0008	.7526	-.0360
17029	.703	25507.7	-.05	.1920	.0144	-.0964	.0001	-.0001	-.0001	.1919	.0146

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17030	.603	20387.5	-2.06	.0027	.0147	-.0734	.0011	.0001	.0001	.0022	.0148
17031	.604	20448.7	-1.60	.0444	.0140	-.0765	.0008	-.0000	.0001	.0440	.0152
17032	.603	20409.2	-.99	.0981	.0138	-.0803	.0008	-.0001	.0001	.0978	.0155
17033	.603	20408.7	-.55	.1380	.0139	-.0836	.0006	-.0001	-.0001	.1379	.0152
17034	.603	20400.9	.10	.1962	.0143	-.0882	.0004	-.0000	-.0002	.1963	.0139
17035	.603	20389.0	.49	.2311	.0148	-.0911	.0003	-.0000	-.0003	.2312	.0129
17036	.603	20400.6	1.00	.2769	.0158	-.0945	.0000	-.0000	-.0004	.2772	.0110
17037	.603	20393.3	1.47	.3193	.0170	-.0970	.0000	.0000	-.0006	.3197	.0088
17038	.602	20366.9	2.05	.3719	.0187	-.1005	-.0003	.0001	-.0007	.3724	.0054
17039	.602	20352.1	2.51	.4132	.0203	-.1029	-.0003	.0001	-.0008	.4137	.0021
17040	.602	20354.7	2.99	.4552	.0221	-.1058	-.0006	.0001	-.0008	.4557	-.0017
17041	.603	20417.9	4.04	.5440	.0271	-.1086	-.0014	.0002	-.0011	.5445	-.0113
17042	.603	20396.6	5.97	.6911	.0393	-.0999	-.0014	.0003	-.0010	.6914	-.0328
17043	.603	20407.3	-.03	.1846	.0141	-.0876	.0004	-.0000	-.0001	.1846	.0142

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 14

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17060	.827	31269.9	.01	.2269	.0156	-.1208	-.0004	-.0001	.0001	.2269	.0156
17061	.826	31250.1	1.05	.3484	.0191	-.1391	-.0011	-.0002	-.0000	.3487	.0127
17062	.827	31287.4	1.44	.3946	.0215	-.1467	-.0017	-.0002	-.0001	.3950	.0116
17063	.826	31259.1	2.04	.4620	.0258	-.1561	-.0024	-.0001	-.0002	.4626	.0094
17064	.827	31290.9	2.53	.5128	.0301	-.1615	-.0033	-.0001	-.0004	.5137	.0074
17065	.826	31259.7	-.05	.2221	.0157	-.1200	-.0004	-.0002	-.0001	.2221	.0159

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17082	.806	30261.8	-2.01	.0010	.0180	-.0905	.0013	.0001	.0005	.0004	.0180
17083	.805	30209.4	-1.53	.0551	.0163	-.0982	.0009	-.0001	.0008	.0547	.0178
17084	.806	30255.9	-1.05	.1084	.0154	-.1059	.0005	-.0002	.0007	.1081	.0174
17085	.806	30216.2	-.58	.1608	.0152	-.1127	.0002	-.0002	.0007	.1606	.0169
17086	.806	30247.8	.09	.2357	.0159	-.1237	-.0002	-.0002	.0006	.2357	.0155
17087	.806	30236.3	.52	.2845	.0166	-.1305	-.0004	-.0002	.0005	.2846	.0140
17088	.806	30220.8	.96	.3340	.0177	-.1382	-.0009	-.0002	.0003	.3343	.0121
17089	.807	30271.8	1.48	.3941	.0199	-.1471	-.0015	-.0001	.0001	.3945	.0097
17090	.806	30223.7	1.92	.4443	.0221	-.1541	-.0019	-.0001	.0000	.4448	.0072
17091	.805	30170.1	2.51	.5102	.0258	-.1637	-.0025	-.0000	-.0003	.5108	.0034
17092	.806	30252.6	2.96	.5617	.0297	-.1723	-.0031	-.0000	-.0003	.5625	.0007
17093	.805	30208.1	3.94	.6645	.0393	-.1816	-.0045	.0002	-.0012	.6657	-.0064
17094	.807	30257.8	5.88	.8145	.0647	-.1682	-.0045	.0003	-.0014	.8169	-.0190
17095	.806	30243.8	-.00	.2242	.0161	-.1226	-.0007	-.0002	.0002	.2242	.0161

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17112	.754	27775.0	-1.96	.0127	.0166	-.0864	.0014	.0000	.0009	.0122	.0170
17113	.753	27725.7	-1.45	.0660	.0152	-.0932	.0010	-.0001	.0011	.0656	.0169
17114	.753	27711.4	-.92	.1209	.0146	-.0999	.0007	-.0002	.0011	.1206	.0166
17115	.755	27778.9	-.52	.1630	.0146	-.1050	.0005	-.0002	.0011	.1628	.0161
17117	.754	27764.9	-.06	.2100	.0150	-.1106	.0002	-.0002	.0010	.2100	.0152
17118	.755	27805.0	.50	.2703	.0156	-.1191	.0000	-.0002	.0009	.2704	.0132
17119	.755	27802.5	1.11	.3328	.0169	-.1267	-.0004	-.0001	.0007	.3331	.0105
17120	.754	27765.3	1.53	.3756	.0182	-.1312	-.0006	-.0001	.0005	.3759	.0082
17121	.753	27723.1	2.02	.4263	.0199	-.1370	-.0010	.0000	.0003	.4268	.0048
17122	.755	27795.7	2.52	.4788	.0220	-.1431	-.0014	.0001	.0001	.4793	.0009
17123	.754	27751.5	2.98	.5268	.0242	-.1482	-.0018	.0002	-.0003	.5273	-.0032
17124	.754	27760.4	4.03	.6384	.0302	-.1585	-.0023	.0003	-.0003	.6389	-.0147
17125	.755	27775.2	6.02	.8232	.0492	-.1567	-.0029	.0003	.0000	.8238	-.0375
17126	.754	27734.4	.07	.2228	.0152	-.1126	.0001	-.0002	.0008	.2228	.0150

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17131	.703	25301.1	-2.00	.0091	.0161	-.0820	.0012	.0000	.0007	.0085	.0164
17132	.703	25286.9	-1.48	.0604	.0149	-.0878	.0009	-.0001	.0007	.0600	.0165
17133	.704	25322.4	-.83	.1236	.0144	-.0953	.0006	-.0002	.0005	.1234	.0162
17134	.703	25298.1	-.52	.1539	.0144	-.0988	.0003	-.0002	.0004	.1538	.0158
17135	.703	25279.9	.04	.2090	.0147	-.1051	.0001	-.0001	.0004	.2090	.0146
17136	.704	25305.7	.60	.2639	.0154	-.1117	-.0001	-.0001	.0002	.2641	.0126
17137	.703	25300.1	1.11	.3145	.0164	-.1172	-.0005	-.0001	.0000	.3147	.0103
17138	.704	25324.2	1.55	.3575	.0175	-.1217	-.0006	-.0000	-.0002	.3578	.0079
17139	.702	25231.7	2.06	.4088	.0190	-.1265	-.0010	.0000	-.0004	.4092	.0043
17140	.704	25308.0	2.55	.4576	.0208	-.1317	-.0012	.0001	-.0005	.4581	.0004
17141	.704	25326.0	3.06	.5069	.0228	-.1368	-.0014	.0002	-.0007	.5074	-.0042
17142	.704	25312.2	4.05	.6022	.0278	-.1430	-.0024	.0003	-.0012	.6027	-.0149
17143	.704	25307.2	6.07	.7690	.0422	-.1335	-.0020	.0004	-.0011	.7691	-.0394
17144	.704	25292.5	.05	.2100	.0148	-.1053	-.0000	-.0001	.0002	.2101	.0146

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17161	.602	20168.2	-1.88	.0216	.0150	-.0776	.0014	.0000	.0010	.0211	.0157
17162	.602	20165.6	-1.43	.0627	.0144	-.0815	.0013	-.0001	.0010	.0623	.0160
17163	.602	20152.0	-.93	.1078	.0142	-.0861	.0010	-.0001	.0008	.1075	.0160
17164	.603	20176.4	-.40	.1564	.0143	-.0914	.0009	-.0001	.0008	.1563	.0154
17165	.602	20163.7	.06	.1995	.0145	-.0955	.0006	-.0001	.0005	.1995	.0142
17166	.602	20151.4	.57	.2465	.0151	-.1002	.0005	-.0001	.0004	.2466	.0126
17167	.602	20158.9	1.11	.2953	.0160	-.1053	.0002	-.0000	.0002	.2956	.0103
17168	.602	20149.0	1.52	.3342	.0170	-.1082	-.0000	.0000	.0001	.3345	.0081
17169	.603	20167.9	2.03	.3812	.0183	-.1125	-.0002	.0001	-.0000	.3816	.0048
17170	.602	20157.5	2.55	.4291	.0199	-.1166	-.0004	.0001	-.0001	.4296	.0008
17171	.602	20131.0	3.03	.4733	.0216	-.1203	-.0006	.0002	-.0003	.4737	-.0035
17172	.603	20166.6	4.05	.5592	.0262	-.1233	-.0013	.0004	-.0008	.5597	-.0133
17173	.602	20142.7	6.03	.7116	.0384	-.1156	-.0010	.0005	-.0011	.7117	-.0366
17174	.603	20171.6	.03	.1971	.0145	-.0953	.0007	-.0001	.0006	.1971	.0144

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17191	.806	30200.0	-2.05	.0007	.0178	-.0878	.0013	.0001	.0008	.0001	.0178
17192	.805	30142.7	-1.47	.0650	.0158	-.0975	.0009	-.0000	.0009	.0645	.0175
17193	.806	30175.7	-.89	.1285	.0150	-.1063	.0005	-.0001	.0008	.1283	.0170
17194	.807	30220.8	-.50	.1731	.0150	-.1124	.0003	-.0002	.0008	.1730	.0165
17195	.806	30194.3	.06	.2361	.0154	-.1215	-.0001	-.0002	.0007	.2362	.0152
17196	.806	30184.3	.54	.2913	.0162	-.1300	-.0004	-.0002	.0007	.2915	.0134
17197	.806	30194.4	.99	.3411	.0174	-.1379	-.0007	-.0002	.0006	.3414	.0115
17198	.807	30231.6	1.46	.3962	.0193	-.1465	-.0010	-.0001	.0005	.3965	.0092
17199	.807	30242.1	2.03	.4630	.0224	-.1573	-.0019	-.0001	.0002	.4635	.0060
17200	.806	30199.5	2.56	.5243	.0259	-.1662	-.0024	.0000	-.0000	.5250	.0025
17201	.807	30211.3	3.06	.5801	.0301	-.1747	-.0034	.0002	-.0006	.5808	-.0009
17202	.805	30155.1	3.98	.6756	.0394	-.1826	-.0042	.0003	-.0010	.6767	-.0076
17203	.806	30181.8	6.00	.8303	.0664	-.1661	-.0040	.0003	-.0007	.8327	-.0208
17204	.806	30204.0	.04	.2337	.0157	-.1217	-.0004	-.0002	.0007	.2337	.0155

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17218	.754	27768.7	-2.00	.0075	.0166	-.0834	.0013	.0001	.0006	.0070	.0169
17219	.754	27732.7	-1.45	.0644	.0151	-.0907	.0009	-.0000	.0006	.0640	.0167
17220	.754	27756.7	-.91	.1198	.0145	-.0975	.0007	-.0001	.0007	.1196	.0164
17221	.754	27772.3	-.42	.1708	.0145	-.1042	.0003	-.0002	.0005	.1706	.0158
17222	.755	27773.3	.04	.2188	.0148	-.1102	.0001	-.0002	.0005	.2188	.0147
17223	.753	27717.3	.52	.2695	.0154	-.1166	-.0003	-.0001	.0003	.2697	.0129
17224	.755	27778.6	.99	.3182	.0164	-.1232	-.0005	-.0001	.0002	.3184	.0109
17225	.754	27737.1	1.55	.3764	.0179	-.1296	-.0010	-.0001	-.0001	.3768	.0078
17226	.754	27745.2	2.01	.4251	.0195	-.1353	-.0011	.0000	-.0001	.4255	.0046
17227	.753	27717.8	2.54	.4788	.0215	-.1412	-.0016	.0001	-.0002	.4793	.0003
17228	.755	27791.5	3.03	.5319	.0238	-.1480	-.0017	.0002	-.0003	.5324	-.0043
17229	.756	27814.1	4.16	.6538	.0305	-.1600	-.0029	.0004	-.0011	.6543	-.0170
17230	.755	27777.1	6.04	.8286	.0488	-.1580	-.0036	.0003	-.0008	.8292	-.0386
17231	.754	27752.1	.05	.2208	.0149	-.1103	-.0000	-.0002	.0005	.2208	.0147

Table II (concluded).

NASA LANGLEY						7 X 10 HIGH SPEED TUNNEL					
TEST 107						RUN 21					
POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17247	.704	25224.0	-2.02	.0056	.0161	-.0791	.0015	.0001	.0012	.0050	.0163
17248	.702	25139.5	-1.50	.0565	.0149	-.0852	.0013	.0000	.0012	.0561	.0163
17249	.703	25171.2	-.92	.1142	.0144	-.0919	.0012	-.0001	.0014	.1140	.0162
17250	.703	25189.2	-.52	.1535	.0144	-.0963	.0009	-.0001	.0013	.1533	.0158
17251	.704	25208.5	.01	.2063	.0147	-.1025	.0007	-.0001	.0011	.2063	.0146
17252	.704	25208.7	.55	.2609	.0154	-.1089	.0004	-.0001	.0009	.2610	.0128
17253	.703	25191.5	1.08	.3130	.0164	-.1148	.0001	-.0001	.0007	.3133	.0105
17254	.704	25209.2	1.50	.3551	.0175	-.1192	-.0002	-.0000	.0005	.3554	.0082
17255	.703	25153.7	1.95	.3992	.0189	-.1236	-.0003	.0000	.0004	.3996	.0053
17256	.704	25198.4	2.62	.4653	.0213	-.1305	-.0007	.0001	.0003	.4658	-.0000
17257	.703	25164.0	3.01	.5044	.0228	-.1340	-.0008	.0002	.0001	.5050	-.0036
17258	.704	25214.4	4.00	.6003	.0277	-.1417	-.0018	.0003	-.0005	.6008	-.0142
17259	.703	25174.2	5.96	.7562	.0413	-.1293	-.0013	.0005	-.0006	.7564	-.0374
17260	.704	25219.9	.07	.2116	.0149	-.1031	.0005	-.0001	.0010	.2116	.0147

NASA LANGLEY						7 X 10 HIGH SPEED TUNNEL					
TEST 107						RUN 22					
POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17263	.602	20116.0	-1.88	.0183	.0150	-.0752	.0013	.0000	.0007	.0178	.0156
17264	.603	20138.8	-1.44	.0589	.0145	-.0792	.0012	-.0001	.0008	.0585	.0159
17265	.603	20155.6	-.90	.1082	.0143	-.0843	.0011	-.0001	.0007	.1080	.0160
17266	.603	20154.6	-.48	.1462	.0143	-.0883	.0008	-.0001	.0006	.1461	.0155
17267	.603	20153.6	.10	.1996	.0145	-.0938	.0006	-.0001	.0004	.1996	.0142
17268	.603	20136.8	.57	.2433	.0151	-.0986	.0005	-.0000	.0003	.2434	.0127
17269	.602	20118.7	1.04	.2867	.0159	-.1027	.0003	-.0000	.0001	.2869	.0107
17270	.602	20096.2	1.50	.3292	.0169	-.1064	.0000	.0000	-.0001	.3295	.0083
17271	.603	20125.3	2.07	.3819	.0184	-.1109	-.0003	.0001	-.0002	.3823	.0046
17272	.603	20132.6	2.54	.4249	.0199	-.1147	-.0005	.0001	-.0004	.4253	.0011
17273	.602	20114.7	3.04	.4707	.0216	-.1191	-.0007	.0002	-.0005	.4712	-.0033
17274	.602	20107.0	4.04	.5551	.0261	-.1224	-.0014	.0003	-.0009	.5555	-.0130
17275	.602	20117.8	6.01	.7085	.0380	-.1155	-.0013	.0005	-.0015	.7086	-.0364
17276	.603	20134.3	.06	.1962	.0145	-.0935	.0006	-.0001	.0005	.1962	.0143

NASA LANGLEY						7 X 10 HIGH SPEED TUNNEL					
TEST 107						RUN 23					
POINT	MACH NUMB	Q PA	ALPHA DEG	CL	CD	CMS	CRMS	CYMS	CYS	CN	CA
17277	.704	25197.0	2.14	.4141	.0194	-.1257	-.0009	.0001	-.0003	.4145	.0039
17278	.704	25197.2	3.03	.5020	.0227	-.1343	-.0014	.0002	-.0006	.5025	-.0038
17279	.702	25123.2	.03	.2045	.0147	-.1026	.0002	-.0001	.0003	.2045	.0146

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16981

MACH .807

Q 30401.2

ALPW

-2.07

BETA

0.00

P1 66705.89

PT1 102381.52

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$
[illegible]

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16983

MACH .806

Q 30366.2

ALPW

-1.54

BETA

0.00

P1 66761.47

PT1 102384.92

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.3056	0.00	.01	.0192	0.00	-.01	.0906	.11	.01	.0177
.05	.05	.0571	.05	.03	.1133	.11	.03	.0183	.21	.00	.0186
.10	.06	-.1020	.10	.04	-.0810	.20	.05	.0104	.31	.00	.0158
.15	.06	-.1871	.15	.05	-.1861	.31	.06	.0089	.41	.01	.0143
.20	.07	-.2369	.20	.06	-.2711	.40	.07	.0137	.51	.01	.0136
.25	.07	-.2938	.25	.06	-.3332	.51	.06	.0122	.62	.01	.0160
.30	.07	-.3451	.30	.07	-.3948	.61	.06	.0140	.71	.00	.4380
.35	.07	-.3915	.35	.07	-.4348	.71	.05	.0119	.11	-.05	.0194
.40	.07	-.4342	.40	.07	-.4757	0.00	-.01	.0152	.22	-.04	.0189
.45	.07	-.4535	.45	.07	-.4935	.11	-.02	.0135	.32	-.03	.0160
.50	.07	-.4437	.50	.07	-.4792	.21	-.02	.0231	.42	-.03	.0145
.55	.06	-.4282	.55	.06	-.4472	.31	-.02	.0222	.51	-.02	.0138
.60	.06	-.3997	.60	.06	-.4173	.40	-.02	.0166	.62	-.01	.0162
.65	.05	-.3494	.65	.05	-.3613	.51	-.01	.0238	.72	-.00	.0134
.70	.05	-.3093	.70	.05	-.3270	.61	-.01	.0226			
.75	.04	-.2660	.75	.04	-.2739	.71	-.00	.0124			
.80	.03	-.2265	.80	.04	-.2228						
.85	.03	-.1594	.85	.03	-.1624						
.90	.02	-.1082	0.00	.01	.4697						
0.00	.03	.5188	.04	-.00	.0222						
.05	.01	-.4995	.09	-.01	-.5893						
.10	.01	-.3714	.14	-.01	-.4489						
.15	.00	-.3441	.19	-.01	-.3348						
.20	-.00	-.3265	.24	-.01	-.2947						
.25	-.00	-.3318	.29	-.01	-.2484						
.30	-.01	-.3104	.34	-.01	-.2146						
.35	-.01	-.3173	.39	-.01	-.1973						
.40	-.01	-.3150	.44	-.01	-.1700						
.45	-.01	-.2886	.49	-.01	-.1258						
.50	-.01	-.2443	.54	-.01	-.0922						
.55	-.01	-.2034	.59	-.01	-.0581						
.60	-.01	-.1607	.64	-.00	-.0565						
.65	-.01	-.1024	.69	-.00	-.0287						
.70	-.00	-.1041	.74	.00	.0028						
.75	-.00	-.0309	.79	.00	.0374						
.80	-.00	.0215	.84	.00	.0663						
.85	.00	.0614									
.90	.00	.0934									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16984

MACH .806

Q 30376.0

ALPW

-.93

BETA

0.00

P1 66746.91

PT1 102384.87

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4039
.05	.05	-.0048
.10	.06	-.1613
.15	.06	-.2179
.20	.07	-.2823
.25	.07	-.3435
.30	.07	-.3819
.35	.07	-.4148
.40	.07	-.4633
.45	.07	-.4890
.50	.07	-.4716
.55	.06	-.4596
.60	.06	-.4193
.65	.05	-.3725
.70	.05	-.3274
.75	.04	-.2729
.80	.03	-.2279
.85	.03	-.1742
.90	.02	-.1050
0.00	.03	.5649
.05	.01	-.4230
.10	.01	-.3148
.15	.00	-.2816
.20	-.00	-.2788
.25	-.00	-.2890
.30	-.01	-.2764
.35	-.01	-.2676
.40	-.01	-.2771
.45	-.01	-.2631
.50	-.01	-.2481
.55	-.01	-.1836
.60	-.01	-.1536
.65	-.01	-.1103
.70	-.00	-.1093
.75	-.00	-.0190
.80	-.00	.0292
.85	.00	.0581
.90	.00	.1038

X/C	Z/C	CP
0.00	.01	.0182
.05	.03	.0378
.10	.04	-.1517
.15	.05	-.2597
.20	.06	-.3276
.25	.06	-.3950
.30	.07	-.4478
.35	.07	-.5002
.40	.07	-.5297
.45	.07	-.5685
.50	.07	-.5102
.55	.06	-.4824
.60	.06	-.4459
.65	.05	-.4476
.70	.05	-.3599
.75	.04	-.3190
.80	.04	-.2272
.85	.03	-.2205
0.00	.01	.5455
.04	-.00	.0234
.09	-.01	-.4177
.14	-.01	-.3165
.19	-.01	-.2590
.24	-.01	-.2367
.29	-.01	-.2102
.34	-.01	-.1924
.39	-.01	-.1754
.44	-.01	-.1557
.49	-.01	-.1499
.54	-.01	-.0792
.59	-.01	-.0481
.64	-.00	-.0474
.69	-.00	-.0148
.74	.00	.0104
.79	.00	.0473
.84	.00	.0788

X/C	Z/C	CP
0.00	-.01	.1084
.11	.03	.0198
.20	.05	.0195
.31	.06	.0069
.40	.07	.0118
.51	.06	.0152
.61	.06	.0161
.71	.05	.0150
0.00	-.01	.0028
.11	-.02	.0176
.21	-.02	.0162
.31	-.02	.0169
.40	-.02	.0169
.51	-.01	.0184
.61	-.01	.0191
.71	-.00	.0166

X/C	Z/C	CP
.11	.01	.0177
.21	.00	.0160
.31	.00	.0166
.41	.01	.0142
.51	.01	.0153
.62	.01	.0149
.71	.00	.5236
.11	-.05	.0184
.22	-.04	.0158
.32	-.03	.0163
.42	-.03	.0140
.51	-.02	.0150
.62	-.01	.0145
.72	-.00	.0178

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16985

MACH .805

Q 30325.0

ALPW

-.51

BETA

0.00

P1 66822.22

PT1 102384.72

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.4570	0.00	.01	.0160	0.00	-.01	.1154	.11	.01	.0072
.05	.05	-.0492	.05	.03	-.0143	.11	.03	.0137	.21	.00	.0181
.10	.06	-.1840	.10	.04	-.2180	.20	.05	.0217	.31	.00	.0134
.15	.06	-.2664	.15	.05	-.3084	.31	.06	.0197	.41	.01	.0115
.20	.07	-.3138	.20	.06	-.3777	.40	.07	.0009	.51	.01	.0165
.25	.07	-.3644	.25	.06	-.4382	.51	.06	.0163	.62	.01	.0178
.30	.07	-.4122	.30	.07	-.4909	.61	.06	-.0071	.71	.00	.5741
.35	.07	-.4583	.35	.07	-.5419	.71	.05	.0077	.11	-.05	.0159
.40	.07	-.4879	.40	.07	-.5696	0.00	-.01	.0108	.22	-.04	.0177
.45	.07	-.5154	.45	.07	-.5848	.11	-.02	.0160	.32	-.03	.0130
.50	.07	-.5075	.50	.07	-.5632	.21	-.02	.0223	.42	-.03	.0110
.55	.06	-.4953	.55	.06	-.5054	.31	-.02	.0217	.51	-.02	.0161
.60	.06	-.4406	.60	.06	-.4495	.40	-.02	.0196	.62	-.01	.0174
.65	.05	-.3930	.65	.05	-.4029	.51	-.01	.0237	.72	-.00	.0177
.70	.05	-.3376	.70	.05	-.3470	.61	-.01	.0288			
.75	.04	-.2799	.75	.04	-.2862	.71	-.00	.0155			
.80	.03	-.2385	.80	.04	-.2309						
.85	.03	-.1773	.85	.03	-.1807						
.90	.02	-.1096	0.00	.01	.5783						
0.00	.03	.5904	.04	-.00	.0213						
.05	.01	-.3786	.09	-.01	-.3237						
.10	.01	-.2790	.14	-.01	-.2554						
.15	.00	-.2525	.19	-.01	-.2257						
.20	-.00	-.2519	.24	-.01	-.2030						
.25	-.00	-.2509	.29	-.01	-.1826						
.30	-.01	-.2623	.34	-.01	-.1713						
.35	-.01	-.2495	.39	-.01	-.1603						
.40	-.01	-.2517	.44	-.01	-.1326						
.45	-.01	-.2439	.49	-.01	-.1278						
.50	-.01	-.2485	.54	-.01	-.0710						
.55	-.01	-.1872	.59	-.01	-.0453						
.60	-.01	-.1477	.64	-.00	-.0421						
.65	-.01	-.1295	.69	-.00	-.0168						
.70	-.00	-.1087	.74	.00	.0203						
.75	-.00	-.0155	.79	.00	.0509						
.80	-.00	.0234	.84	.00	.0806						
.85	.00	.0523									
.90	.00	.1051									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16986

MACH .806

Q 30374.0

ALPW

.02

BETA

0.00:

P1 66748.97

PT1 102384.09

Y/B/2 = .31

$$Y/B/2 = .74$$

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5129
.05	.05	-.1063
.10	.06	-.2409
.15	.06	-.3006
.20	.07	-.3490
.25	.07	-.4021
.30	.07	-.4482
.35	.07	-.4941
.40	.07	-.5318
.45	.07	-.5683
.50	.07	-.5398
.55	.06	-.5056
.60	.06	-.4815
.65	.05	-.4086
.70	.05	-.3410
.75	.04	-.2917
.80	.03	-.2448
.85	.03	-.1797
.90	.02	-.1097
0.00	.03	.6103
.05	.01	-.3078
.10	.01	-.2477
.15	.00	-.2284
.20	-.00	-.2165
.25	-.00	-.2224
.30	-.01	-.2328
.35	-.01	-.2240
.40	-.01	-.2247
.45	-.01	-.2243
.50	-.01	-.2194
.55	-.01	-.1486
.60	-.01	-.1196
.65	-.01	-.1040
.70	-.00	-.0963
.75	-.00	.0007
.80	-.00	.0165
.85	.00	.0368
.90	.00	.1100

X/C	Z/C	CP
0.00	.01	.0149
.05	.03	-.1036
.10	.04	-.2915
.15	.05	-.3766
.20	.06	-.4338
.25	.06	-.4976
.30	.07	-.5572
.35	.07	-.5975
.40	.07	-.6315
.45	.07	-.6348
.50	.07	-.6178
.55	.06	-.5458
.60	.06	-.4690
.65	.05	-.4257
.70	.05	-.3567
.75	.04	-.2971
.80	.04	-.2400
.85	.03	-.1798
0.00	.01	.6160
.04	-.00	.0137
.09	-.01	-.2497
.14	-.01	-.1927
.19	-.01	-.1846
.24	-.01	-.1713
.29	-.01	-.1517
.34	-.01	-.1409
.39	-.01	-.1293
.44	-.01	-.1140
.49	-.01	-.1112
.54	-.01	-.0516
.59	-.01	-.0295
.64	-.00	-.0277
.69	-.00	-.0007
.74	.00	.0296
.79	.00	.0664
.84	.00	.0967

X/C	Z/C	CP
0.00	-.01	.1282
.11	.03	.0308
.20	.05	.0129
.31	.06	.0103
.40	.07	.0200
.51	.06	.0082
.61	.06	.0256
.71	.05	.0188
0.00	-.01	.0134
.11	-.02	.0142
.21	-.02	.0124
.31	-.02	.0121
.40	-.02	.0175
.51	-.01	.0152
.61	-.01	.0148
.71	-.00	.0185

X/C	Z/C	CP
.11	.01	.0109
.21	.00	.0153
.31	.00	.0132
.41	.01	.0170
.51	.01	.0164
.62	.01	.0142
.71	.00	.6214
.11	-.05	.0301
.22	-.04	.0151
.32	-.03	.0131
.42	-.03	.0170
.51	-.02	.0163
.62	-.01	.0141
.72	-.00	.0168

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16987

MACH .808

Q 30435.4 ALPW

.49

BETA

0.00 P1 66658.53

PT1 102384.67

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5504	0.00	.01	.0185	0.00	-.01	.1323	.11	.01	.0186
.05	.05	-.1518	.05	.03	-.1826	.11	.03	.0258	.21	.00	.0153
.10	.06	-.2785	.10	.04	-.3467	.20	.05	.0104	.31	.00	.0181
.15	.06	-.3517	.15	.05	-.4384	.31	.06	.0086	.41	.01	.0127
.20	.07	-.3915	.20	.06	-.4821	.40	.07	.0268	.51	.01	.0229
.25	.07	-.4456	.25	.06	-.5479	.51	.06	.0131	.62	.01	.0151
.30	.07	-.4773	.30	.07	-.5994	.61	.06	.0116	.71	.00	.6359
.35	.07	-.5308	.35	.07	-.6478	.71	.05	.0142	.11	-.05	.0201
.40	.07	-.5752	.40	.07	-.7468	0.00	-.01	.0155	.22	-.04	.0164
.45	.07	-.6115	.45	.07	-.6723	.11	-.02	.0132	.32	-.03	.0180
.50	.07	-.6019	.50	.07	-.6488	.21	-.02	.0153	.42	-.03	.0126
.55	.06	-.5790	.55	.06	-.5917	.31	-.02	.0137	.51	-.02	.0228
.60	.06	-.5135	.60	.06	-.4944	.40	-.02	.0143	.62	-.01	.0150
.65	.05	-.4304	.65	.05	-.4662	.51	-.01	.0192	.72	-.00	.0160
.70	.05	-.3586	.70	.05	-.3695	.61	-.01	.0242			
.75	.04	-.3034	.75	.04	-.3153	.71	-.00	.0140			
.80	.03	-.2530	.80	.04	-.2443						
.85	.03	-.1801	.85	.03	-.1850						
.90	.02	-.1142	0.00	.01	.6388						
0.00	.03	.6207	.04	-.00	.0152						
.05	.01	-.2513	.09	-.01	-.1654						
.10	.01	-.2066	.14	-.01	-.1532						
.15	.00	-.2079	.19	-.01	-.1540						
.20	-.00	-.2067	.24	-.01	-.1340						
.25	-.00	-.2084	.29	-.01	-.1198						
.30	-.01	-.2241	.34	-.01	-.1199						
.35	-.01	-.2169	.39	-.01	-.1129						
.40	-.01	-.2254	.44	-.01	-.0936						
.45	-.01	-.2068	.49	-.01	-.0957						
.50	-.01	-.2050	.54	-.01	-.0368						
.55	-.01	-.1567	.59	-.01	-.0158						
.60	-.01	-.1380	.64	-.00	-.0115						
.65	-.01	-.1228	.69	-.00	.0155						
.70	-.00	-.0986	.74	.00	.0392						
.75	-.00	.0062	.79	.00	.0847						
.80	-.00	.0218	.84	.00	.1040						
.85	.00	.0532									
.90	.00	.1143									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16988

MACH .806

Q

30349.3

ALPH

1.05

BETA

0.00

P1 66783.82

PT1 102382.56

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5953
.05	.05	-.2225
.10	.06	-.3487
.15	.06	-.3943
.20	.07	-.4322
.25	.07	-.4880
.30	.07	-.5103
.35	.07	-.5632
.40	.07	-.6096
.45	.07	-.6450
.50	.07	-.6254
.55	.06	-.6235
.60	.06	-.5352
.65	.05	-.4419
.70	.05	-.3689
.75	.04	-.3066
.80	.03	-.2485
.85	.03	-.1889
.90	.02	-.1158
0.00	.03	.6201
.05	.01	-.1766
.10	.01	-.1577
.15	.00	-.1596
.20	-.00	-.1637
.25	-.00	-.1867
.30	-.01	-.1899
.35	-.01	-.1891
.40	-.01	-.1910
.45	-.01	-.1821
.50	-.01	-.1719
.55	-.01	-.1526
.60	-.01	-.1131
.65	-.01	-.1121
.70	-.00	-.0872
.75	-.00	-.0084
.80	-.00	.0171
.85	.00	.0388
.90	.00	.1278

X/C	Z/C	CP
0.00	.01	.0133
.05	.03	-.2922
.10	.04	-.4489
.15	.05	-.5190
.20	.06	-.5733
.25	.06	-.6273
.30	.07	-.6821
.35	.07	-.7133
.40	.07	-.8017
.45	.07	-.8339
.50	.07	-.7341
.55	.06	-.5796
.60	.06	-.5085
.65	.05	-.4353
.70	.05	-.3748
.75	.04	-.3089
.80	.04	-.2459
.85	.03	-.1791
0.00	.01	.6525
.04	-.00	.0195
.09	-.01	-.1202
.14	-.01	-.0967
.19	-.01	-.0919
.24	-.01	-.0954
.29	-.01	-.0895
.34	-.01	-.0853
.39	-.01	-.0856
.44	-.01	-.0705
.49	-.01	-.0653
.54	-.01	-.0253
.59	-.01	.0015
.64	-.00	.0128
.69	-.00	.0292
.74	.00	.0522
.79	.00	.0978
.84	.00	.1199

X/C	Z/C	CP
0.00	-.01	.1476
.11	.03	.0170
.20	.05	.0077
.31	.06	.0145
.40	.07	.0091
.51	.06	.0310
.61	.06	.0176
.71	.05	.0277
0.00	-.01	.0103
.11	-.02	.0131
.21	-.02	.0162
.31	-.02	.0146
.40	-.02	.0170
.51	-.01	.0224
.61	-.01	.0155
.71	-.00	.0137

X/C	Z/C	CP
.11	.01	.0135
.21	.00	.0125
.31	.00	.0155
.41	.01	.0174
.51	.01	.0159
.62	.01	.0168
.71	.00	.6502
.11	-.05	.0235
.22	-.04	.0120
.32	-.03	.0149
.42	-.03	.0169
.51	-.02	.0153
.62	-.01	.0163
.72	-.00	.0141

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16989

MACH .806

Q 30365.6

ALPW

1.48

BETA

0.00

P1 66756.15

PT1 102379.25

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6113
.05	.05	-.2833
.10	.06	-.3860
.15	.06	-.4204
.20	.07	-.4730
.25	.07	-.5067
.30	.07	-.5426
.35	.07	-.5809
.40	.07	-.6395
.45	.07	-.6875
.50	.07	-.6794
.55	.06	-.6664
.60	.06	-.5662
.65	.05	-.4560
.70	.05	-.3759
.75	.04	-.3112
.80	.03	-.2570
.85	.03	-.1906
.90	.02	-.1106
0.00	.03	.6142
.05	.01	-.1274
.10	.01	-.1216
.15	.00	-.1308
.20	-.00	-.1413
.25	-.00	-.1571
.30	-.01	-.1689
.35	-.01	-.1657
.40	-.01	-.1707
.45	-.01	-.1728
.50	-.01	-.1668
.55	-.01	-.1498
.60	-.01	-.1022
.65	-.01	-.0863
.70	-.00	-.0637
.75	-.00	.0228
.80	-.00	.0218
.85	.00	.0648
.90	.00	.1226

X/C	Z/C	CP
0.00	.01	.0138
.05	.03	-.3453
.10	.04	-.5055
.15	.05	-.5798
.20	.06	-.6462
.25	.06	-.6924
.30	.07	-.7427
.35	.07	-.7803
.40	.07	-.8327
.45	.07	-.8815
.50	.07	-.8112
.55	.06	-.6281
.60	.06	-.4835
.65	.05	-.4805
.70	.05	-.3638
.75	.04	-.3062
.80	.04	-.2490
.85	.03	-.1789
0.00	.01	.6462
.04	-.00	.0199
.09	-.01	-.0843
.14	-.01	-.0737
.19	-.01	-.0732
.24	-.01	-.0737
.29	-.01	-.0691
.34	-.01	-.0686
.39	-.01	-.0712
.44	-.01	-.0554
.49	-.01	-.0574
.54	-.01	-.0126
.59	-.01	.0069
.64	-.00	.0182
.69	-.00	.0450
.74	.00	.0674
.79	.00	.0965
.84	.00	.1203

X/C	Z/C	CP
0.00	-.01	.1439
.11	.03	.0122
.20	.05	.0089
.31	.06	.0197
.40	.07	.0160
.51	.06	.0104
.61	.06	.0114
.71	.05	.0145
0.00	-.01	.0170
.11	-.02	.0136
.21	-.02	.0210
.31	-.02	.0194
.40	-.02	.0159
.51	-.01	.0224
.61	-.01	.0127
.71	-.00	.0187

X/C	Z/C	CP
.11	.01	.0109
.21	.00	.0157
.31	.00	.0133
.41	.01	.0147
.51	.01	.0156
.62	.01	.0121
.71	.00	.6459
.11	-.05	.0213
.22	-.04	.0155
.32	-.03	.0132
.42	-.03	.0145
.51	-.02	.0155
.62	-.01	.0121
.72	-.00	.0164

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16990

MACH .806

Q 30362.9

ALPW

1.47

BETA

0.00

P1 66761.68

PT1 102380.72

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6125
.05	.05	-.2714
.10	.06	-.3816
.15	.06	-.4362
.20	.07	-.4770
.25	.07	-.5137
.30	.07	-.5434
.35	.07	-.5813
.40	.07	-.6358
.45	.07	-.6844
.50	.07	-.6777
.55	.06	-.6406
.60	.06	-.6020
.65	.05	-.4594
.70	.05	-.3705
.75	.04	-.3121
.80	.03	-.2561
.85	.03	-.1896
.90	.02	-.1172
0.00	.03	.6152
.05	.01	-.1387
.10	.01	-.1185
.15	.00	-.1275
.20	-.00	-.1432
.25	-.00	-.1541
.30	-.01	-.1673
.35	-.01	-.1725
.40	-.01	-.1754
.45	-.01	-.1700
.50	-.01	-.1744
.55	-.01	-.1377
.60	-.01	-.1166
.65	-.01	-.0931
.70	-.00	-.0706
.75	-.00	.0165
.80	-.00	.0215
.85	.00	.0565
.90	.00	.1143

X/C	Z/C	CP
0.00	.01	.0116
.05	.03	-.3478
.10	.04	-.5076
.15	.05	-.5780
.20	.06	-.6343
.25	.06	-.6834
.30	.07	-.7487
.35	.07	-.7812
.40	.07	-.8361
.45	.07	-.8832
.50	.07	-.8733
.55	.06	-.7086
.60	.06	-.4831
.65	.05	-.4807
.70	.05	-.3685
.75	.04	-.3343
.80	.04	-.2447
.85	.03	-.1795
0.00	.01	.6247
.04	-.00	.0178
.09	-.01	-.0715
.14	-.01	-.0723
.19	-.01	-.0763
.24	-.01	-.0665
.29	-.01	-.0700
.34	-.01	-.0737
.39	-.01	-.0720
.44	-.01	-.0593
.49	-.01	-.0586
.54	-.01	-.0193
.59	-.01	.0019
.64	-.00	.0082
.69	-.00	.0430
.74	.00	.0672
.79	.00	.0975
.84	.00	.1177

X/C	Z/C	CP
0.00	-.01	.1458
.11	.03	.0216
.20	.05	.0217
.31	.06	.0169
.40	.07	.0073
.51	.06	.0206
.61	.06	.0160
.71	.05	.0146
0.00	-.01	.0160
.11	-.02	.0107
.21	-.02	.0096
.31	-.02	.0086
.40	-.02	.0149
.51	-.01	.0174
.61	-.01	.0109
.71	-.00	.0125

X/C	Z/C	CP
.11	.01	.0176
.21	.00	.0158
.31	.00	.0142
.41	.01	.0178
.51	.01	.0104
.62	.01	.0144
.71	.00	.6460
.11	-.05	.0183
.22	-.04	.0153
.32	-.03	.0136
.42	-.03	.0173
.51	-.02	.0077
.62	-.01	.0138
.72	-.00	.0163

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16991

MACH .806

Q 30358.9

ALPW

1.92

BETA

0.00

P1 66766.51

PT1 102379.74

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6154
.05	.05	-.3334
.10	.06	-.4332
.15	.06	-.4763
.20	.07	-.5090
.25	.07	-.5393
.30	.07	-.5713
.35	.07	-.6150
.40	.07	-.6653
.45	.07	-.7084
.50	.07	-.7122
.55	.06	-.7107
.60	.06	-.6806
.65	.05	-.4889
.70	.05	-.3780
.75	.04	-.3148
.80	.03	-.2629
.85	.03	-.1928
.90	.02	-.1112
0.00	.03	.5988
.05	.01	-.0746
.10	.01	-.0888
.15	.00	-.1028
.20	-.00	-.1117
.25	-.00	-.1273
.30	-.01	-.1416
.35	-.01	-.1525
.40	-.01	-.1584
.45	-.01	-.1497
.50	-.01	-.1626
.55	-.01	-.1188
.60	-.01	-.0917
.65	-.01	-.0921
.70	-.00	-.0652
.75	-.00	.0245
.80	-.00	.0385
.85	.00	.0624
.90	.00	.1260

X/C	Z/C	CP
0.00	.01	.0106
.05	.03	-.4197
.10	.04	-.5752
.15	.05	-.6370
.20	.06	-.6951
.25	.06	-.7476
.30	.07	-.7976
.35	.07	-.8499
.40	.07	-.8881
.45	.07	-.9407
.50	.07	-.9437
.55	.06	-.7618
.60	.06	-.4789
.65	.05	-.4943
.70	.05	-.3623
.75	.04	-.3017
.80	.04	-.2387
.85	.03	-.1728
0.00	.01	.6254
.04	-.00	.0117
.09	-.01	-.0391
.14	-.01	-.0355
.19	-.01	-.0299
.24	-.01	-.0465
.29	-.01	-.0476
.34	-.01	-.0508
.39	-.01	-.0452
.44	-.01	-.0410
.49	-.01	-.0353
.54	-.01	-.0056
.59	-.01	.0175
.64	-.00	.0178
.69	-.00	.0421
.74	.00	.0669
.79	.00	.0979
.84	.00	.1200

X/C	Z/C	CP
0.00	-.01	.1633
.11	.03	.0371
.20	.05	.0123
.31	.06	.0108
.40	.07	.0111
.51	.06	.0184
.61	.06	.0257
.71	.05	.0125
0.00	-.01	.0151
.11	-.02	.0119
.21	-.02	.0083
.31	-.02	.0117
.40	-.02	.0159
.51	-.01	.0096
.61	-.01	.0158
.71	-.00	.0175

X/C	Z/C	CP
.11	.01	.0129
.21	.00	.0144
.31	.00	.0111
.41	.01	.0146
.51	.01	.0130
.62	.01	.0111
.71	.00	.6328
.11	-.05	.0112
.22	-.04	.0142
.32	-.03	.0111
.42	-.03	.0145
.51	-.02	.0128
.62	-.01	.0109
.72	-.00	.0146

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16992

MACH .806

Q 30355.2

ALPW

2.50

BETA

0.00

P1 66770.48

PT1 102378.26

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6166
.05	.05	-.4034
.10	.06	-.4900
.15	.06	-.5174
.20	.07	-.5562
.25	.07	-.5986
.30	.07	-.6069
.35	.07	-.6425
.40	.07	-.6839
.45	.07	-.7423
.50	.07	-.7523
.55	.06	-.7614
.60	.06	-.7486
.65	.05	-.5880
.70	.05	-.3869
.75	.04	-.3195
.80	.03	-.2602
.85	.03	-.1905
.90	.02	-.1157
0.00	.03	.5712
.05	.01	-.0227
.10	.01	-.0477
.15	.00	-.0612
.20	-.00	-.0873
.25	-.00	-.1051
.30	-.01	-.1103
.35	-.01	-.1253
.40	-.01	-.1316
.45	-.01	-.1284
.50	-.01	-.1222
.55	-.01	-.1030
.60	-.01	-.0704
.65	-.01	-.0702
.70	-.00	-.0452
.75	-.00	.0386
.80	-.00	.0397
.85	.00	.0693
.90	.00	.1382

X/C	Z/C	CP
0.00	.01	.0136
.05	.03	-.5360
.10	.04	-.6781
.15	.05	-.7308
.20	.06	-.7626
.25	.06	-.8028
.30	.07	-.8727
.35	.07	-.9026
.40	.07	-.9622
.45	.07	-1.0110
.50	.07	-.9955
.55	.06	-.9524
.60	.06	-.5821
.65	.05	-.4254
.70	.05	-.3444
.75	.04	-.2880
.80	.04	-.2262
.85	.03	-.1661
0.00	.01	.6235
.04	-.00	.0141
.09	-.01	.0269
.14	-.01	.0069
.19	-.01	.0092
.24	-.01	-.0070
.29	-.01	-.0198
.34	-.01	-.0247
.39	-.01	-.0290
.44	-.01	-.0226
.49	-.01	-.0228
.54	-.01	.0134
.59	-.01	.0308
.64	-.00	.0318
.69	-.00	.0594
.74	.00	.0801
.79	.00	.1129
.84	.00	.1352

X/C	Z/C	CP
0.00	-.01	.1572
.11	.03	.0244
.20	.05	.0048
.31	.06	.0132
.40	.07	.0150
.51	.06	.0158
.61	.06	.0124
.71	.05	.0163
0.00	-.01	.0111
.11	-.02	.0131
.21	-.02	.0122
.31	-.02	.0157
.40	-.02	.0119
.51	-.01	.0181
.61	-.01	.0090
.71	-.00	.0107

X/C	Z/C	CP
.11	.01	.0175
.21	.00	.0098
.31	.00	.0147
.41	.01	.0147
.51	.01	.0139
.62	.01	.0168
.71	.00	.6015
.11	-.05	.0099
.22	-.04	.0173
.32	-.03	.0147
.42	-.03	.0147
.51	-.02	.0139
.62	-.01	.0168
.72	-.00	.0107

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16993

MACH .807

Q 30385.2

ALPH

3.07

BETA

0.00

P1 66728.65

PT1 102380.68

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6055	0.00	.01	.0089	0.00	-.01	.1727	.11	.01	.0180
.05	.05	-.4839	.05	.03	-.6466	.11	.03	.0211	.21	.00	.0100
.10	.06	-.5466	.10	.04	-.7782	.20	.05	.0172	.31	.00	.0153
.15	.06	-.5809	.15	.05	-.8329	.31	.06	.0190	.41	.01	.0123
.20	.07	-.5960	.20	.06	-.8422	.40	.07	.0231	.51	.01	.0162
.25	.07	-.6327	.25	.06	-.8706	.51	.06	.0135	.62	.01	.0109
.30	.07	-.6712	.30	.07	-.9224	.61	.06	.0092	.71	.00	.5588
.35	.07	-.6854	.35	.07	-.9653	.71	.05	.0079	.11	-.05	.0122
.40	.07	-.7167	.40	.07	-1.0137	0.00	-.01	.0127	.22	-.04	.0096
.45	.07	-.7749	.45	.07	-1.0642	.11	-.02	.0113	.32	-.03	.0149
.50	.07	-.7842	.50	.07	-1.0941	.21	-.02	.0137	.42	-.03	.0121
.55	.06	-.7968	.55	.06	-1.0303	.31	-.02	.0160	.51	-.02	.0159
.60	.06	-.8021	.60	.06	-.6375	.40	-.02	.0109	.62	-.01	.0106
.65	.05	-.6901	.65	.05	-.4667	.51	-.01	.0091	.72	-.00	.0131
.70	.05	-.4239	.70	.05	-.3731	.61	-.01	.0159			
.75	.04	-.3223	.75	.04	-.2887	.71	-.00	.0104			
.80	.03	-.2594	.80	.04	-.2225						
.85	.03	-.1832	.85	.03	-.1543						
.90	.02	-.1127	0.00	.01	.5625						
0.00	.03	.5116	.04	-.00	.0100						
.05	.01	.0318	.09	-.01	.0765						
.10	.01	-.0002	.14	-.01	.0568						
.15	.00	-.0357	.19	-.01	.0453						
.20	-.00	-.0463	.24	-.01	.0203						
.25	-.00	-.0695	.29	-.01	.0127						
.30	-.01	-.0929	.34	-.01	.0057						
.35	-.01	-.1010	.39	-.01	-.0027						
.40	-.01	-.1070	.44	-.01	.0024						
.45	-.01	-.1123	.49	-.01	.0068						
.50	-.01	-.1180	.54	-.01	.0260						
.55	-.01	-.0711	.59	-.01	.0496						
.60	-.01	-.0552	.64	-.00	.0552						
.65	-.01	-.0475	.69	-.00	.0741						
.70	-.00	-.0277	.74	.00	.0911						
.75	-.00	.0487	.79	.00	.1147						
.80	-.00	.0713	.84	.00	.1289						
.85	.00	.0957									
.90	.00	.1328									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16994

MACH .807

Q 30420.1

ALPW

4.06

BETA

0.00

P1 66682.24

PT1 102385.55

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5639
.05	.05	-.6068
.10	.06	-.6704
.15	.06	-.6773
.20	.07	-.6760
.25	.07	-.7055
.30	.07	-.7396
.35	.07	-.7684
.40	.07	-.8039
.45	.07	-.8151
.50	.07	-.8216
.55	.06	-.8396
.60	.06	-.8504
.65	.05	-.8547
.70	.05	-.5941
.75	.04	-.3478
.80	.03	-.2628
.85	.03	-.1795
.90	.02	-.1082
0.00	.03	.4109
.05	.01	.1198
.10	.01	.0584
.15	.00	.0219
.20	-.00	-.0038
.25	-.00	-.0231
.30	-.01	-.0405
.35	-.01	-.0645
.40	-.01	-.0637
.45	-.01	-.0775
.50	-.01	-.0800
.55	-.01	-.0574
.60	-.01	-.0105
.65	-.01	.0110
.70	-.00	.0019
.75	-.00	.0563
.80	-.00	.0691
.85	.00	.0992
.90	.00	.1378

X/C	Z/C	CP
0.00	.01	.0140
.05	.03	-.8232
.10	.04	-.9070
.15	.05	-.9849
.20	.06	-1.0189
.25	.06	-1.0369
.30	.07	-1.0455
.35	.07	-1.0481
.40	.07	-1.0955
.45	.07	-1.1213
.50	.07	-1.0770
.55	.06	-.8062
.60	.06	-.6392
.65	.05	-.6270
.70	.05	-.4662
.75	.04	-.3630
.80	.04	-.2643
.85	.03	-.1869
0.00	.01	.4486
.04	-.00	.0168
.09	-.01	.1552
.14	-.01	.1088
.19	-.01	.1067
.24	-.01	.0663
.29	-.01	.0516
.34	-.01	.0463
.39	-.01	.0290
.44	-.01	.0370
.49	-.01	.0329
.54	-.01	.0404
.59	-.01	.0674
.64	-.00	.0651
.69	-.00	.0781
.74	.00	.1006
.79	.00	.1227
.84	.00	.1372

X/C	Z/C	CP
0.00	-.01	.1675
.11	.03	.0227
.20	.05	.0143
.31	.06	.0035
.40	.07	.0136
.51	.06	.0046
.61	.06	.0073
.71	.05	.0096
0.00	-.01	.0104
.11	-.02	.0060
.21	-.02	.0060
.31	-.02	.0039
.40	-.02	.0096
.51	-.01	.0100
.61	-.01	.0133
.71	-.00	.0089

X/C	Z/C	CP
.11	.01	.0162
.21	.00	.0080
.31	.00	.0120
.41	.01	.0081
.51	.01	.0153
.62	.01	.0071
.71	.00	.4336
.11	-.05	-.0008
.22	-.04	.0081
.32	-.03	.0119
.42	-.03	.0081
.51	-.02	.0155
.62	-.01	.0070
.72	-.00	.0063

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16995

MACH .808

Q 30434.3

ALPW

5.88

BETA

0.00

P1 66666.89

PT1 102390.54

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4251
.05	.05	-.9350
.10	.06	-.8783
.15	.06	-.8992
.20	.07	-.7700
.25	.07	-.8081
.30	.07	-.8768
.35	.07	-.9033
.40	.07	-.9234
.45	.07	-.9654
.50	.07	-.9987
.55	.06	-.9390
.60	.06	-.9270
.65	.05	-.9310
.70	.05	-.5730
.75	.04	-.3927
.80	.03	-.3174
.85	.03	-.2345
.90	.02	-.1471
0.00	.03	.1716
.05	.01	.2438
.10	.01	.1577
.15	.00	.1075
.20	-.00	.0749
.25	-.00	.0479
.30	-.01	.0315
.35	-.01	.0001
.40	-.01	-.0183
.45	-.01	-.0265
.50	-.01	-.0209
.55	-.01	-.0173
.60	-.01	-.0076
.65	-.01	-.0025
.70	-.00	.0095
.75	-.00	.0608
.80	-.00	.0647
.85	.00	.0803
.90	.00	.1318

X/C	Z/C	CP
0.00	.01	-.0005
.05	.03	-1.2890
.10	.04	-1.2490
.15	.05	-1.2569
.20	.06	-1.2516
.25	.06	-1.2318
.30	.07	-1.2176
.35	.07	-1.1475
.40	.07	-.9898
.45	.07	-.7846
.50	.07	-.6117
.55	.06	-.5284
.60	.06	-.4803
.65	.05	-.4230
.70	.05	-.3959
.75	.04	-.3421
.80	.04	-.3003
.85	.03	-.2860
0.00	.01	.1891
.04	-.00	.0083
.09	-.01	.2392
.14	-.01	.1858
.19	-.01	.1626
.24	-.01	.1209
.29	-.01	.1051
.34	-.01	.0757
.39	-.01	.0593
.44	-.01	.0512
.49	-.01	.0510
.54	-.01	.0620
.59	-.01	.0679
.64	-.00	.0706
.69	-.00	.0765
.74	.00	.0823
.79	.00	.0986
.84	.00	.1126

X/C	Z/C	CP
0.00	-.01	.1153
.11	.03	.0257
.20	.05	-.0060
.31	.06	-.0028
.40	.07	.0021
.51	.06	-.0087
.61	.06	-.0053
.71	.05	.0026
0.00	-.01	.0050
.11	-.02	.0018
.21	-.02	.0036
.31	-.02	.0005
.40	-.02	.0045
.51	-.01	.0022
.61	-.01	.0022
.71	-.00	.0025

X/C	Z/C	CP
.11	.01	.0110
.21	.00	.0055
.31	.00	.0026
.41	.01	.0029
.51	.01	.0011
.62	.01	.0028
.71	.00	.2294
.11	-.05	-.0006
.22	-.04	.0054
.32	-.03	.0026
.42	-.03	.0029
.51	-.02	.0011
.62	-.01	.0029
.72	-.00	.0077

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 10

TP 16996

MACH .807

Q 30395.5

ALPW

-.01

BETA

0.00

P1 66725.32

PT1 102391.69

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5114
.05	.05	-.0949
.10	.06	-.2319
.15	.06	-.2994
.20	.07	-.3536
.25	.07	-.4013
.30	.07	-.4447
.35	.07	-.4882
.40	.07	-.5397
.45	.07	-.5639
.50	.07	-.5616
.55	.06	-.5189
.60	.06	-.4665
.65	.05	-.4137
.70	.05	-.3456
.75	.04	-.2962
.80	.03	-.2421
.85	.03	-.1894
.90	.02	-.1128
0.00	.03	.6069
.05	.01	-.3178
.10	.01	-.2456
.15	.00	-.2328
.20	-.00	-.2261
.25	-.00	-.2301
.30	-.01	-.2306
.35	-.01	-.2247
.40	-.01	-.2336
.45	-.01	-.2248
.50	-.01	-.2111
.55	-.01	-.1505
.60	-.01	-.1174
.65	-.01	-.1130
.70	-.00	-.1003
.75	-.00	.0021
.80	-.00	.0292
.85	.00	.0622
.90	.00	.1173

X/C	Z/C	CP
0.00	.01	.0178
.05	.03	-.0979
.10	.04	-.2779
.15	.05	-.3753
.20	.06	-.4387
.25	.06	-.4960
.30	.07	-.5636
.35	.07	-.5908
.40	.07	-.6226
.45	.07	-.6267
.50	.07	-.6181
.55	.06	-.5572
.60	.06	-.4714
.65	.05	-.4440
.70	.05	-.3542
.75	.04	-.3046
.80	.04	-.2357
.85	.03	-.1766
0.00	.01	.6141
.04	-.00	.0245
.09	-.01	-.2376
.14	-.01	-.2071
.19	-.01	-.1807
.24	-.01	-.1656
.29	-.01	-.1624
.34	-.01	-.1410
.39	-.01	-.1358
.44	-.01	-.1158
.49	-.01	-.1074
.54	-.01	-.0656
.59	-.01	-.0261
.64	-.00	-.0227
.69	-.00	-.0051
.74	.00	.0252
.79	.00	.0773
.84	.00	.0992

X/C	Z/C	CP
0.00	-.01	.1173
.11	.03	.0467
.20	.05	.0120
.31	.06	.0065
.40	.07	.0223
.51	.06	.0205
.61	.06	.0123
.71	.05	.0135
0.00	-.01	.0085
.11	-.02	.0172
.21	-.02	.0106
.31	-.02	.0041
.40	-.02	.0155
.51	-.01	.0142
.61	-.01	.0076
.71	-.00	.0131

X/C	Z/C	CP
.11	.01	.0010
.21	.00	.0136
.31	.00	.0156
.41	.01	.0136
.51	.01	.0110
.62	.01	.0136
.71	.00	.6168
.11	-.05	.0181
.22	-.04	.0134
.32	-.03	.0155
.42	-.03	.0136
.51	-.02	.0110
.62	-.01	.0136
.72	-.00	.0096

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 16999

MACH .754

Q 27951.6

ALPW

-0.02

BETA

0.00

P1 70266.39

PT1 102417.41

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5066
.05	.05	-.1254
.10	.06	-.2445
.15	.06	-.3052
.20	.07	-.3546
.25	.07	-.3922
.30	.07	-.4333
.35	.07	-.4616
.40	.07	-.4864
.45	.07	-.4893
.50	.07	-.4687
.55	.06	-.4428
.60	.06	-.3971
.65	.05	-.3561
.70	.05	-.3168
.75	.04	-.2658
.80	.03	-.2244
.85	.03	-.1719
.90	.02	-.1120
0.00	.03	.6031
.05	.01	-.2824
.10	.01	-.2255
.15	.00	-.2073
.20	-.00	-.2047
.25	-.00	-.2058
.30	-.01	-.2105
.35	-.01	-.2007
.40	-.01	-.2030
.45	-.01	-.2000
.50	-.01	-.1981
.55	-.01	-.1470
.60	-.01	-.1315
.65	-.01	-.1222
.70	-.00	-.0938
.75	-.00	-.0030
.80	-.00	-.0016
.85	.00	.0344
.90	.00	.0938

X/C	Z/C	CP
0.00	.01	.0174
.05	.03	-.1065
.10	.04	-.2694
.15	.05	-.3507
.20	.06	-.4081
.25	.06	-.4492
.30	.07	-.5065
.35	.07	-.5340
.40	.07	-.5643
.45	.07	-.5536
.50	.07	-.5214
.55	.06	-.4819
.60	.06	-.4402
.65	.05	-.4297
.70	.05	-.3427
.75	.04	-.2867
.80	.04	-.2357
.85	.03	-.1795
0.00	.01	.6131
.04	-.00	.0132
.09	-.01	-.2156
.14	-.01	-.1893
.19	-.01	-.1672
.24	-.01	-.1540
.29	-.01	-.1420
.34	-.01	-.1385
.39	-.01	-.1298
.44	-.01	-.1087
.49	-.01	-.0984
.54	-.01	-.0529
.59	-.01	-.0259
.64	-.00	-.0181
.69	-.00	-.0075
.74	.00	.0224
.79	.00	.0544
.84	.00	.0800

X/C	Z/C	CP
0.00	-.01	.1067
.11	.03	.0247
.20	.05	.0110
.31	.06	.0243
.40	.07	.0108
.51	.06	.0182
.61	.06	.0110
.71	.05	.0118
0.00	-.01	.0108
.11	-.02	.0158
.21	-.02	.0157
.31	-.02	.0245
.40	-.02	.0152
.51	-.01	.0124
.61	-.01	.0137
.71	-.00	.0112

X/C	Z/C	CP
.11	.01	.0178
.21	.00	.0126
.31	.00	.0139
.41	.01	.0122
.51	.01	.0101
.62	.01	.0136
.71	.00	.6176
.11	-.05	.0174
.22	-.04	.0122
.32	-.03	.0135
.42	-.03	.0118
.51	-.02	.0097
.62	-.01	.0132
.72	-.00	.0105

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17000

MACH .754

Q 27980.0

ALPW

-2.06

BETA

0.00

P1 70230.99

P11 102421.34

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.1780
.05	.05	.1000
.10	.06	-.0530
.15	.06	-.1392
.20	.07	-.1989
.25	.07	-.2532
.30	.07	-.2969
.35	.07	-.3351
.40	.07	-.3702
.45	.07	-.3849
.50	.07	-.3774
.55	.06	-.3504
.60	.06	-.3337
.65	.05	-.2976
.70	.05	-.2654
.75	.04	-.2370
.80	.03	-.1919
.85	.03	-.1559
.90	.02	-.0945
0.00	.03	.4376
.05	.01	-.5166
.10	.01	-.4021
.15	.00	-.3504
.20	-.00	-.3276
.25	-.00	-.3234
.30	-.01	-.3112
.35	-.01	-.3052
.40	-.01	-.3016
.45	-.01	-.2799
.50	-.01	-.2793
.55	-.01	-.2252
.60	-.01	-.1826
.65	-.01	-.1806
.70	-.00	-.1438
.75	-.00	-.0407
.80	-.00	-.0426
.85	.00	-.0063
.90	.00	.0840

X/C	Z/C	CP
0.00	.01	.0058
.05	.03	.1637
.10	.04	-.0298
.15	.05	-.1374
.20	.06	-.2049
.25	.06	-.2626
.30	.07	-.3175
.35	.07	-.3690
.40	.07	-.4004
.45	.07	-.4158
.50	.07	-.3980
.55	.06	-.3789
.60	.06	-.3582
.65	.05	-.3257
.70	.05	-.2946
.75	.04	-.2809
.80	.04	-.2081
.85	.03	-.1623
0.00	.01	.3497
.04	-.00	.0200
.09	-.01	-.6426
.14	-.01	-.4972
.19	-.01	-.3927
.24	-.01	-.3191
.29	-.01	-.2676
.34	-.01	-.2435
.39	-.01	-.2132
.44	-.01	-.1815
.49	-.01	-.1884
.54	-.01	-.1633
.59	-.01	-.0939
.64	-.00	-.0869
.69	-.00	-.0534
.74	.00	-.0162
.79	.00	.0130
.84	.00	.0438

X/C	Z/C	CP
0.00	-.01	.0666
.11	.03	.0416
.20	.05	.0041
.31	.06	.0181
.40	.07	-.0000
.51	.06	.0042
.61	.06	.0153
.71	.05	.0152
0.00	-.01	.0148
.11	-.02	.0101
.21	-.02	.0156
.31	-.02	.0172
.40	-.02	.0130
.51	-.01	.0133
.61	-.01	.0095
.71	-.00	.0149

X/C	Z/C	CP
.11	.01	.0058
.21	.00	.0124
.31	.00	.0141
.41	.01	.0089
.51	.01	.0139
.62	.01	.0129
.71	.00	.3457
.11	-.05	.0058
.22	-.04	.0123
.32	-.03	.0139
.42	-.03	.0087
.51	-.02	.0138
.62	-.01	.0129
.72	-.00	.0135

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17001

MACH .755

Q 28009.5

ALPW

-1.57

BETA

0.00

P1 70192.92

PT1 102424.30

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.2872	0.00	.01	.0120	0.00	-.01	.0823	.11	.01	.0122
.05	.05	.0545	.05	.03	.1147	.11	.03	.0313	.21	.00	.0133
.10	.06	-.1044	.10	.04	-.0779	.20	.05	.0033	.31	.00	.0121
.15	.06	-.1866	.15	.05	-.1818	.31	.06	.0097	.41	.01	.0096
.20	.07	-.2368	.20	.06	-.2468	.40	.07	.0109	.51	.01	.0116
.25	.07	-.2914	.25	.06	-.2999	.51	.06	.0157	.62	.01	.0132
.30	.07	-.3280	.30	.07	-.3631	.61	.06	.0103	.71	.00	.4180
.35	.07	-.3677	.35	.07	-.4083	.71	.05	.0108	.11	-.05	.0120
.40	.07	-.3943	.40	.07	-.4418	0.00	-.01	.0103	.22	-.04	.0131
.45	.07	-.4092	.45	.07	-.4467	.11	-.02	.0106	.32	-.03	.0119
.50	.07	-.3914	.50	.07	-.4332	.21	-.02	.0162	.42	-.03	.0095
.55	.06	-.3760	.55	.06	-.4014	.31	-.02	.0109	.51	-.02	.0115
.60	.06	-.3544	.60	.06	-.3806	.40	-.02	.0129	.62	-.01	.0132
.65	.05	-.3125	.65	.05	-.3755	.51	-.01	.0121	.72	-.00	.0101
.70	.05	-.2747	.70	.05	-.3025	.61	-.01	.0107			
.75	.04	-.2471	.75	.04	-.2579	.71	-.00	.0105			
.80	.03	-.2062	.80	.04	-.2152						
.85	.03	-.1589	.85	.03	-.1624						
.90	.02	-.1041	0.00	.01	.4183						
0.00	.03	.4989	.04	-.00	.0276						
.05	.01	-.4745	.09	-.01	-.4985						
.10	.01	-.3530	.14	-.01	-.3681						
.15	.00	-.3166	.19	-.01	-.3354						
.20	-.00	-.2939	.24	-.01	-.2690						
.25	-.00	-.2898	.29	-.01	-.2315						
.30	-.01	-.2900	.34	-.01	-.2119						
.35	-.01	-.2686	.39	-.01	-.1931						
.40	-.01	-.2703	.44	-.01	-.1663						
.45	-.01	-.2618	.49	-.01	-.1596						
.50	-.01	-.2539	.54	-.01	-.0975						
.55	-.01	-.2209	.59	-.01	-.0559						
.60	-.01	-.1918	.64	-.00	-.0582						
.65	-.01	-.1757	.69	-.00	-.0364						
.70	-.00	-.1392	.74	.00	-.0122						
.75	-.00	-.0428	.79	.00	.0259						
.80	-.00	-.0229	.84	.00	.0594						
.85	.00	-.0052									
.90	.00	.0828									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17002

MACH .755

Q 27988.8

ALPW

-1.04

BETA

0.00

P1 70219.92

PT1 102422.55

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.3584
.05	.05	.0034
.10	.06	-.1489
.15	.06	-.2144
.20	.07	-.2737
.25	.07	-.3263
.30	.07	-.3625
.35	.07	-.4041
.40	.07	-.4194
.45	.07	-.4298
.50	.07	-.4155
.55	.06	-.3998
.60	.06	-.3667
.65	.05	-.3316
.70	.05	-.2881
.75	.04	-.2599
.80	.03	-.2149
.85	.03	-.1643
.90	.02	-.1118
0.00	.03	.5446
.05	.01	-.4390
.10	.01	-.3000
.15	.00	-.2749
.20	-.00	-.2595
.25	-.00	-.2631
.30	-.01	-.2593
.35	-.01	-.2563
.40	-.01	-.2522
.45	-.01	-.2418
.50	-.01	-.2384
.55	-.01	-.2084
.60	-.01	-.1711
.65	-.01	-.1576
.70	-.00	-.1268
.75	-.00	-.0233
.80	-.00	-.0224
.85	.00	.0006
.90	.00	.0929

X/C	Z/C	CP
0.00	.01	.0106
.05	.03	.0472
.10	.04	-.1384
.15	.05	-.2444
.20	.06	-.3044
.25	.06	-.3634
.30	.07	-.4107
.35	.07	-.4451
.40	.07	-.4790
.45	.07	-.4754
.50	.07	-.4515
.55	.06	-.4214
.60	.06	-.3985
.65	.05	-.3513
.70	.05	-.3200
.75	.04	-.2657
.80	.04	-.2189
.85	.03	-.1666
0.00	.01	.4881
.04	-.00	.0182
.09	-.01	-.3708
.14	-.01	-.2746
.19	-.01	-.2486
.24	-.01	-.2220
.29	-.01	-.1992
.34	-.01	-.1892
.39	-.01	-.1770
.44	-.01	-.1504
.49	-.01	-.1435
.54	-.01	-.0867
.59	-.01	-.0557
.64	-.00	-.0518
.69	-.00	-.0212
.74	.00	.0041
.79	.00	.0367
.84	.00	.0680

X/C	Z/C	CP
0.00	-.01	.0984
.11	.03	.0359
.20	.05	.0062
.31	.06	.0100
.40	.07	.0126
.51	.06	.0096
.61	.06	.0153
.71	.05	.0080
0.00	-.01	.0122
.11	-.02	.0121
.21	-.02	.0141
.31	-.02	.0111
.40	-.02	.0110
.51	-.01	.0193
.61	-.01	.0138
.71	-.00	.0078

X/C	Z/C	CP
.11	.01	.0107
.21	.00	.0129
.31	.00	.0133
.41	.01	.0173
.51	.01	.0123
.62	.01	.0110
.71	.00	.5076
.11	-.05	.0104
.22	-.04	.0126
.32	-.03	.0131
.42	-.03	.0173
.51	-.02	.0122
.62	-.01	.0106
.72	-.00	.0123

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17003

MACH .754

Q 27959.6

ALPW

-.59

BETA

0.00

P1 70265.26

PT1 102426.82

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4408
.05	.05	-.0469
.10	.06	-.1878
.15	.06	-.2513
.20	.07	-.3056
.25	.07	-.3563
.30	.07	-.3990
.35	.07	-.4235
.40	.07	-.4485
.45	.07	-.4564
.50	.07	-.4378
.55	.06	-.4161
.60	.06	-.3863
.65	.05	-.3462
.70	.05	-.2998
.75	.04	-.2655
.80	.03	-.2189
.85	.03	-.1685
.90	.02	-.1068
0.00	.03	.5789
.05	.01	-.3609
.10	.01	-.2702
.15	.00	-.2309
.20	-.00	-.2348
.25	-.00	-.2370
.30	-.01	-.2420
.35	-.01	-.2392
.40	-.01	-.2410
.45	-.01	-.2196
.50	-.01	-.2298
.55	-.01	-.2093
.60	-.01	-.1847
.65	-.01	-.1507
.70	-.00	-.1168
.75	-.00	-.0285
.80	-.00	-.0174
.85	.00	.0058
.90	.00	.0875

X/C	Z/C	CP
0.00	.01	.0141
.05	.03	-.0158
.10	.04	-.2004
.15	.05	-.2863
.20	.06	-.3493
.25	.06	-.3954
.30	.07	-.4483
.35	.07	-.4842
.40	.07	-.5104
.45	.07	-.5093
.50	.07	-.4759
.55	.06	-.4511
.60	.06	-.4202
.65	.05	-.3789
.70	.05	-.3279
.75	.04	-.2789
.80	.04	-.2265
.85	.03	-.1725
0.00	.01	.5380
.04	-.00	.0107
.09	-.01	-.2910
.14	-.01	-.2416
.19	-.01	-.2394
.24	-.01	-.1947
.29	-.01	-.1793
.34	-.01	-.1637
.39	-.01	-.1510
.44	-.01	-.1309
.49	-.01	-.1236
.54	-.01	-.0685
.59	-.01	-.0320
.64	-.00	-.0382
.69	-.00	-.0145
.74	.00	.0094
.79	.00	.0628
.84	.00	.0751

X/C	Z/C	CP
0.00	-.01	.1054
.11	.03	.0221
.20	.05	.0167
.31	.06	.0210
.40	.07	.0120
.51	.06	.0190
.61	.06	.0040
.71	.05	.0142
0.00	-.01	.0128
.11	-.02	.0093
.21	-.02	.0123
.31	-.02	.0177
.40	-.02	.0161
.51	-.01	.0105
.61	-.01	.0119
.71	-.00	.0139

X/C	Z/C	CP
.11	.01	.0143
.21	.00	.0129
.31	.00	.0087
.41	.01	.0138
.51	.01	.0097
.62	.01	.0113
.71	.00	.5592
.11	-.05	.0142
.22	-.04	.0126
.32	-.03	.0084
.42	-.03	.0135
.51	-.02	.0094
.62	-.01	.0110
.72	-.00	.0106

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17004

MACH .755

Q 27994.7

ALPW

-02

BETA

0.00

P1 70213.75

PT1 102424.45

$$Y/B/2 = .31$$

Y/B/2 = .74

$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.5124
.05	.05	-.1165
.10	.06	-.2467
.15	.06	-.3077
.20	.07	-.3413
.25	.07	-.3983
.30	.07	-.4344
.35	.07	-.4615
.40	.07	-.4872
.45	.07	-.4917
.50	.07	-.4704
.55	.06	-.4497
.60	.06	-.4028
.65	.05	-.3644
.70	.05	-.3129
.75	.04	-.2812
.80	.03	-.2267
.85	.03	-.1701
.90	.02	-.1143
0.00	.03	.6020
.05	.01	-.2979
.10	.01	-.2279
.15	.00	-.2109
.20	-.00	-.1933
.25	-.00	-.2104
.30	-.01	-.2074
.35	-.01	-.2074
.40	-.01	-.2086
.45	-.01	-.2029
.50	-.01	-.2082
.55	-.01	-.1886
.60	-.01	-.1637
.65	-.01	-.1390
.70	-.00	-.1046
.75	-.00	-.0119
.80	-.00	-.0101
.85	.00	.0110
.90	.00	.0927

X/C	Z/C	CP
0.00	.01	.0118
.05	.03	-.1085
.10	.04	-.2729
.15	.05	-.3603
.20	.06	-.4137
.25	.06	-.4589
.30	.07	-.5039
.35	.07	-.5362
.40	.07	-.5661
.45	.07	-.5491
.50	.07	-.5221
.55	.06	-.4711
.60	.06	-.4452
.65	.05	-.4339
.70	.05	-.3438
.75	.04	-.2928
.80	.04	-.2362
.85	.03	-.1794
0.00	.01	.6003
.04	-.00	.0304
.09	-.01	-.2340
.14	-.01	-.1829
.19	-.01	-.1850
.24	-.01	-.1545
.29	-.01	-.1378
.34	-.01	-.1341
.39	-.01	-.1309
.44	-.01	-.1068
.49	-.01	-.0964
.54	-.01	-.0584
.59	-.01	-.0204
.64	-.00	-.0205
.69	-.00	.0006
.74	.00	.0213
.79	.00	.0507
.84	.00	.0792

X/C	Z/C	CP
0.00	-.01	.1103
.11	.03	.0213
.20	.05	.0100
.31	.06	.0167
.40	.07	.0128
.51	.06	.0139
.61	.06	.0104
.71	.05	.0117
0.00	-.01	.0084
.11	-.02	.0133
.21	-.02	.0157
.31	-.02	.0156
.40	-.02	.0122
.51	-.01	.0136
.61	-.01	.0171
.71	-.00	.0113

X/C	Z/C	CP
.11	.01	.0116
.21	.00	.0111
.31	.00	.0118
.41	.01	.0110
.51	.01	.0116
.62	.01	.0137
.71	.00	.6216
.11	-.05	.0115
.22	-.04	.0107
.32	-.03	.0116
.42	-.03	.0107
.51	-.02	.0113
.62	-.01	.0134
.72	-.00	.0146

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17005

MACH .754

Q 27984.4

ALPW

.48

BETA

0.00

P1 70225.70

PT1 102422.21

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5628
.05	.05	-.1736
.10	.06	-.2886
.15	.06	-.3446
.20	.07	-.3862
.25	.07	-.4343
.30	.07	-.4662
.35	.07	-.4891
.40	.07	-.5219
.45	.07	-.5117
.50	.07	-.4944
.55	.06	-.4691
.60	.06	-.4310
.65	.05	-.3790
.70	.05	-.3207
.75	.04	-.2930
.80	.03	-.2331
.85	.03	-.1805
.90	.02	-.1148
0.00	.03	.6171
.05	.01	-.2321
.10	.01	-.1931
.15	.00	-.1826
.20	-.00	-.1810
.25	-.00	-.1883
.30	-.01	-.1962
.35	-.01	-.1952
.40	-.01	-.1967
.45	-.01	-.1811
.50	-.01	-.1899
.55	-.01	-.1691
.60	-.01	-.1444
.65	-.01	-.1227
.70	-.00	-.0936
.75	-.00	-.0163
.80	-.00	-.0067
.85	.00	.0211
.90	.00	.0967

X/C	Z/C	CP
0.00	.01	.0167
.05	.03	-.1823
.10	.04	-.3416
.15	.05	-.4188
.20	.06	-.4708
.25	.06	-.5121
.30	.07	-.5640
.35	.07	-.5842
.40	.07	-.6059
.45	.07	-.5887
.50	.07	-.5503
.55	.06	-.5012
.60	.06	-.4635
.65	.05	-.4196
.70	.05	-.3498
.75	.04	-.3040
.80	.04	-.2397
.85	.03	-.1862
0.00	.01	.6067
.04	-.00	.0119
.09	-.01	-.1628
.14	-.01	-.1359
.19	-.01	-.1307
.24	-.01	-.1205
.29	-.01	-.1164
.34	-.01	-.1086
.39	-.01	-.1063
.44	-.01	-.0893
.49	-.01	-.0793
.54	-.01	-.0363
.59	-.01	-.0139
.64	-.00	-.0115
.69	-.00	.0068
.74	.00	.0344
.79	.00	.0634
.84	.00	.0872

X/C	Z/C	CP
0.00	-.01	.1183
.11	.03	.0249
.20	.05	.0044
.31	.06	.0080
.40	.07	.0240
.51	.06	.0012
.61	.06	.0106
.71	.05	.0122
0.00	-.01	.0078
.11	-.02	.0091
.21	-.02	.0137
.31	-.02	.0089
.40	-.02	.0112
.51	-.01	.0180
.61	-.01	.0108
.71	-.00	.0118

X/C	Z/C	CP
.11	.01	.0171
.21	.00	.0112
.31	.00	.0131
.41	.01	.0120
.51	.01	.0102
.62	.01	.0132
.71	.00	.6378
.11	-.05	.0167
.22	-.04	.0109
.32	-.03	.0128
.42	-.03	.0117
.51	-.02	.0099
.62	-.01	.0128
.72	-.00	.0078

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17006

MACH .754

Q 27975.7

ALPW

.95

-BETA

0.00

P1 70234.04

PT1 102418.61

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5916
.05	.05	-.2449
.10	.06	-.3383
.15	.06	-.3863
.20	.07	-.4196
.25	.07	-.4639
.30	.07	-.5050
.35	.07	-.5218
.40	.07	-.5504
.45	.07	-.5410
.50	.07	-.5212
.55	.06	-.4830
.60	.06	-.4422
.65	.05	-.3949
.70	.05	-.3338
.75	.04	-.2983
.80	.03	-.2366
.85	.03	-.1857
.90	.02	-.1177
0.00	.03	.6157
.05	.01	-.1707
.10	.01	-.1449
.15	.00	-.1475
.20	-.00	-.1510
.25	-.00	-.1598
.30	-.01	-.1735
.35	-.01	-.1714
.40	-.01	-.1776
.45	-.01	-.1620
.50	-.01	-.1637
.55	-.01	-.1445
.60	-.01	-.1277
.65	-.01	-.1095
.70	-.00	-.0864
.75	-.00	.0021
.80	-.00	.0008
.85	.00	.0288
.90	.00	.1082

X/C	Z/C	CP
0.00	.01	.0099
.05	.03	-.2728
.10	.04	-.4196
.15	.05	-.4855
.20	.06	-.5308
.25	.06	-.5720
.30	.07	-.5980
.35	.07	-.6229
.40	.07	-.6556
.45	.07	-.6225
.50	.07	-.5732
.55	.06	-.5251
.60	.06	-.4784
.65	.05	-.4155
.70	.05	-.3621
.75	.04	-.3103
.80	.04	-.2446
.85	.03	-.1904
0.00	.01	.6172
.04	-.00	.0245
.09	-.01	-.0968
.14	-.01	-.1053
.19	-.01	-.0912
.24	-.01	-.0975
.29	-.01	-.0823
.34	-.01	-.0837
.39	-.01	-.0858
.44	-.01	-.0634
.49	-.01	-.0601
.54	-.01	-.0187
.59	-.01	.0041
.64	-.00	.0081
.69	-.00	.0222
.74	.00	.0462
.79	.00	.0769
.84	.00	.1041

X/C	Z/C	CP
0.00	-.01	.1331
.11	.03	.0269
.20	.05	.0004
.31	.06	-.0055
.40	.07	.0115
.51	.06	.0110
.61	.06	.0124
.71	.05	.0114
0.00	-.01	.0110
.11	-.02	.0113
.21	-.02	.0112
.31	-.02	-.0058
.40	-.02	.0127
.51	-.01	.0088
.61	-.01	.0093
.71	-.00	.0111

X/C	Z/C	CP
.11	.01	.0100
.21	.00	.0123
.31	.00	.0125
.41	.01	.0132
.51	.01	.0106
.62	.01	.0094
.71	.00	.6464
.11	-.05	.0097
.22	-.04	.0120
.32	-.03	.0122
.42	-.03	.0128
.51	-.02	.0103
.62	-.01	.0091
.72	-.00	.0127

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17007

MACH .754

Q 27957.6

ALPW

1.46

BETA

0.00

P1 70266.28

PT1 102425.11

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6089	0.00	.01	.0134	0.00	-.01	.1519	.11	.01	.0139
.05	.05	-.3032	.05	.03	-.3675	.11	.03	.0298	.21	.00	.0128
.10	.06	-.3957	.10	.04	-.5159	.20	.05	.0077	.31	.00	.0110
.15	.06	-.4295	.15	.05	-.5640	.31	.06	.0203	.41	.01	.0117
.20	.07	-.4684	.20	.06	-.6095	.40	.07	.0136	.51	.01	.0088
.25	.07	-.5044	.25	.06	-.6268	.51	.06	.0131	.62	.01	.0133
.30	.07	-.5329	.30	.07	-.6582	.61	.06	.0125	.71	.00	.6426
.35	.07	-.5584	.35	.07	-.6778	.71	.05	.0121	.11	-.05	.0133
.40	.07	-.5830	.40	.07	-.6898	0.00	-.01	.0128	.22	-.04	.0123
.45	.07	-.5770	.45	.07	-.6745	.11	-.02	.0076	.32	-.03	.0107
.50	.07	-.5484	.50	.07	-.6038	.21	-.02	.0140	.42	-.03	.0114
.55	.06	-.4956	.55	.06	-.5541	.31	-.02	.0222	.51	-.02	.0086
.60	.06	-.4656	.60	.06	-.5011	.40	-.02	.0082	.62	-.01	.0129
.65	.05	-.4034	.65	.05	-.4879	.51	-.01	.0102	.72	-.00	.0131
.70	.05	-.3452	.70	.05	-.3789	.61	-.01	.0083			
.75	.04	-.3125	.75	.04	-.3178	.71	-.00	.0115			
.80	.03	-.2440	.80	.04	-.2529						
.85	.03	-.1910	.85	.03	-.1917						
.90	.02	-.1185	0.00	.01	.6285						
0.00	.03	.6013	.04	-.00	.0089						
.05	.01	-.1122	.09	-.01	-.0450						
.10	.01	-.1107	.14	-.01	-.0661						
.15	.00	-.1153	.19	-.01	-.0669						
.20	-.00	-.1287	.24	-.01	-.0672						
.25	-.00	-.1390	.29	-.01	-.0672						
.30	-.01	-.1405	.34	-.01	-.0641						
.35	-.01	-.1517	.39	-.01	-.0681						
.40	-.01	-.1470	.44	-.01	-.0562						
.45	-.01	-.1478	.49	-.01	-.0583						
.50	-.01	-.1435	.54	-.01	-.0090						
.55	-.01	-.1349	.59	-.01	.0079						
.60	-.01	-.1104	.64	-.00	.0103						
.65	-.01	-.0960	.69	-.00	.0353						
.70	-.00	-.0652	.74	.00	.0608						
.75	-.00	.0197	.79	.00	.0831						
.80	-.00	.0233	.84	.00	.1121						
.85	.00	.0405									
.90	.00	.1158									

7 X 10 HIGH SPEED TUNNEL

TFST 107

RUN 11

TP 17008

MACH .755

Q 27993.4

ALPW

1.91

BETA

0.00

P1 70227.54

PT1 102435.73

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6137
.05	.05	-.3599
.10	.06	-.4509
.15	.06	-.4737
.20	.07	-.5064
.25	.07	-.5399
.30	.07	-.5698
.35	.07	-.5935
.40	.07	-.6114
.45	.07	-.6043
.50	.07	-.5685
.55	.06	-.5250
.60	.06	-.4747
.65	.05	-.4195
.70	.05	-.3533
.75	.04	-.3235
.80	.03	-.2492
.85	.03	-.1900
.90	.02	-.1241
0.00	.03	.5763
.05	.01	-.0608
.10	.01	-.0753
.15	.00	-.0910
.20	-.00	-.1014
.25	-.00	-.1119
.30	-.01	-.1182
.35	-.01	-.1281
.40	-.01	-.1320
.45	-.01	-.1337
.50	-.01	-.1283
.55	-.01	-.1153
.60	-.01	-.1017
.65	-.01	-.0806
.70	-.00	-.0560
.75	-.00	.0338
.80	-.00	.0316
.85	.00	.0498
.90	.00	.1193

X/C	Z/C	CP
0.00	.01	.0125
.05	.03	-.4570
.10	.04	-.5889
.15	.05	-.6231
.20	.06	-.6551
.25	.06	-.6717
.30	.07	-.7104
.35	.07	-.7056
.40	.07	-.7428
.45	.07	-.7125
.50	.07	-.6294
.55	.06	-.5707
.60	.06	-.5110
.65	.05	-.4431
.70	.05	-.3854
.75	.04	-.3206
.80	.04	-.2547
.85	.03	-.1905
0.00	.01	.6403
.04	-.00	.0214
.09	-.01	-.0250
.14	-.01	-.0236
.19	-.01	-.0235
.24	-.01	-.0357
.29	-.01	-.0390
.34	-.01	-.0437
.39	-.01	-.0465
.44	-.01	-.0377
.49	-.01	-.0274
.54	-.01	-.0011
.59	-.01	.0183
.64	-.00	.0180
.69	-.00	.0485
.74	.00	.0648
.79	.00	.1070
.84	.00	.1216

X/C	Z/C	CP
0.00	-.01	.1428
.11	.03	.0276
.20	.05	.0109
.31	.06	.0092
.40	.07	.0190
.51	.06	.0096
.61	.06	.0147
.71	.05	.0089
0.00	-.01	.0105
.11	-.02	.0086
.21	-.02	.0102
.31	-.02	.0088
.40	-.02	.0064
.51	-.01	.0022
.61	-.01	.0116
.71	-.00	.0085

X/C	Z/C	CP
.11	.01	.0125
.21	.00	.0122
.31	.00	.0059
.41	.01	.0143
.51	.01	.0113
.62	.01	.0112
.71	.00	.6293
.11	-.05	.0123
.22	-.04	.0119
.32	-.03	.0056
.42	-.03	.0140
.51	-.02	.0110
.62	-.01	.0109
.72	-.00	.0115

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17009

MACH .754

Q 27974.9

ALPW

2.48

BETA

0.00

P1 70260.62

PT1 102442.48

Y/B/2 = .31

Y/R/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6047
.05	.05	-.4470
.10	.06	-.5218
.15	.06	-.5386
.20	.07	-.5544
.25	.07	-.5865
.30	.07	-.6118
.35	.07	-.6316
.40	.07	-.6722
.45	.07	-.6455
.50	.07	-.6016
.55	.06	-.5509
.60	.06	-.4989
.65	.05	-.4363
.70	.05	-.3679
.75	.04	-.3125
.80	.03	-.2582
.85	.03	-.1941
.90	.02	-.1254
0.00	.03	.5350
.05	.01	.0034
.10	.01	-.0290
.15	.00	-.0544
.20	-.00	-.0708
.25	-.00	-.0877
.30	-.01	-.1004
.35	-.01	-.1155
.40	-.01	-.1094
.45	-.01	-.1111
.50	-.01	-.1126
.55	-.01	-.1025
.60	-.01	-.0850
.65	-.01	-.0650
.70	-.00	-.0453
.75	-.00	.0234
.80	-.00	.0256
.85	.00	.0460
.90	.00	.1196

X/C	Z/C	CP
0.00	.01	.0110
.05	.03	-.5702
.10	.04	-.6951
.15	.05	-.7066
.20	.06	-.7371
.25	.06	-.7641
.30	.07	-.7789
.35	.07	-.7886
.40	.07	-.7791
.45	.07	-.7696
.50	.07	-.6845
.55	.06	-.5898
.60	.06	-.5306
.65	.05	-.4613
.70	.05	-.3907
.75	.04	-.3356
.80	.04	-.2563
.85	.03	-.1907
0.00	.01	.5825
.04	-.00	.0264
.09	-.01	.0271
.14	-.01	.0256
.19	-.01	.0102
.24	-.01	-.0062
.29	-.01	-.0118
.34	-.01	-.0219
.39	-.01	-.0197
.44	-.01	-.0161
.49	-.01	-.0070
.54	-.01	.0207
.59	-.01	.0339
.64	-.00	.0331
.69	-.00	.0608
.74	.00	.0840
.79	.00	.0973
.84	.00	.1214

X/C	Z/C	CP
0.00	-.01	.1411
.11	.03	.0290
.20	.05	.0103
.31	.06	.0174
.40	.07	.0040
.51	.06	.0221
.61	.06	.0127
.71	.05	.0089
0.00	-.01	.0087
.11	-.02	.0074
.21	-.02	.0113
.31	-.02	.0116
.40	-.02	.0125
.51	-.01	.0106
.61	-.01	.0097
.71	-.00	.0084

X/C	Z/C	CP
.11	.01	.0113
.21	.00	.0111
.31	.00	.0095
.41	.01	.0123
.51	.01	.0089
.62	.01	.0078
.71	.00	.5831
.11	-.05	.0108
.22	-.04	.0107
.32	-.03	.0091
.42	-.03	.0120
.51	-.02	.0086
.62	-.01	.0075
.72	-.00	.0122

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17010

MACH .754

Q 27967.1

ALPW

2.95

BETA

0.00

P1 70280.36

PT1 102450.76

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5938
.05	.05	-.5124
.10	.06	-.5758
.15	.06	-.5864
.20	.07	-.5969
.25	.07	-.6248
.30	.07	-.6315
.35	.07	-.6675
.40	.07	-.6936
.45	.07	-.6717
.50	.07	-.6284
.55	.06	-.5730
.60	.06	-.5168
.65	.05	-.4474
.70	.05	-.3734
.75	.04	-.3227
.80	.03	-.2601
.85	.03	-.2025
.90	.02	-.1257
0.00	.03	.4885
.05	.01	.0435
.10	.01	.0069
.15	.00	-.0293
.20	-.00	-.0428
.25	-.00	-.0635
.30	-.01	-.0761
.35	-.01	-.0940
.40	-.01	-.0871
.45	-.01	-.0961
.50	-.01	-.1011
.55	-.01	-.0919
.60	-.01	-.0424
.65	-.01	-.0420
.70	-.00	-.0278
.75	-.00	.0442
.80	-.00	.0460
.85	.00	.0662
.90	.00	.1310

X/C	Z/C	CP
0.00	.01	.0115
.05	.03	-.6855
.10	.04	-.7687
.15	.05	-.8045
.20	.06	-.8170
.25	.06	-.8209
.30	.07	-.8556
.35	.07	-.8287
.40	.07	-.8274
.45	.07	-.7950
.50	.07	-.7087
.55	.06	-.6033
.60	.06	-.5420
.65	.05	-.4658
.70	.05	-.3976
.75	.04	-.3327
.80	.04	-.2567
.85	.03	-.1918
0.00	.01	.5605
.04	-.00	.0083
.09	-.01	.0681
.14	-.01	.0578
.19	-.01	.0550
.24	-.01	.0248
.29	-.01	.0102
.34	-.01	.0045
.39	-.01	-.0003
.44	-.01	.0018
.49	-.01	.0157
.54	-.01	.0345
.59	-.01	.0470
.64	-.00	.0524
.69	-.00	.0740
.74	.00	.0903
.79	.00	.1086
.84	.00	.1264

X/C	Z/C	CP
0.00	-.01	.1437
.11	.03	.0425
.20	.05	.0158
.31	.06	.0104
.40	.07	.0180
.51	.06	.0071
.61	.06	.0143
.71	.05	.0093
0.00	-.01	.0097
.11	-.02	.0047
.21	-.02	.0089
.31	-.02	.0067
.40	-.02	.0096
.51	-.01	.0155
.61	-.01	.0064
.71	-.00	.0091

X/C	Z/C	CP
.11	.01	.0114
.21	.00	.0092
.31	.00	.0098
.41	.01	.0083
.51	.01	.0079
.62	.01	.0114
.71	.00	.5205
.11	-.05	.0111
.22	-.04	.0090
.32	-.03	.0096
.42	-.03	.0080
.51	-.02	.0076
.62	-.01	.0110
.72	-.00	.0091

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17011

MACH .755

0

28030.1

ALPW

4.00

BETA

0.00

P1 70205.21

PT1 102462.86

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5370
.05	.05	-.6888
.10	.06	-.7074
.15	.06	-.6923
.20	.07	-.6915
.25	.07	-.6779
.30	.07	-.7269
.35	.07	-.7467
.40	.07	-.7770
.45	.07	-.7844
.50	.07	-.6855
.55	.06	-.6208
.60	.06	-.5417
.65	.05	-.4640
.70	.05	-.3957
.75	.04	-.3306
.80	.03	-.2713
.85	.03	-.2000
.90	.02	-.1273
0.00	.03	.3431
.05	.01	.1363
.10	.01	.0686
.15	.00	.0364
.20	-.00	.0062
.25	-.00	-.0137
.30	-.01	-.0283
.35	-.01	-.0530
.40	-.01	-.0497
.45	-.01	-.0612
.50	-.01	-.0809
.55	-.01	-.0606
.60	-.01	-.0512
.65	-.01	-.0365
.70	-.00	-.0115
.75	-.00	.0628
.80	-.00	.0629
.85	.00	.0731
.90	.00	.1405

X/C	Z/C	CP
0.00	.01	.0088
.05	.03	-.9292
.10	.04	-.9903
.15	.05	-1.0345
.20	.06	-.9779
.25	.06	-.9919
.30	.07	-.9995
.35	.07	-1.0034
.40	.07	-.9846
.45	.07	-.9049
.50	.07	-.6792
.55	.06	-.6209
.60	.06	-.5491
.65	.05	-.4765
.70	.05	-.4059
.75	.04	-.3314
.80	.04	-.2606
.85	.03	-.1886
0.00	.01	.3534
.04	-.00	.0076
.09	-.01	.1667
.14	-.01	.1304
.19	-.01	.1082
.24	-.01	.0800
.29	-.01	.0652
.34	-.01	.0487
.39	-.01	.0398
.44	-.01	.0359
.49	-.01	.0447
.54	-.01	.0602
.59	-.01	.0722
.64	-.00	.0804
.69	-.00	.0951
.74	.00	.1076
.79	.00	.1253
.84	.00	.1344

X/C	Z/C	CP
0.00	-.01	.1611
.11	.03	.0301
.20	.05	.0071
.31	.06	.0093
.40	.07	-.0014
.51	.06	.0047
.61	.06	.0092
.71	.05	.0059
0.00	-.01	.0077
.11	-.02	.0095
.21	-.02	.0106
.31	-.02	.0088
.40	-.02	.0091
.51	-.01	.0068
.61	-.01	.0086
.71	-.00	.0055

X/C	Z/C	CP
.11	.01	.0090
.21	.00	.0077
.31	.00	.0114
.41	.01	.0095
.51	.01	.0107
.62	.01	.0082
.71	.00	.3553
.11	-.05	.0086
.22	-.04	.0071
.32	-.03	.0110
.42	-.03	.0090
.51	-.02	.0103
.62	-.01	.0078
.72	-.00	.0102

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17012

MACH .755

Q 28018.1

ALPW

6.02

BETA

0.00

P1 70223.77

PT1 102464.53

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.3066
.05	.05	-1.1336
.10	.06	-.9012
.15	.06	-.9227
.20	.07	-.8707
.25	.07	-.8953
.30	.07	-.9095
.35	.07	-.8663
.40	.07	-.9128
.45	.07	-.9215
.50	.07	-.8632
.55	.06	-.6874
.60	.06	-.5777
.65	.05	-.4937
.70	.05	-.4072
.75	.04	-.3398
.80	.03	-.2623
.85	.03	-.1932
.90	.02	-.1225
0.00	.03	.0002
.05	.01	.2752
.10	.01	.1861
.15	.00	.1371
.20	-.00	.0984
.25	-.00	.0718
.30	-.01	.0489
.35	-.01	.0339
.40	-.01	.0392
.45	-.01	-.0023
.50	-.01	-.0121
.55	-.01	-.0081
.60	-.01	.0179
.65	-.01	.0171
.70	-.00	.0286
.75	-.00	.0782
.80	-.00	.0775
.85	.00	.0946
.90	.00	.1400

X/C	Z/C	CP
0.00	.01	.0009
.05	.03	-1.5837
.10	.04	-1.5268
.15	.05	-1.5161
.20	.06	-1.4848
.25	.06	-1.4422
.30	.07	-1.4503
.35	.07	-1.3591
.40	.07	-1.3295
.45	.07	-1.0658
.50	.07	-.6516
.55	.06	-.4876
.60	.06	-.4392
.65	.05	-.3918
.70	.05	-.3410
.75	.04	-.2781
.80	.04	-.2181
.85	.03	-.1602
0.00	.01	-.0289
.04	-.00	.0075
.09	-.01	.2806
.14	-.01	.2260
.19	-.01	.1993
.24	-.01	.1620
.29	-.01	.1293
.34	-.01	.1091
.39	-.01	.0952
.44	-.01	.0865
.49	-.01	.0876
.54	-.01	.1016
.59	-.01	.1100
.64	-.00	.1146
.69	-.00	.1231
.74	.00	.1355
.79	.00	.1436
.84	.00	.1492

X/C	Z/C	CP
0.00	-.01	.1653
.11	.03	.0320
.20	.05	.0001
.31	.06	-.0043
.40	.07	.0153
.51	.06	-.0107
.61	.06	.0002
.71	.05	.0030
0.00	-.01	.0009
.11	-.02	.0032
.21	-.02	.0015
.31	-.02	-.0055
.40	-.02	.0033
.51	-.01	.0083
.61	-.01	.0060
.71	-.00	.0025

X/C	Z/C	CP
.11	.01	.0009
.21	.00	.0070
.31	.00	.0037
.41	.01	.0022
.51	.01	.0025
.62	.01	.0106
.71	.00	.0194
.11	-.05	.0003
.22	-.04	.0064
.32	-.03	.0031
.42	-.03	.0016
.51	-.02	.0021
.62	-.01	.0101
.72	-.00	-.0010

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 11

TP 17013

MACH .755

Q 28011.7

ALPW

-.01

BETA

0.00

P1 70240.62

PT1 102471.96

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5151	0.00	.01	.0093	0.00	-.01	.1089	.11	.01	.0098
.05	.05	-.1219	.05	.03	-.1025	.11	.03	.0282	.21	.00	.0109
.10	.06	-.2434	.10	.04	-.2815	.20	.05	.0179	.31	.00	.0113
.15	.06	-.2982	.15	.05	-.3616	.31	.06	.0038	.41	.01	.0115
.20	.07	-.3572	.20	.06	-.4123	.40	.07	.0150	.51	.01	.0086
.25	.07	-.3955	.25	.06	-.4571	.51	.06	.0115	.62	.01	.0111
.30	.07	-.4307	.30	.07	-.5058	.61	.06	.0093	.71	.00	.6191
.35	.07	-.4631	.35	.07	-.5331	.71	.05	.0098	.11	-.05	.0096
.40	.07	-.4801	.40	.07	-.5648	0.00	-.01	.0118	.22	-.04	.0106
.45	.07	-.4954	.45	.07	-.5501	.11	-.02	.0119	.32	-.03	.0112
.50	.07	-.4692	.50	.07	-.5152	.21	-.02	.0116	.42	-.03	.0114
.55	.06	-.4408	.55	.06	-.4876	.31	-.02	.0068	.51	-.02	.0083
.60	.06	-.4057	.60	.06	-.4440	.40	-.02	.0128	.62	-.01	.0107
.65	.05	-.3656	.65	.05	-.4443	.51	-.01	.0078	.72	-.00	.0119
.70	.05	-.3146	.70	.05	-.3427	.61	-.01	.0132			
.75	.04	-.2737	.75	.04	-.2866	.71	-.00	.0094			
.80	.03	-.2334	.80	.04	-.2386						
.85	.03	-.1731	.85	.03	-.1761						
.90	.02	-.1149	0.00	.01	.6005						
0.00	.03	.6014	.04	-.00	.0234						
.05	.01	-.2838	.09	-.01	-.2304						
.10	.01	-.2295	.14	-.01	-.1807						
.15	.00	-.2067	.19	-.01	-.1673						
.20	-.00	-.2071	.24	-.01	-.1558						
.25	-.00	-.2101	.29	-.01	-.1375						
.30	-.01	-.2010	.34	-.01	-.1339						
.35	-.01	-.2033	.39	-.01	-.1284						
.40	-.01	-.2030	.44	-.01	-.1065						
.45	-.01	-.2036	.49	-.01	-.0974						
.50	-.01	-.2081	.54	-.01	-.0553						
.55	-.01	-.1896	.59	-.01	-.0189						
.60	-.01	-.1598	.64	-.00	-.0235						
.65	-.01	-.1340	.69	-.00	-.0002						
.70	-.00	-.1055	.74	.00	.0227						
.75	-.00	.0053	.79	.00	.0567						
.80	-.00	.0062	.84	.00	.0799						
.85	.00	.0163									
.90	.00	.1091									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17016

MACH .703

Q

25488.9

ALPW

-2.04

BETA

0.00

P1 73697.35

PT1 102491.88

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.1314
.05	.05	.0876
.10	.06	-.0630
.15	.06	-.1480
.20	.07	-.2039
.25	.07	-.2508
.30	.07	-.2837
.35	.07	-.3143
.40	.07	-.3481
.45	.07	-.3587
.50	.07	-.3453
.55	.06	-.3343
.60	.06	-.3123
.65	.05	-.2861
.70	.05	-.2496
.75	.04	-.2176
.80	.03	-.1861
.85	.03	-.1480
.90	.02	-.0966
0.00	.03	.4208
.05	.01	-.4897
.10	.01	-.3834
.15	.00	-.3289
.20	-.00	-.3096
.25	-.00	-.2997
.30	-.01	-.2853
.35	-.01	-.2756
.40	-.01	-.2695
.45	-.01	-.2571
.50	-.01	-.2433
.55	-.01	-.2432
.60	-.01	-.2172
.65	-.01	-.1861
.70	-.00	-.1501
.75	-.00	-.0526
.80	-.00	-.0509
.85	.00	-.0253
.90	.00	.0624

X/C	Z/C	CP
0.00	.01	.0074
.05	.03	.1596
.10	.04	-.0368
.15	.05	-.1337
.20	.06	-.1999
.25	.06	-.2538
.30	.07	-.2988
.35	.07	-.3385
.40	.07	-.3749
.45	.07	-.3873
.50	.07	-.3731
.55	.06	-.3591
.60	.06	-.3380
.65	.05	-.3044
.70	.05	-.2724
.75	.04	-.2379
.80	.04	-.1992
.85	.03	-.1548
0.00	.01	.3365
.04	-.00	.0148
.09	-.01	-.5811
.14	-.01	-.4259
.19	-.01	-.3236
.24	-.01	-.2996
.29	-.01	-.2526
.34	-.01	-.2249
.39	-.01	-.2046
.44	-.01	-.1758
.49	-.01	-.1398
.54	-.01	-.1061
.59	-.01	-.0703
.64	-.00	-.0754
.69	-.00	-.0567
.74	.00	-.0196
.79	.00	.0081
.84	.00	.0434

X/C	Z/C	CP
0.00	-.01	.0657
.11	.03	.0589
.20	.05	.0035
.31	.06	.0054
.40	.07	.0153
.51	.06	.0066
.61	.06	.0061
.71	.05	.0087
0.00	-.01	.0069
.11	-.02	.0080
.21	-.02	.0075
.31	-.02	.0067
.40	-.02	.0089
.51	-.01	.0097
.61	-.01	.0061
.71	-.00	.0085

X/C	Z/C	CP
.11	.01	.0076
.21	.00	.0070
.31	.00	.0068
.41	.01	.0089
.51	.01	.0083
.62	.01	.0072
.71	.00	.2989
.11	-.05	.0075
.22	-.04	.0068
.32	-.03	.0067
.42	-.03	.0089
.51	-.02	.0082
.62	-.01	.0071
.72	-.00	.0082

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17017

MACH .703

Q 25513.7

ALPW

-1.51

BETA

0.00

P1 73667.43

PT1 102494.82

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.2650
.05	.05	.0314
.10	.06	-.1094
.15	.06	-.1833
.20	.07	-.2371
.25	.07	-.2872
.30	.07	-.3285
.35	.07	-.3491
.40	.07	-.3782
.45	.07	-.3862
.50	.07	-.3715
.55	.06	-.3523
.60	.06	-.3294
.65	.05	-.2983
.70	.05	-.2588
.75	.04	-.2319
.80	.03	-.1927
.85	.03	-.1528
.90	.02	-.0994
0.00	.03	.4920
.05	.01	-.4459
.10	.01	-.3279
.15	.00	-.2927
.20	-.00	-.2809
.25	-.00	-.2707
.30	-.01	-.2649
.35	-.01	-.2542
.40	-.01	-.2542
.45	-.01	-.2336
.50	-.01	-.2406
.55	-.01	-.2203
.60	-.01	-.1766
.65	-.01	-.1591
.70	-.00	-.1320
.75	-.00	-.0488
.80	-.00	-.0441
.85	.00	-.0129
.90	.00	.0768

X/C	Z/C	CP
0.00	.01	.0114
.05	.03	.1010
.10	.04	-.0863
.15	.05	-.1879
.20	.06	-.2450
.25	.06	-.2947
.30	.07	-.3493
.35	.07	-.3748
.40	.07	-.4167
.45	.07	-.4137
.50	.07	-.3956
.55	.06	-.3799
.60	.06	-.3583
.65	.05	-.3598
.70	.05	-.2850
.75	.04	-.2498
.80	.04	-.2093
.85	.03	-.1628
0.00	.01	.3893
.04	-.00	.0141
.09	-.01	-.4178
.14	-.01	-.3295
.19	-.01	-.2881
.24	-.01	-.2497
.29	-.01	-.2234
.34	-.01	-.1953
.39	-.01	-.1871
.44	-.01	-.1550
.49	-.01	-.1346
.54	-.01	-.0924
.59	-.01	-.0575
.64	-.00	-.0589
.69	-.00	-.0316
.74	.00	-.0039
.79	.00	.0300
.84	.00	.0475

X/C	Z/C	CP
0.00	-.01	.0821
.11	.03	.0432
.20	.05	.0078
.31	.06	.0019
.40	.07	.0047
.51	.06	-.0038
.61	.06	.0052
.71	.05	.0103
0.00	-.01	.0105
.11	-.02	.0080
.21	-.02	.0082
.31	-.02	.0002
.40	-.02	.0061
.51	-.01	.0117
.61	-.01	.0077
.71	-.00	.0100

X/C	Z/C	CP
.11	.01	.0115
.21	.00	.0098
.31	.00	.0061
.41	.01	.0074
.51	.01	.0097
.62	.01	.0096
.71	.00	.4057
.11	-.05	.0114
.22	-.04	.0097
.32	-.03	.0061
.42	-.03	.0074
.51	-.02	.0097
.62	-.01	.0095
.72	-.00	.0054

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17018

MACH .704

Q. 25532.9

ALPW

-94-

BETA

0.00

P1 73648.79

PT1 102501.30

Y/B/2 = .31

Y/B/2 = .74

$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.3772
.05	.05	-.0248
.10	.06	-.1643
.15	.06	-.2244
.20	.07	-.2703
.25	.07	-.3239
.30	.07	-.3621
.35	.07	-.3795
.40	.07	-.4024
.45	.07	-.4063
.50	.07	-.3917
.55	.06	-.3740
.60	.06	-.3412
.65	.05	-.3096
.70	.05	-.2758
.75	.04	-.2366
.80	.03	-.2018
.85	.03	-.1598
.90	.02	-.1061
0.00	.03	.5531
.05	.01	-.3872
.10	.01	-.2799
.15	.00	-.2448
.20	-.00	-.2388
.25	-.00	-.2367
.30	-.01	-.2361
.35	-.01	-.2298
.40	-.01	-.2326
.45	-.01	-.2157
.50	-.01	-.2115
.55	-.01	-.2051
.60	-.01	-.1824
.65	-.01	-.1522
.70	-.00	-.1259
.75	-.00	-.0384
.80	-.00	-.0370
.85	.00	-.0086
.90	.00	.0738

X/C	Z/C	CP
0.00	.01	.0100
.05	.03	.0197
.10	.04	-.1524
.15	.05	-.2393
.20	.06	-.3017
.25	.06	-.3450
.30	.07	-.3903
.35	.07	-.4221
.40	.07	-.4565
.45	.07	-.4548
.50	.07	-.4245
.55	.06	-.4023
.60	.06	-.3782
.65	.05	-.3430
.70	.05	-.3011
.75	.04	-.2592
.80	.04	-.2144
.85	.03	-.1676
0.00	.01	.4809
.04	-.00	.0247
.09	-.01	-.3313
.14	-.01	-.2626
.19	-.01	-.2311
.24	-.01	-.2123
.29	-.01	-.1877
.34	-.01	-.1679
.39	-.01	-.1643
.44	-.01	-.1383
.49	-.01	-.1190
.54	-.01	-.0769
.59	-.01	-.0426
.64	-.00	-.0361
.69	-.00	-.0235
.74	.00	.0008
.79	.00	.0339
.84	.00	.0693

X/C	Z/C	CP
0.00	-.01	.0938
.11	.03	.0367
.20	.05	.0097
.31	.06	.0062
.40	.07	.0150
.51	.06	.0074
.61	.06	.0153
.71	.05	.0090
0.00	-.01	.0087
.11	-.02	.0120
.21	-.02	.0127
.31	-.02	.0081
.40	-.02	.0108
.51	-.01	.0117
.61	-.01	.0080
.71	-.00	.0088

X/C	Z/C	CP
.11	.01	.0101
.21	.00	.0055
.31	.00	.0116
.41	.01	.0132
.51	.01	.0073
.62	.01	.0082
.71	.00	.5098
.11	-.05	.0099
.22	-.04	.0053
.32	-.03	.0114
.42	-.03	.0131
.51	-.02	.0073
.62	-.01	.0081
.72	-.00	.0110

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17019

MACH .703

Q 25515.8

ALPW

-.56

BETA

0.00

P1 73676.59

PT1 102506.20

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4602
.05	.05	-.0669
.10	.06	-.1967
.15	.06	-.2550
.20	.07	-.3026
.25	.07	-.3511
.30	.07	-.3833
.35	.07	-.4134
.40	.07	-.4203
.45	.07	-.4305
.50	.07	-.4046
.55	.06	-.3863
.60	.06	-.3579
.65	.05	-.3220
.70	.05	-.2782
.75	.04	-.2461
.80	.03	-.2068
.85	.03	-.1628
.90	.02	-.1103
0.00	.03	.5807
.05	.01	-.3376
.10	.01	-.2560
.15	.00	-.2211
.20	-.00	-.2202
.25	-.00	-.2183
.30	-.01	-.2152
.35	-.01	-.2115
.40	-.01	-.2086
.45	-.01	-.2081
.50	-.01	-.2071
.55	-.01	-.1990
.60	-.01	-.1787
.65	-.01	-.1485
.70	-.00	-.1126
.75	-.00	-.0525
.80	-.00	-.0317
.85	.00	-.0019
.90	.00	.0907

X/C	Z/C	CP
0.00	.01	.0101
.05	.03	-.0303
.10	.04	-.2055
.15	.05	-.2821
.20	.06	-.3320
.25	.06	-.3727
.30	.07	-.4254
.35	.07	-.4548
.40	.07	-.4797
.45	.07	-.4754
.50	.07	-.4477
.55	.06	-.4255
.60	.06	-.3970
.65	.05	-.3870
.70	.05	-.3184
.75	.04	-.2620
.80	.04	-.2247
.85	.03	-.1705
0.00	.01	.5277
.04	-.00	.0275
.09	-.01	-.2788
.14	-.01	-.2243
.19	-.01	-.1933
.24	-.01	-.1792
.29	-.01	-.1640
.34	-.01	-.1502
.39	-.01	-.1446
.44	-.01	-.1246
.49	-.01	-.1010
.54	-.01	-.0679
.59	-.01	-.0340
.64	-.00	-.0333
.69	-.00	-.0127
.74	.00	.0145
.79	.00	.0477
.84	.00	.0722

X/C	Z/C	CP
0.00	-.01	.0919
.11	.03	.0135
.20	.05	.0081
.31	.06	.0142
.40	.07	.0091
.51	.06	.0074
.61	.06	.0089
.71	.05	.0060
0.00	-.01	.0100
.11	-.02	.0073
.21	-.02	.0117
.31	-.02	.0139
.40	-.02	.0084
.51	-.01	.0109
.61	-.01	.0085
.71	-.00	.0058

X/C	Z/C	CP
.11	.01	.0102
.21	.00	.0098
.31	.00	.0083
.41	.01	.0093
.51	.01	.0106
.62	.01	.0136
.71	.00	.5663
.11	-.05	.0102
.22	-.04	.0095
.32	-.03	.0080
.42	-.03	.0090
.51	-.02	.0104
.62	-.01	.0134
.72	-.00	.0102

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17020

MACH .703

Q

25506.3

ALPW

-.02

BETA

0.00

P1

73688.34

PT1 102505.33

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5238
.05	.05	-.1275
.10	.06	-.2457
.15	.06	-.3054
.20	.07	-.3458
.25	.07	-.3852
.30	.07	-.4169
.35	.07	-.4383
.40	.07	-.4511
.45	.07	-.4436
.50	.07	-.4355
.55	.06	-.4092
.60	.06	-.3713
.65	.05	-.3422
.70	.05	-.2926
.75	.04	-.2531
.80	.03	-.2157
.85	.03	-.1649
.90	.02	-.1107
0.00	.03	.6014
.05	.01	-.2646
.10	.01	-.2186
.15	.00	-.1996
.20	-.00	-.1963
.25	-.00	-.1986
.30	-.01	-.1982
.35	-.01	-.1956
.40	-.01	-.1956
.45	-.01	-.1785
.50	-.01	-.1842
.55	-.01	-.1691
.60	-.01	-.1546
.65	-.01	-.1238
.70	-.00	-.0963
.75	-.00	-.0152
.80	-.00	-.0128
.85	.00	.0118
.90	.00	.0958

X/C	Z/C	CP
0.00	.01	.0075
.05	.03	-.1121
.10	.04	-.2702
.15	.05	-.3425
.20	.06	-.3858
.25	.06	-.4394
.30	.07	-.4733
.35	.07	-.4934
.40	.07	-.5158
.45	.07	-.5079
.50	.07	-.4821
.55	.06	-.4477
.60	.06	-.4146
.65	.05	-.4187
.70	.05	-.3274
.75	.04	-.2792
.80	.04	-.2247
.85	.03	-.1821
0.00	.01	.5605
.04	-.00	.0150
.09	-.01	-.1936
.14	-.01	-.1722
.19	-.01	-.1514
.24	-.01	-.1488
.29	-.01	-.1340
.34	-.01	-.1237
.39	-.01	-.1195
.44	-.01	-.1039
.49	-.01	-.0810
.54	-.01	-.0510
.59	-.01	-.0204
.64	-.00	-.0218
.69	-.00	.0010
.74	.00	.0212
.79	.00	.0511
.84	.00	.0779

X/C	Z/C	CP
0.00	-.01	.1084
.11	.03	.0216
.20	.05	.0110
.31	.06	.0102
.40	.07	.0149
.51	.06	-.0007
.61	.06	.0099
.71	.05	.0094
0.00	-.01	.0075
.11	-.02	.0110
.21	-.02	.0082
.31	-.02	.0089
.40	-.02	.0094
.51	-.01	.0098
.61	-.01	.0120
.71	-.00	.0089

X/C	Z/C	CP
.11	.01	.0077
.21	.00	.0107
.31	.00	.0099
.41	.01	.0090
.51	.01	.0134
.62	.01	.0072
.71	.00	.6215
.11	-.05	.0074
.22	-.04	.0104
.32	-.03	.0096
.42	-.03	.0086
.51	-.02	.0130
.62	-.01	.0068
.72	-.00	.0111

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17021

MACH .703

Q 25512.8 ALPW

.51 BETA

0.00 P1 73685.57

PT1 102510.92

Y/B/2 = .33

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5674	0.00	.01	.0084	0.00	-.01	.1098	.11	.01	.0086
.05	.05	-.1877	.05	.03	-.1958	.11	.03	.0187	.21	.00	.0097
.10	.06	-.3024	.10	.04	-.3376	.20	.05	.0135	.31	.00	.0120
.15	.06	-.3486	.15	.05	-.4033	.31	.05	.0124	.41	.01	.0106
.20	.07	-.3872	.20	.06	-.4571	.40	.07	.0116	.51	.01	.0071
.25	.07	-.4264	.25	.06	-.4871	.51	.06	.0055	.62	.01	.0095
.30	.07	-.4497	.30	.07	-.5217	.61	.06	.0080	.71	.00	.6377
.35	.07	-.4649	.35	.07	-.5389	.71	.05	.0113	.11	-.05	.0082
.40	.07	-.4849	.40	.07	-.5551	0.00	-.01	.0129	.22	-.04	.0093
.45	.07	-.4809	.45	.07	-.5425	.11	-.02	.0072	.32	-.03	.0117
.50	.07	-.4538	.50	.07	-.5058	.21	-.02	.0065	.42	-.03	.0103
.55	.06	-.4200	.55	.06	-.4774	.31	-.02	.0101	.51	-.02	.0068
.60	.06	-.3911	.60	.06	-.4384	.40	-.02	.0092	.62	-.01	.0092
.65	.05	-.3551	.65	.05	-.3885	.51	-.01	.0088	.72	-.00	.0083
.70	.05	-.3051	.70	.05	-.3391	.61	-.01	.0069			
.75	.04	-.2630	.75	.04	-.2922	.71	-.00	.0110			
.80	.03	-.2249	.80	.04	-.2415						
.85	.03	-.1738	.85	.03	-.1856						
.90	.02	-.1103	0.00	.01	.5891						
0.00	.03	.6079	.04	-.00	.0262						
.05	.01	-.2021	.09	-.01	-.1431						
.10	.01	-.1722	.14	-.01	-.1170						
.15	.00	-.1631	.19	-.01	-.1129						
.20	-.00	-.1688	.24	-.01	-.1105						
.25	-.00	-.1727	.29	-.01	-.1004						
.30	-.01	-.1797	.34	-.01	-.1003						
.35	-.01	-.1760	.39	-.01	-.0958						
.40	-.01	-.1769	.44	-.01	-.0821						
.45	-.01	-.1708	.49	-.01	-.0731						
.50	-.01	-.1724	.54	-.01	-.0354						
.55	-.01	-.1582	.59	-.01	-.0016						
.60	-.01	-.1365	.64	-.00	-.0106						
.65	-.01	-.1098	.69	-.00	.0091						
.70	-.00	-.0840	.74	.00	.0340						
.75	-.00	-.0204	.79	.00	.0573						
.80	-.00	-.0101	.84	.00	.0839						
.85	.00	.0176									
.90	.00	.0916									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17022

MACH .704

Q 25557.9

ALPW

1.02

BETA

0.00

P1 73627.14

PT1 102512.34

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5967
.05	.05	-.2597
.10	.06	-.3506
.15	.06	-.3929
.20	.07	-.4214
.25	.07	-.4601
.30	.07	-.4851
.35	.07	-.4982
.40	.07	-.5114
.45	.07	-.5036
.50	.07	-.4734
.55	.06	-.4496
.60	.06	-.4099
.65	.05	-.3655
.70	.05	-.3174
.75	.04	-.2711
.80	.03	-.2284
.85	.03	-.1769
.90	.02	-.1192
0.00	.03	.6050
.05	.01	-.1409
.10	.01	-.1359
.15	.00	-.1345
.20	-.00	-.1419
.25	-.00	-.1482
.30	-.01	-.1402
.35	-.01	-.1450
.40	-.01	-.1467
.45	-.01	-.1509
.50	-.01	-.1442
.55	-.01	-.1241
.60	-.01	-.1121
.65	-.01	-.0937
.70	-.00	-.0692
.75	-.00	.0176
.80	-.00	.0125
.85	.00	.0360
.90	.00	.1118

X/C	Z/C	CP
0.00	.01	.0128
.05	.03	-.2980
.10	.04	-.4181
.15	.05	-.4760
.20	.06	-.5098
.25	.06	-.5386
.30	.07	-.5699
.35	.07	-.5832
.40	.07	-.5950
.45	.07	-.5770
.50	.07	-.5392
.55	.06	-.5006
.60	.06	-.4562
.65	.05	-.4536
.70	.05	-.3544
.75	.04	-.3029
.80	.04	-.2464
.85	.03	-.1900
0.00	.01	.6397
.04	-.00	.0266
.09	-.01	-.1112
.14	-.01	-.0892
.19	-.01	-.0869
.24	-.01	-.0821
.29	-.01	-.0794
.34	-.01	-.0783
.39	-.01	-.0763
.44	-.01	-.0652
.49	-.01	-.0447
.54	-.01	-.0169
.59	-.01	.0117
.64	-.00	.0128
.69	-.00	.0253
.74	.00	.0509
.79	.00	.0764
.84	.00	.1006

X/C	Z/C	CP
0.00	-.01	.1343
.11	.03	.0157
.20	.05	-.0008
.31	.06	.0099
.40	.07	.0035
.51	.06	.0147
.61	.06	.0101
.71	.05	.0078
0.00	-.01	.0076
.11	-.02	.0089
.21	-.02	.0124
.31	-.02	.0104
.40	-.02	.0101
.51	-.01	.0111
.61	-.01	.0098
.71	-.00	.0075

X/C	Z/C	CP
.11	.01	.0130
.21	.00	.0101
.31	.00	.0083
.41	.01	.0104
.51	.01	.0082
.62	.01	.0090
.71	.00	.6450
.11	-.05	.0128
.22	-.04	.0095
.32	-.03	.0080
.42	-.03	.0103
.51	-.02	.0081
.62	-.01	.0088
.72	-.00	.0081

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17023

MACH .703

Q 25513.0

ALPW

1.58

BETA

0.00

P1 73685.80

PT1 102511.40

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6066
.05	.05	-.3354
.10	.06	-.4194
.15	.06	-.4465
.20	.07	-.4717
.25	.07	-.4908
.30	.07	-.5159
.35	.07	-.5311
.40	.07	-.5366
.45	.07	-.5226
.50	.07	-.5045
.55	.06	-.4640
.60	.06	-.4259
.65	.05	-.3828
.70	.05	-.3289
.75	.04	-.2835
.80	.03	-.2376
.85	.03	-.1858
.90	.02	-.1220
0.00	.03	.5828
.05	.01	-.0845
.10	.01	-.0857
.15	.00	-.0978
.20	-.00	-.1112
.25	-.00	-.1182
.30	-.01	-.1263
.35	-.01	-.1242
.40	-.01	-.1329
.45	-.01	-.1280
.50	-.01	-.1264
.55	-.01	-.1213
.60	-.01	-.0996
.65	-.01	-.0783
.70	-.00	-.0634
.75	-.00	.0078
.80	-.00	.0086
.85	.00	.0321
.90	.00	.1059

X/C	Z/C	CP
0.00	.01	.0104
.05	.03	-.3876
.10	.04	-.5020
.15	.05	-.5603
.20	.06	-.5708
.25	.06	-.5971
.30	.07	-.6153
.35	.07	-.6323
.40	.07	-.6478
.45	.07	-.6120
.50	.07	-.5668
.55	.06	-.5281
.60	.06	-.4696
.65	.05	-.4179
.70	.05	-.3670
.75	.04	-.3068
.80	.04	-.2487
.85	.03	-.1995
0.00	.01	.6014
.04	-.00	.0343
.09	-.01	-.0465
.14	-.01	-.0528
.19	-.01	-.0507
.24	-.01	-.0484
.29	-.01	-.0541
.34	-.01	-.0582
.39	-.01	-.0566
.44	-.01	-.0491
.49	-.01	-.0244
.54	-.01	-.0084
.59	-.01	.0134
.64	-.00	.0119
.69	-.00	.0435
.74	.00	.0581
.79	.00	.0959
.84	.00	.1160

X/C	Z/C	CP
0.00	-.01	.1300
.11	.03	.0192
.20	.05	.0094
.31	.06	-.0040
.40	.07	.0071
.51	.06	.0094
.61	.06	.0061
.71	.05	.0071
0.00	-.01	.0066
.11	-.02	.0077
.21	-.02	.0085
.31	-.02	-.0024
.40	-.02	.0078
.51	-.01	.0057
.61	-.01	.0059
.71	-.00	.0068

X/C	Z/C	CP
.11	.01	.0107
.21	.00	.0099
.31	.00	.0093
.41	.01	.0067
.51	.01	.0088
.62	.01	.0090
.71	.00	.6379
.11	-.05	.0105
.22	-.04	.0096
.32	-.03	.0093
.42	-.03	.0067
.51	-.02	.0085
.62	-.01	.0087
.72	-.00	.0142

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17024

MACH .704

Q 25528.0

ALPW

1.94

BETA

0.00

P1 73659.07

PT1 102504.88

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6092
.05	.05	-.3871
.10	.06	-.4565
.15	.06	-.4816
.20	.07	-.4975
.25	.07	-.5164
.30	.07	-.5460
.35	.07	-.5531
.40	.07	-.5642
.45	.07	-.5388
.50	.07	-.5138
.55	.06	-.4830
.60	.06	-.4378
.65	.05	-.3926
.70	.05	-.3336
.75	.04	-.2819
.80	.03	-.2418
.85	.03	-.1826
.90	.02	-.1256
0.00	.03	.5689
.05	.01	-.0445
.10	.01	-.0628
.15	.00	-.0712
.20	-.00	-.0889
.25	-.00	-.0976
.30	-.01	-.1114
.35	-.01	-.1198
.40	-.01	-.1229
.45	-.01	-.1210
.50	-.01	-.1217
.55	-.01	-.1184
.60	-.01	-.1000
.65	-.01	-.0765
.70	-.00	-.0555
.75	-.00	.0024
.80	-.00	.0015
.85	.00	.0242
.90	.00	.1008

X/C	Z/C	CP
0.00	.01	.0073
.05	.03	-.4783
.10	.04	-.5664
.15	.05	-.5892
.20	.06	-.6111
.25	.06	-.6379
.30	.07	-.6560
.35	.07	-.6583
.40	.07	-.6770
.45	.07	-.6378
.50	.07	-.5872
.55	.06	-.5366
.60	.06	-.4818
.65	.05	-.4313
.70	.05	-.3721
.75	.04	-.3172
.80	.04	-.2513
.85	.03	-.1974
0.00	.01	.5948
.04	-.00	.0142
.09	-.01	-.0036
.14	-.01	-.0173
.19	-.01	-.0197
.24	-.01	-.0299
.29	-.01	-.0363
.34	-.01	-.0386
.39	-.01	-.0464
.44	-.01	-.0348
.49	-.01	-.0155
.54	-.01	.0044
.59	-.01	.0296
.64	-.00	.0328
.69	-.00	.0484
.74	.00	.0679
.79	.00	.0947
.84	.00	.1138

X/C	Z/C	CP
0.00	-.01	.1335
.11	.03	.0200
.20	.05	.0078
.31	.06	.0120
.40	.07	.0102
.51	.06	-.0036
.61	.06	.0108
.71	.05	.0043
0.00	-.01	.0067
.11	-.02	.0062
.21	-.02	.0082
.31	-.02	.0091
.40	-.02	.0128
.51	-.01	.0078
.61	-.01	.0107
.71	-.00	.0038

X/C	Z/C	CP
.11	.01	.0075
.21	.00	.0084
.31	.00	.0115
.41	.01	.0094
.51	.01	.0088
.62	.01	.0109
.71	.00	.6186
.11	-.05	.0071
.22	-.04	.0079
.32	-.03	.0110
.42	-.03	.0090
.51	-.02	.0084
.62	-.01	.0107
.72	-.00	.0077

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17025

MACH .703

Q 25511.8

ALPW

2.48

BETA

0.00

P1 73686.00

PT1 102510.04

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5962	0.00	.01	.0067	0.00	-.01	.1411	.11	.01	.0068
.05	.05	-.4711	.05	.03	-.5633	.11	.03	.0196	.21	.00	.0126
.10	.06	-.5062	.10	.04	-.6672	.20	.05	.0103	.31	.00	.0058
.15	.06	-.5319	.15	.05	-.6658	.31	.06	.0029	.41	.01	.0105
.20	.07	-.5414	.20	.06	-.6731	.40	.07	.0039	.51	.01	.0091
.25	.07	-.5580	.25	.06	-.6963	.51	.06	.0088	.62	.01	.0080
.30	.07	-.5748	.30	.07	-.7016	.61	.06	.0084	.71	.00	.5664
.35	.07	-.5835	.35	.07	-.7130	.71	.05	.0092	.11	-.05	.0066
.40	.07	-.5900	.40	.07	-.7176	0.00	-.01	.0050	.22	-.04	.0124
.45	.07	-.5738	.45	.07	-.6666	.11	-.02	.0108	.32	-.03	.0057
.50	.07	-.5413	.50	.07	-.6179	.21	-.02	.0089	.42	-.03	.0103
.55	.06	-.5030	.55	.06	-.5564	.31	-.02	.0037	.51	-.02	.0087
.60	.06	-.4517	.60	.06	-.5019	.40	-.02	.0079	.62	-.01	.0077
.65	.05	-.4043	.65	.05	-.4447	.51	-.01	.0102	.72	-.00	.0126
.70	.05	-.3447	.70	.05	-.3820	.61	-.01	.0080			
.75	.04	-.2979	.75	.04	-.3226	.71	-.00	.0086			
.80	.03	-.2461	.80	.04	-.2607						
.85	.03	-.1894	.85	.03	-.2022						
.90	.02	-.1230	0.00	.01	.5660						
0.00	.03	.5167	.04	-.00	.0194						
.05	.01	.0063	.09	-.01	.0184						
.10	.01	-.0173	.14	-.01	.0241						
.15	.00	-.0438	.19	-.01	.0284						
.20	-.00	-.0612	.24	-.01	.0021						
.25	-.00	-.0736	.29	-.01	-.0040						
.30	-.01	-.0879	.34	-.01	-.0166						
.35	-.01	-.0987	.39	-.01	-.0210						
.40	-.01	-.1078	.44	-.01	-.0093						
.45	-.01	-.1007	.49	-.01	-.0010						
.50	-.01	-.1067	.54	-.01	.0188						
.55	-.01	-.0913	.59	-.01	.0399						
.60	-.01	-.0798	.64	-.00	.0374						
.65	-.01	-.0601	.69	-.00	.0534						
.70	-.00	-.0445	.74	.00	.0728						
.75	-.00	.0135	.79	.00	.0924						
.80	-.00	.0207	.84	.00	.1146						
.85	.00	.0425									
.90	.00	.1132									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17026

MACH .704

Q 25542.4 ALPW

3.01

BETA

0.00

P1 73647.72

PT1 102512.39

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5702
.05	.05	-.5463
.10	.06	-.5754
.15	.06	-.5839
.20	.07	-.5844
.25	.07	-.6033
.30	.07	-.6079
.35	.07	-.6146
.40	.07	-.6251
.45	.07	-.6076
.50	.07	-.5640
.55	.06	-.5192
.60	.06	-.4631
.65	.05	-.4148
.70	.05	-.3618
.75	.04	-.3031
.80	.03	-.2535
.85	.03	-.1887
.90	.02	-.1246
0.00	.03	.4331
.05	.01	.0552
.10	.01	.0182
.15	.00	-.0105
.20	-.00	-.0308
.25	-.00	-.0572
.30	-.01	-.0646
.35	-.01	-.0636
.40	-.01	-.0752
.45	-.01	-.0870
.50	-.01	-.0953
.55	-.01	-.0848
.60	-.01	-.0656
.65	-.01	-.0475
.70	-.00	-.0275
.75	-.00	.0080
.80	-.00	.0198
.85	.00	.0484
.90	.00	.1077

X/C	Z/C	CP
0.00	.01	.0067
.05	.03	-.6984
.10	.04	-.7650
.15	.05	-.7536
.20	.06	-.7376
.25	.06	-.7522
.30	.07	-.7595
.35	.07	-.7552
.40	.07	-.7584
.45	.07	-.6996
.50	.07	-.6507
.55	.06	-.5762
.60	.06	-.5278
.65	.05	-.4612
.70	.05	-.3938
.75	.04	-.3315
.80	.04	-.2677
.85	.03	-.2040
0.00	.01	.4884
.04	-.00	.0240
.09	-.01	.0875
.14	-.01	.0695
.19	-.01	.0619
.24	-.01	.0313
.29	-.01	.0188
.34	-.01	.0088
.39	-.01	-.0018
.44	-.01	.0084
.49	-.01	.0112
.54	-.01	.0336
.59	-.01	.0493
.64	-.00	.0522
.69	-.00	.0704
.74	.00	.0856
.79	.00	.1088
.84	.00	.1208

X/C	Z/C	CP
0.00	-.01	.1392
.11	.03	.0281
.20	.05	.0058
.31	.06	.0029
.40	.07	.0082
.51	.06	.0003
.61	.06	.0069
.71	.05	.0078
0.00	-.01	.0075
.11	-.02	.0096
.21	-.02	.0090
.31	-.02	.0054
.40	-.02	.0087
.51	-.01	.0072
.61	-.01	.0109
.71	-.00	.0074

X/C	Z/C	CP
.11	.01	.0066
.21	.00	.0045
.31	.00	.0065
.41	.01	.0081
.51	.01	.0133
.62	.01	.0079
.71	.00	.4832
.11	-.05	.0064
.22	-.04	.0045
.32	-.03	.0063
.42	-.03	.0078
.51	-.02	.0130
.62	-.01	.0077
.72	-.00	.0062

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17027

MACH .704

Q 25538.1

ALPW

4.03

BETA

0.00

P1 73660.73

PT1 102519.30

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.4884	0.00	.01	.0097	0.00	-.01	.1493	.11	.01	.0099
.05	.05	-.7026	.05	.03	-.9321	.11	.03	.0136	.21	.00	.0074
.10	.06	-.7169	.10	.04	-.9524	.20	.05	.0117	.31	.00	.0054
.15	.06	-.6798	.15	.05	-.9022	.31	.06	.0135	.41	.01	.0085
.20	.07	-.6636	.20	.06	-.8622	.40	.07	.0043	.51	.01	.0066
.25	.07	-.6743	.25	.06	-.8547	.51	.06	.0094	.62	.01	.0042
.30	.07	-.6845	.30	.07	-.8514	.61	.06	.0042	.71	.00	.2698
.35	.07	-.6774	.35	.07	-.8215	.71	.05	.0076	.11	-.05	.0096
.40	.07	-.6815	.40	.07	-.8082	0.00	-.01	.0042	.22	-.04	.0071
.45	.07	-.6538	.45	.07	-.7661	.11	-.02	.0065	.32	-.03	.0051
.50	.07	-.6018	.50	.07	-.6809	.21	-.02	.0044	.42	-.03	.0081
.55	.06	-.5539	.55	.06	-.6087	.31	-.02	.0087	.51	-.02	.0062
.60	.06	-.4975	.60	.06	-.5432	.40	-.02	.0073	.62	-.01	.0039
.65	.05	-.4427	.65	.05	-.4683	.51	-.01	.0071	.72	-.00	.0078
.70	.05	-.3755	.70	.05	-.3996	.61	-.01	.0038			
.75	.04	-.3182	.75	.04	-.3298	.71	-.00	.0072			
.80	.03	-.2620	.80	.04	-.2546						
.85	.03	-.2011	.85	.03	-.1952						
.90	.02	-.1265	0.00	.01	.2622						
0.00	.03	.2718	.04	-.00	.0246						
.05	.01	.1518	.09	-.01	.1728						
.10	.01	.0769	.14	-.01	.1310						
.15	.00	.0456	.19	-.01	.1197						
.20	-.00	.0169	.24	-.01	.0782						
.25	-.00	-.0084	.29	-.01	.0652						
.30	-.01	-.0267	.34	-.01	.0507						
.35	-.01	-.0368	.39	-.01	.0445						
.40	-.01	-.0359	.44	-.01	.0351						
.45	-.01	-.0485	.49	-.01	.0457						
.50	-.01	-.0331	.54	-.01	.0604						
.55	-.01	-.0413	.59	-.01	.0723						
.60	-.01	-.0335	.64	-.00	.0757						
.65	-.01	-.0204	.69	-.00	.0891						
.70	-.00	-.0011	.74	.00	.1035						
.75	-.00	.0596	.79	.00	.1214						
.80	-.00	.0589	.84	.00	.1392						
.85	.00	.0749									
.90	.00	.1320									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17028

MACH .703

Q 25520.9

ALPW

6.05

BETA

0.00

P1 73687.70

P11 102523.24

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.2251
.05	.05	-.9214
.10	.06	-.9610
.15	.06	-.8737
.20	.07	-.8455
.25	.07	-.8245
.30	.07	-.8118
.35	.07	-.8086
.40	.07	-.7900
.45	.07	-.7447
.50	.07	-.6723
.55	.06	-.6009
.60	.06	-.5336
.65	.05	-.4667
.70	.05	-.3900
.75	.04	-.3233
.80	.03	-.2647
.85	.03	-.1973
.90	.02	-.1233
0.00	.03	-.1416
.05	.01	.2843
.10	.01	.2013
.15	.00	.1429
.20	-.00	.1073
.25	-.00	.0731
.30	-.01	.0545
.35	-.01	.0605
.40	-.01	.0559
.45	-.01	.0032
.50	-.01	.0077
.55	-.01	.0043
.60	-.01	.0151
.65	-.01	.0285
.70	-.00	.0376
.75	-.00	.0787
.80	-.00	.0819
.85	.00	.0863
.90	.00	.1332

X/C	Z/C	CP
0.00	.01	.0026
.05	.03	-1.8416
.10	.04	-1.6897
.15	.05	-1.4799
.20	.06	-.8747
.25	.06	-.8539
.30	.07	-.9059
.35	.07	-.8763
.40	.07	-.8531
.45	.07	-.7764
.50	.07	-.6835
.55	.06	-.6001
.60	.06	-.5158
.65	.05	-.4345
.70	.05	-.3572
.75	.04	-.2828
.80	.04	-.2139
.85	.03	-.1536
0.00	.01	-.2009
.04	-.00	-.0168
.09	-.01	.2739
.14	-.01	.2343
.19	-.01	.1997
.24	-.01	.1554
.29	-.01	.1307
.34	-.01	.1108
.39	-.01	.0895
.44	-.01	.0833
.49	-.01	.0818
.54	-.01	.0871
.59	-.01	.0970
.64	-.00	.0989
.69	-.00	.1068
.74	.00	.1154
.79	.00	.1239
.84	.00	.1339

X/C	Z/C	CP
0.00	-.01	.1410
.11	.03	.0279
.20	.05	.0154
.31	.06	.0077
.40	.07	.0025
.51	.06	.0092
.61	.06	-.0017
.71	.05	.0041
0.00	-.01	.0029
.11	-.02	.0011
.21	-.02	.0018
.31	-.02	.0033
.40	-.02	.0055
.51	-.01	.0033
.61	-.01	.0023
.71	-.00	.0036

X/C	Z/C	CP
.11	.01	.0026
.21	.00	.0047
.31	.00	.0012
.41	.01	.0042
.51	.01	.0045
.62	.01	.0004
.71	.00	-.1298
.11	-.05	.0023
.22	-.04	.0043
.32	-.03	.0009
.42	-.03	.0040
.51	-.02	.0042
.62	-.01	.0001
.72	-.00	.0022

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 12

TP 17029

MACH .703

Q 25507.7

ALPW

-.05

BETA

0.00

P1 73700.15

PT1 102518.40

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5137
.05	.05	-.1225
.10	.06	-.2459
.15	.06	-.3054
.20	.07	-.3403
.25	.07	-.3794
.30	.07	-.4186
.35	.07	-.4403
.40	.07	-.4499
.45	.07	-.4505
.50	.07	-.4261
.55	.06	-.4091
.60	.06	-.3716
.65	.05	-.3405
.70	.05	-.2908
.75	.04	-.2532
.80	.03	-.2115
.85	.03	-.1655
.90	.02	-.1109
0.00	.03	.5971
.05	.01	-.2696
.10	.01	-.2256
.15	.00	-.2053
.20	-.00	-.1937
.25	-.00	-.1972
.30	-.01	-.2004
.35	-.01	-.1964
.40	-.01	-.1969
.45	-.01	-.1849
.50	-.01	-.1828
.55	-.01	-.1726
.60	-.01	-.1519
.65	-.01	-.1270
.70	-.00	-.1022
.75	-.00	-.0254
.80	-.00	-.0146
.85	.00	.0128
.90	.00	.0789

X/C	Z/C	CP
0.00	.01	.0094
.05	.03	-.1102
.10	.04	-.2621
.15	.05	-.3424
.20	.06	-.3880
.25	.06	-.4329
.30	.07	-.4717
.35	.07	-.4970
.40	.07	-.5088
.45	.07	-.5070
.50	.07	-.4863
.55	.06	-.4461
.60	.06	-.4123
.65	.05	-.4068
.70	.05	-.3305
.75	.04	-.2778
.80	.04	-.2298
.85	.03	-.1767
0.00	.01	.5794
.04	-.00	.0456
.09	-.01	-.2190
.14	-.01	-.1804
.19	-.01	-.1730
.24	-.01	-.1491
.29	-.01	-.1341
.34	-.01	-.1292
.39	-.01	-.1201
.44	-.01	-.1074
.49	-.01	-.0853
.54	-.01	-.0445
.59	-.01	-.0252
.64	-.00	-.0192
.69	-.00	.0016
.74	.00	.0190
.79	.00	.0523
.84	.00	.0785

X/C	Z/C	CP
0.00	-.01	.1053
.11	.03	.0322
.20	.05	.0077
.31	.06	.0091
.40	.07	.0138
.51	.06	.0029
.61	.06	.0112
.71	.05	.0081
0.00	-.01	.0074
.11	-.02	.0100
.21	-.02	.0084
.31	-.02	.0056
.40	-.02	.0098
.51	-.01	.0131
.61	-.01	.0107
.71	-.00	.0078

X/C	Z/C	CP
.11	.01	.0100
.21	.00	.0082
.31	.00	.0110
.41	.01	.0073
.51	.01	.0094
.62	.01	.0098
.71	.00	.6129
.11	-.05	.0097
.22	-.04	.0080
.32	-.03	.0107
.42	-.03	.0072
.51	-.02	.0093
.62	-.01	.0096
.72	-.00	.0076

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17030

MACH .603

Q

20387.5

ALPW

-2.06

BETA

0.00

P1 80220.14

PT1 102525.86

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.0897
.05	.05	.0730
.10	.06	-.0714
.15	.06	-.1409
.20	.07	-.1952
.25	.07	-.2416
.30	.07	-.2760
.35	.07	-.3023
.40	.07	-.3215
.45	.07	-.3250
.50	.07	-.3127
.55	.06	-.3039
.60	.06	-.2834
.65	.05	-.2619
.70	.05	-.2205
.75	.04	-.2037
.80	.03	-.1688
.85	.03	-.1359
.90	.02	-.0925
0.00	.03	.3926
.05	.01	-.4703
.10	.01	-.3532
.15	.00	-.3078
.20	-.00	-.2800
.25	-.00	-.2723
.30	-.01	-.2621
.35	-.01	-.2623
.40	-.01	-.2599
.45	-.01	-.2312
.50	-.01	-.2322
.55	-.01	-.2175
.60	-.01	-.1948
.65	-.01	-.1694
.70	-.00	-.1358
.75	-.00	-.0702
.80	-.00	-.0511
.85	.00	-.0226
.90	.00	.0460

X/C	Z/C	CP
0.00	.01	.0080
.05	.03	.1524
.10	.04	-.0246
.15	.05	-.1327
.20	.06	-.1857
.25	.06	-.2392
.30	.07	-.2834
.35	.07	-.3170
.40	.07	-.3473
.45	.07	-.3507
.50	.07	-.3409
.55	.06	-.3230
.60	.06	-.3076
.65	.05	-.2801
.70	.05	-.2538
.75	.04	-.2228
.80	.04	-.1860
.85	.03	-.1485
0.00	.01	.1994
.04	-.00	.0175
.09	-.01	-.4467
.14	-.01	-.3546
.19	-.01	-.2985
.24	-.01	-.2649
.29	-.01	-.2302
.34	-.01	-.2112
.39	-.01	-.1971
.44	-.01	-.1679
.49	-.01	-.1398
.54	-.01	-.0999
.59	-.01	-.0677
.64	-.00	-.0689
.69	-.00	-.0471
.74	.00	-.0193
.79	.00	.0071
.84	.00	.0399

X/C	Z/C	CP
0.00	-.01	.0711
.11	.03	.0436
.20	.05	.0064
.31	.06	.0019
.40	.07	.0034
.51	.06	.0044
.61	.06	.0050
.71	.05	.0034
0.00	-.01	.0024
.11	-.02	.0035
.21	-.02	.0023
.31	-.02	.0049
.40	-.02	-.0007
.51	-.01	.0079
.61	-.01	.0050
.71	-.00	.0034

X/C	Z/C	CP
.11	.01	.0079
.21	.00	.0015
.31	.00	.0054
.41	.01	.0022
.51	.01	.0063
.62	.01	.0052
.71	.00	.2382
.11	-.05	.0078
.22	-.04	.0012
.32	-.03	.0053
.42	-.03	.0020
.51	-.02	.0062
.62	-.01	.0050
.72	-.00	.0047

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17031

MACH .604

Q 20448.7

ALPW

-1.60

BETA

0.00

P1 80147.47

PT1 102527.89

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.2057	0.00	.01	.0062	0.00	-.01	.0768	.11	.01	.0063
.05	.05	.0236	.05	.03	.1063	.11	.03	.0570	.21	.00	.0052
.10	.06	-.1121	.10	.04	-.0759	.20	.05	.0028	.31	.00	.0068
.15	.06	-.1687	.15	.05	-.1705	.31	.06	.0021	.41	.01	.0056
.20	.07	-.2264	.20	.06	-.2294	.40	.07	.0122	.51	.01	.0025
.25	.07	-.2603	.25	.06	-.2739	.51	.06	.0152	.62	.01	.0071
.30	.07	-.3046	.30	.07	-.3161	.61	.06	.0041	.71	.00	.3545
.35	.07	-.3257	.35	.07	-.3440	.71	.05	.0035	.11	-.05	.0060
.40	.07	-.3386	.40	.07	-.3770	0.00	-.01	.0051	.22	-.04	.0050
.45	.07	-.3443	.45	.07	-.3778	.11	-.02	.0064	.32	-.03	.0063
.50	.07	-.3290	.50	.07	-.3609	.21	-.02	.0054	.42	-.03	.0053
.55	.06	-.3175	.55	.06	-.3438	.31	-.02	.0025	.51	-.02	.0021
.60	.06	-.2909	.60	.06	-.3182	.40	-.02	.0063	.62	-.01	.0067
.65	.05	-.2693	.65	.05	-.3179	.51	-.01	.0052	.72	-.00	.0057
.70	.05	-.2323	.70	.05	-.2648	.61	-.01	.0038			
.75	.04	-.2032	.75	.04	-.2645	.71	-.00	.0032			
.80	.03	-.1782	.80	.04	-.1955						
.85	.03	-.1413	.85	.03	-.1538						
.90	.02	-.0974	0.00	.01	.3331						
0.00	.03	.4592	.04	-.00	.0105						
.05	.01	-.4277	.09	-.01	-.3543						
.10	.01	-.3152	.14	-.01	-.3057						
.15	.00	-.2739	.19	-.01	-.2643						
.20	-.00	-.2563	.24	-.01	-.2329						
.25	-.00	-.2454	.29	-.01	-.2082						
.30	-.01	-.2418	.34	-.01	-.1904						
.35	-.01	-.2326	.39	-.01	-.1817						
.40	-.01	-.2350	.44	-.01	-.1551						
.45	-.01	-.2170	.49	-.01	-.1202						
.50	-.01	-.2166	.54	-.01	-.0888						
.55	-.01	-.2015	.59	-.01	-.0536						
.60	-.01	-.1805	.64	-.00	-.0539						
.65	-.01	-.1513	.69	-.00	-.0351						
.70	-.00	-.1207	.74	.00	-.0119						
.75	-.00	-.0425	.79	.00	.0245						
.80	-.00	-.0375	.84	.00	.0458						
.85	.00	-.0157									
.90	.00	.0531									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17032

MACH .603

Q

20409.2

ALPW

-.99

BETA

0.00

P1 80200.34

PT1 102532.36

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.3528
.05	.05	-.0281
.10	.06	-.1654
.15	.06	-.2193
.20	.07	-.2611
.25	.07	-.3034
.30	.07	-.3309
.35	.07	-.3538
.40	.07	-.3677
.45	.07	-.3683
.50	.07	-.3512
.55	.06	-.3334
.60	.06	-.3099
.65	.05	-.2835
.70	.05	-.2455
.75	.04	-.2194
.80	.03	-.1844
.85	.03	-.1475
.90	.02	-.0977
0.00	.03	.5397
.05	.01	-.3704
.10	.01	-.2634
.15	.00	-.2247
.20	-.00	-.2201
.25	-.00	-.2197
.30	-.01	-.2134
.35	-.01	-.2091
.40	-.01	-.2140
.45	-.01	-.1985
.50	-.01	-.2011
.55	-.01	-.1925
.60	-.01	-.1728
.65	-.01	-.1372
.70	-.00	-.1057
.75	-.00	-.0294
.80	-.00	-.0292
.85	.00	.0002
.90	.00	.0582

X/C	Z/C	CP
0.00	.01	.0057
.05	.03	.0243
.10	.04	-.1468
.15	.05	-.2260
.20	.06	-.2786
.25	.06	-.3231
.30	.07	-.3602
.35	.07	-.3854
.40	.07	-.4090
.45	.07	-.4084
.50	.07	-.3880
.55	.06	-.3660
.60	.06	-.3452
.65	.05	-.3078
.70	.05	-.2793
.75	.04	-.2433
.80	.04	-.2047
.85	.03	-.1616
0.00	.01	.4555
.04	-.00	.0025
.09	-.01	-.2865
.14	-.01	-.2419
.19	-.01	-.2223
.24	-.01	-.1961
.29	-.01	-.1730
.34	-.01	-.1619
.39	-.01	-.1546
.44	-.01	-.1320
.49	-.01	-.1037
.54	-.01	-.0714
.59	-.01	-.0453
.64	-.00	-.0459
.69	-.00	-.0248
.74	.00	-.0031
.79	.00	.0300
.84	.00	.0555

X/C	Z/C	CP
0.00	-.01	.0804
.11	.03	.0361
.20	.05	.0146
.31	.06	.0096
.40	.07	-.0011
.51	.06	.0080
.61	.06	.0051
.71	.05	.0073
0.00	-.01	.0058
.11	-.02	.0051
.21	-.02	.0060
.31	-.02	.0125
.40	-.02	.0040
.51	-.01	.0072
.61	-.01	.0045
.71	-.00	.0067

X/C	Z/C	CP
.11	.01	.0062
.21	.00	.0043
.31	.00	.0044
.41	.01	.0049
.51	.01	.0070
.62	.01	.0050
.71	.00	.4952
.11	-.05	.0058
.22	-.04	.0039
.32	-.03	.0041
.42	-.03	.0046
.51	-.02	.0067
.62	-.01	.0048
.72	-.00	.0065

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17033

MACH .603

Q 20408.7

ALPW

-.55

BETA

0.00

P1 80198.81

PT1 102530.31

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4440
.05	.05	-.0716
.10	.06	-.2078
.15	.06	-.2561
.20	.07	-.2976
.25	.07	-.3275
.30	.07	-.3604
.35	.07	-.3776
.40	.07	-.3921
.45	.07	-.3853
.50	.07	-.3725
.55	.06	-.3459
.60	.06	-.3222
.65	.05	-.2919
.70	.05	-.2564
.75	.04	-.2249
.80	.03	-.1898
.85	.03	-.1507
.90	.02	-.1024
0.00	.03	.5687
.05	.01	-.3218
.10	.01	-.2308
.15	.00	-.2057
.20	-.00	-.1969
.25	-.00	-.1940
.30	-.01	-.1948
.35	-.01	-.1909
.40	-.01	-.1901
.45	-.01	-.1800
.50	-.01	-.1788
.55	-.01	-.1722
.60	-.01	-.1569
.65	-.01	-.1307
.70	-.00	-.0978
.75	-.00	-.0515
.80	-.00	-.0342
.85	.00	-.0051
.90	.00	.0493

X/C	Z/C	CP
0.00	.01	.0055
.05	.03	-.0356
.10	.04	-.1964
.15	.05	-.2706
.20	.06	-.3248
.25	.06	-.3574
.30	.07	-.3978
.35	.07	-.4200
.40	.07	-.4307
.45	.07	-.4318
.50	.07	-.4130
.55	.06	-.3874
.60	.06	-.3571
.65	.05	-.3248
.70	.05	-.2923
.75	.04	-.2556
.80	.04	-.2101
.85	.03	-.1707
0.00	.01	.5068
.04	-.00	.0180
.09	-.01	-.2368
.14	-.01	-.2056
.19	-.01	-.1825
.24	-.01	-.1685
.29	-.01	-.1537
.34	-.01	-.1422
.39	-.01	-.1291
.44	-.01	-.1169
.49	-.01	-.0836
.54	-.01	-.0620
.59	-.01	-.0309
.64	-.00	-.0336
.69	-.00	-.0086
.74	.00	.0120
.79	.00	.0379
.84	.00	.0678

X/C	Z/C	CP
0.00	-.01	.0906
.11	.03	.0228
.20	.05	.0019
.31	.06	.0061
.40	.07	.0030
.51	.06	-.0046
.61	.06	.0053
.71	.05	.0054
0.00	-.01	.0067
.11	-.02	.0047
.21	-.02	.0073
.31	-.02	.0085
.40	-.02	.0049
.51	-.01	.0074
.61	-.01	.0050
.71	-.00	.0050

X/C	Z/C	CP
.11	.01	.0056
.21	.00	.0075
.31	.00	.0061
.41	.01	.0056
.51	.01	.0029
.62	.01	.0064
.71	.00	.5645
.11	-.05	.0053
.22	-.04	.0069
.32	-.03	.0055
.42	-.03	.0051
.51	-.02	.0025
.62	-.01	.0059
.72	-.00	.0053

7 X 10 HIGH SPEED TUNNEL

TP 17034

PT1 102526.01

$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.01	.0072
.05	.03	-.1278
.10	.04	-.2769
.15	.05	-.3402
.20	.06	-.3769
.25	.06	-.4100
.30	.07	-.4413
.35	.07	-.4609
.40	.07	-.4737
.45	.07	-.4606
.50	.07	-.4417
.55	.06	-.4128
.60	.06	-.3791
.65	.05	-.3845
.70	.05	-.3049
.75	.04	-.3123
.80	.04	-.2219
.85	.03	-.1754
0.00	.01	.5713
.04	-.00	.0109
.09	-.01	-.1463
.14	-.01	-.1476
.19	-.01	-.1277
.24	-.01	-.1274
.29	-.01	-.1123
.34	-.01	-.1090
.39	-.01	-.1093
.44	-.01	-.0891
.49	-.01	-.0659
.54	-.01	-.0439
.59	-.01	-.0153
.64	-.00	-.0195
.69	-.00	.0042
.74	.00	.0182
.79	.00	.0498
.84	.00	.0732

X/C	Z/C	CP
0.00	-.01	.0986
.11	.03	.0332
.20	.05	.0104
.31	.06	.0090
.40	.07	.0070
.51	.06	-.0029
.61	.06	.0075
.71	.05	.0064
0.00	-.01	.0042
.11	-.02	.0049
.21	-.02	.0089
.31	-.02	.0089
.40	-.02	.0051
.51	-.01	.0064
.61	-.01	.0073
.71	-.00	.0064

X/C	Z/C	CP
.11	.01	.0072
.21	.00	.0055
.31	.00	.0075
.41	.01	.0064
.51	.01	.0069
.62	.01	.0052
.71	.00	.6215
.11	-.05	.0072
.22	-.04	.0055
.32	-.03	.0075
.42	-.03	.0064
.51	-.02	.0067
.62	-.01	.0054
.72	-.00	.0091

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17035

MACH .603

Q 20389.0

ALPW

.49

BETA

0.00

P1 80223.79

PT1 102531.25

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5634	0.00	.01	.0043	0.00	-.01	.1109	.11	.01	.0046
.05	.05	-.1930	.05	.03	-.2011	.11	.03	.0215	.21	.00	.0062
.10	.06	-.2936	.10	.04	-.3272	.20	.05	.0052	.31	.00	.0048
.15	.06	-.3373	.15	.05	-.3750	.31	.06	.0006	.41	.01	.0083
.20	.07	-.3661	.20	.06	-.4151	.40	.07	.0082	.51	.01	.0087
.25	.07	-.3959	.25	.06	-.4421	.51	.06	.0017	.62	.01	.0080
.30	.07	-.4177	.30	.07	-.4783	.61	.06	.0061	.71	.00	.6285
.35	.07	-.4305	.35	.07	-.4868	.71	.05	.0055	.11	-.05	.0043
.40	.07	-.4318	.40	.07	-.4970	0.00	-.01	.0045	.22	-.04	.0059
.45	.07	-.4286	.45	.07	-.4864	.11	-.02	.0080	.32	-.03	.0045
.50	.07	-.4021	.50	.07	-.4607	.21	-.02	.0060	.42	-.03	.0081
.55	.06	-.3815	.55	.06	-.4309	.31	-.02	.0002	.51	-.02	.0084
.60	.06	-.3471	.60	.06	-.3986	.40	-.02	.0053	.62	-.01	.0077
.65	.05	-.3182	.65	.05	-.3542	.51	-.01	.0089	.72	-.00	.0033
.70	.05	-.2751	.70	.05	-.3169	.61	-.01	.0056			
.75	.04	-.2410	.75	.04	-.2712	.71	-.00	.0054			
.80	.03	-.2024	.80	.04	-.2284						
.85	.03	-.1593	.85	.03	-.1795						
.90	.02	-.1088	0.00	.01	.5914						
0.00	.03	.5998	.04	-.00	.0322						
.05	.01	-.1889	.09	-.01	-.1384						
.10	.01	-.1566	.14	-.01	-.1141						
.15	.00	-.1492	.19	-.01	-.1184						
.20	-.00	-.1516	.24	-.01	-.1013						
.25	-.00	-.1549	.29	-.01	-.0945						
.30	-.01	-.1598	.34	-.01	-.0925						
.35	-.01	-.1558	.39	-.01	-.0880						
.40	-.01	-.1563	.44	-.01	-.0767						
.45	-.01	-.1524	.49	-.01	-.0505						
.50	-.01	-.1501	.54	-.01	-.0325						
.55	-.01	-.1376	.59	-.01	-.0085						
.60	-.01	-.1210	.64	-.00	-.0052						
.65	-.01	-.1013	.69	-.00	.0135						
.70	-.00	-.0767	.74	.00	.0333						
.75	-.00	-.0204	.79	.00	.0589						
.80	-.00	-.0064	.84	.00	.0839						
.85	.00	.0160									
.90	.00	.0731									

TP 17036

PT1 102533.79

$$Y/B/2 = 1.011$$

X/C	Z/C	CP
.11	.01	.0089
.21	.00	.0074
.31	.00	.0059
.41	.01	.0069
.51	.01	.0062
.62	.01	.0063
.71	.00	.6354
.11	-.05	.0083
.22	-.04	.0068
.32	-.03	.0052
.42	-.03	.0063
.51	-.02	.0056
.62	-.01	.0058
.72	-.00	.0059

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17037

MACH .603

Q 20393.3

ALPW

1.47

BETA

0.00

P1 80227.11

PT1 102539.58

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5989	0.00	.01	.0051	0.00	-.01	.1211	.11	.01	.0052
.05	.05	-.3271	.05	.03	-.3645	.11	.03	.0310	.21	.00	.0044
.10	.06	-.3979	.10	.04	-.4578	.20	.05	.0122	.31	.00	.0054
.15	.06	-.4148	.15	.05	-.4912	.31	.06	.0034	.41	.01	.0068
.20	.07	-.4378	.20	.06	-.5101	.40	.07	.0094	.51	.01	.0070
.25	.07	-.4534	.25	.06	-.5302	.51	.06	.0064	.62	.01	.0054
.30	.07	-.4758	.30	.07	-.5482	.61	.06	.0066	.71	.00	.6262
.35	.07	-.4695	.35	.07	-.5566	.71	.05	.0073	.11	-.05	.0051
.40	.07	-.4818	.40	.07	-.5588	0.00	-.01	.0026	.22	-.04	.0042
.45	.07	-.4689	.45	.07	-.5423	.11	-.02	.0055	.32	-.03	.0050
.50	.07	-.4399	.50	.07	-.5061	.21	-.02	.0088	.42	-.03	.0066
.55	.06	-.4163	.55	.06	-.4721	.31	-.02	.0013	.51	-.02	.0068
.60	.06	-.3777	.60	.06	-.4263	.40	-.02	.0058	.62	-.01	.0052
.65	.05	-.3386	.65	.05	-.3800	.51	-.01	.0061	.72	-.00	.0055
.70	.05	-.2941	.70	.05	-.3328	.61	-.01	.0063			
.75	.04	-.2555	.75	.04	-.2912	.71	-.00	.0071			
.80	.03	-.2164	.80	.04	-.2417						
.85	.03	-.1684	.85	.03	-.1905						
.90	.02	-.1125	0.00	.01	.5738						
0.00	.03	.5747	.04	-.00	.0393						
.05	.01	-.0751	.09	-.01	-.0481						
.10	.01	-.0843	.14	-.01	-.0473						
.15	.00	-.0886	.19	-.01	-.0471						
.20	-.00	-.1015	.24	-.01	-.0477						
.25	-.00	-.1046	.29	-.01	-.0523						
.30	-.01	-.1053	.34	-.01	-.0554						
.35	-.01	-.1074	.39	-.01	-.0564						
.40	-.01	-.1201	.44	-.01	-.0509						
.45	-.01	-.1205	.49	-.01	-.0246						
.50	-.01	-.1239	.54	-.01	-.0090						
.55	-.01	-.1120	.59	-.01	.0142						
.60	-.01	-.0952	.64	-.00	.0174						
.65	-.01	-.0717	.69	-.00	.0356						
.70	-.00	-.0542	.74	.00	.0520						
.75	-.00	-.0108	.79	.00	.0763						
.80	-.00	.0074	.84	.00	.0948						
.85	.00	.0318									
.90	.00	.1014									

7 X 10 HIGH SPEED TUNNEL

TEST 107

PUN 13

TP 17038

MACH .602

Q 20366.9

ALPW

2.05

BETA

0.00

P1 80264.21

PT1 102544.32

Y/B/2 = .31

$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.5924
.05	.05	-.4091
.10	.06	-.4571
.15	.06	-.4721
.20	.07	-.4712
.25	.07	-.4999
.30	.07	-.5050
.35	.07	-.5060
.40	.07	-.5108
.45	.07	-.4974
.50	.07	-.4603
.55	.06	-.4245
.60	.06	-.3930
.65	.05	-.3568
.70	.05	-.3035
.75	.04	-.2626
.80	.03	-.2221
.85	.03	-.1759
.90	.02	-.1208
0.00	.03	.5236
.05	.01	-.0236
.10	.01	-.0387
.15	.00	-.0563
.20	-.00	-.0685
.25	-.00	-.0850
.30	-.01	-.0807
.35	-.01	-.0820
.40	-.01	-.0850
.45	-.01	-.1044
.50	-.01	-.1043
.55	-.01	-.0978
.60	-.01	-.0799
.65	-.01	-.0600
.70	-.00	-.0399
.75	-.00	.0345
.80	-.00	.0341
.85	.00	.0477
.90	.00	.1059

X/C	Z/C	CP
0.00	.01	.0052
.05	.03	-.4737
.10	.04	-.5512
.15	.05	-.5597
.20	.06	-.5682
.25	.06	-.5878
.30	.07	-.5987
.35	.07	-.5927
.40	.07	-.6056
.45	.07	-.5685
.50	.07	-.5351
.55	.06	-.4849
.60	.06	-.4524
.65	.05	-.3989
.70	.05	-.3508
.75	.04	-.2997
.80	.04	-.2520
.85	.03	-.1940
0.00	.01	.6087
.04	-.00	.0142
.09	-.01	.0151
.14	-.01	-.0029
.19	-.01	.0014
.24	-.01	-.0211
.29	-.01	-.0241
.34	-.01	-.0288
.39	-.01	-.0346
.44	-.01	-.0252
.49	-.01	-.0074
.54	-.01	.0092
.59	-.01	.0248
.64	-.00	.0277
.69	-.00	.0482
.74	.00	.0640
.79	.00	.0881
.84	.00	.1059

X/C	Z/C	CP
0.00	-.01	.1244
.11	.03	.0152
.20	.05	.0070
.31	.06	.0014
.40	.07	.0075
.51	.06	.0006
.61	.06	.0038
.71	.05	.0017
0.00	-.01	.0081
.11	-.02	.0047
.21	-.02	.0048
.31	-.02	.0051
.40	-.02	.0060
.51	-.01	.0069
.61	-.01	.0034
.71	-.00	.0013

X/C	Z/C	CP
.11	.01	.0054
.21	.00	.0047
.31	.00	.0059
.41	.01	.0076
.51	.01	.0076
.62	.01	.0047
.71	.00	.5859
.11	-.05	.0051
.22	-.04	.0043
.32	-.03	.0056
.42	-.03	.0074
.51	-.02	.0073
.62	-.01	.0047
.72	-.00	.0048

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17039

MACH .602

Q 20352.1

ALPW

2.51

BETA

0.00

P1 80280.28

PT1 102542.36

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5771
.05	.05	-.4748
.10	.06	-.5024
.15	.06	-.4986
.20	.07	-.5178
.25	.07	-.5241
.30	.07	-.5381
.35	.07	-.5316
.40	.07	-.5331
.45	.07	-.5098
.50	.07	-.4718
.55	.06	-.4460
.60	.06	-.4037
.65	.05	-.3655
.70	.05	-.3136
.75	.04	-.2696
.80	.03	-.2302
.85	.03	-.1789
.90	.02	-.1165
0.00	.03	.4661
.05	.01	.0276
.10	.01	-.0109
.15	.00	-.0268
.20	-.00	-.0499
.25	-.00	-.0628
.30	-.01	-.0638
.35	-.01	-.0649
.40	-.01	-.0660
.45	-.01	-.0882
.50	-.01	-.0918
.55	-.01	-.0817
.60	-.01	-.0673
.65	-.01	-.0504
.70	-.00	-.0289
.75	-.00	.0393
.80	-.00	.0384
.85	.00	.0542
.90	.00	.1149

X/C	Z/C	CP
0.00	.01	.0059
.05	.03	-.5615
.10	.04	-.6179
.15	.05	-.6104
.20	.06	-.6230
.25	.06	-.6237
.30	.07	-.6355
.35	.07	-.6226
.40	.07	-.6292
.45	.07	-.5953
.50	.07	-.5483
.55	.06	-.5093
.60	.06	-.4627
.65	.05	-.4649
.70	.05	-.3601
.75	.04	-.3088
.80	.04	-.2537
.85	.03	-.1954
0.00	.01	.5400
.04	-.00	.0240
.09	-.01	.0322
.14	-.01	.0288
.19	-.01	.0265
.24	-.01	.0060
.29	-.01	-.0048
.34	-.01	-.0100
.39	-.01	-.0172
.44	-.01	-.0108
.49	-.01	.0052
.54	-.01	.0159
.59	-.01	.0364
.64	-.00	.0327
.69	-.00	.0518
.74	.00	.0714
.79	.00	.0926
.84	.00	.1095

X/C	Z/C	CP
0.00	-.01	.1299
.11	.03	.0199
.20	.05	.0079
.31	.06	.0071
.40	.07	.0059
.51	.06	.0093
.61	.06	.0045
.71	.05	.0074
0.00	-.01	.0036
.11	-.02	.0054
.21	-.02	.0044
.31	-.02	.0090
.40	-.02	.0059
.51	-.01	.0034
.61	-.01	.0041
.71	-.00	.0070

X/C	Z/C	CP
.11	.01	.0059
.21	.00	.0038
.31	.00	.0066
.41	.01	.0078
.51	.01	.0026
.62	.01	.0055
.71	.00	.5269
.11	-.05	.0058
.22	-.04	.0035
.32	-.03	.0063
.42	-.03	.0074
.51	-.02	.0023
.62	-.01	.0051
.72	-.00	.0020

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17040

MACH .602

Q 20354.7

ALPW

2.99

BETA

0.00

P1 80286.00

PT1 102551.02

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5509
.05	.05	-.5358
.10	.06	-.5560
.15	.06	-.5434
.20	.07	-.5382
.25	.07	-.5481
.30	.07	-.5556
.35	.07	-.5458
.40	.07	-.5499
.45	.07	-.5323
.50	.07	-.4959
.55	.06	-.4618
.60	.06	-.4156
.65	.05	-.3766
.70	.05	-.3192
.75	.04	-.2789
.80	.03	-.2334
.85	.03	-.1789
.90	.02	-.1190
0.00	.03	.4101
.05	.01	.0727
.10	.01	.0251
.15	.00	-.0017
.20	-.00	-.0210
.25	-.00	-.0429
.30	-.01	-.0450
.35	-.01	-.0427
.40	-.01	-.0499
.45	-.01	-.0765
.50	-.01	-.0769
.55	-.01	-.0647
.60	-.01	-.0576
.65	-.01	-.0370
.70	-.00	-.0221
.75	-.00	.0427
.80	-.00	.0435
.85	.00	.0580
.90	.00	.1169

X/C	Z/C	CP
0.00	.01	.0045
.05	.03	-.6716
.10	.04	-.6793
.15	.05	-.6825
.20	.06	-.6736
.25	.06	-.6659
.30	.07	-.6691
.35	.07	-.6611
.40	.07	-.6581
.45	.07	-.6224
.50	.07	-.5732
.55	.06	-.5207
.60	.06	-.4803
.65	.05	-.4241
.70	.05	-.3706
.75	.04	-.3161
.80	.04	-.2606
.85	.03	-.2028
0.00	.01	.4452
.04	-.00	.0096
.09	-.01	.0663
.14	-.01	.0674
.19	-.01	.0691
.24	-.01	.0322
.29	-.01	.0225
.34	-.01	.0132
.39	-.01	.0019
.44	-.01	.0071
.49	-.01	.0163
.54	-.01	.0334
.59	-.01	.0462
.64	-.00	.0442
.69	-.00	.0618
.74	.00	.0797
.79	.00	.1093
.84	.00	.1191

X/C	Z/C	CP
0.00	-.01	.1376
.11	.03	.0100
.20	.05	.0109
.31	.06	.0042
.40	.07	.0016
.51	.06	.0021
.61	.06	.0069
.71	.05	.0068
0.00	-.01	.0023
.11	-.02	.0055
.21	-.02	.0048
.31	-.02	.0032
.40	-.02	.0034
.51	-.01	.0048
.61	-.01	.0061
.71	-.00	.0061

X/C	Z/C	CP
.11	.01	.0050
.21	.00	.0052
.31	.00	.0075
.41	.01	.0030
.51	.01	.0064
.62	.01	.0059
.71	.00	.4398
.11	-.05	.0043
.22	-.04	.0046
.32	-.03	.0067
.42	-.03	.0024
.51	-.02	.0058
.62	-.01	.0054
.72	-.00	.0065

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17041

MACH .603

Q 20417.9

ALPW

4.04

BETA

0.00

P1 80202.41

PT1 102544.77

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4143
.05	.05	-.6920
.10	.06	-.6806
.15	.06	-.6370
.20	.07	-.6101
.25	.07	-.6113
.30	.07	-.6159
.35	.07	-.6059
.40	.07	-.6007
.45	.07	-.5738
.50	.07	-.5302
.55	.06	-.4930
.60	.06	-.4380
.65	.05	-.3983
.70	.05	-.3397
.75	.04	-.2888
.80	.03	-.2403
.85	.03	-.1858
.90	.02	-.1216
0.00	.03	.1784
.05	.01	.1599
.10	.01	.0893
.15	.00	.0538
.20	-.00	.0328
.25	-.00	.0013
.30	-.01	.0019
.35	-.01	-.0013
.40	-.01	-.0048
.45	-.01	-.0451
.50	-.01	-.0478
.55	-.01	-.0388
.60	-.01	-.0311
.65	-.01	-.0188
.70	-.00	-.0014
.75	-.00	.0612
.80	-.00	.0584
.85	.00	.0690
.90	.00	.1230

X/C	Z/C	CP
0.00	.01	.0019
.05	.03	-.8690
.10	.04	-.8352
.15	.05	-.7829
.20	.06	-.7681
.25	.06	-.7453
.30	.07	-.7417
.35	.07	-.7200
.40	.07	-.7028
.45	.07	-.6666
.50	.07	-.6128
.55	.06	-.5552
.60	.06	-.5033
.65	.05	-.4397
.70	.05	-.3794
.75	.04	-.3171
.80	.04	-.2562
.85	.03	-.1931
0.00	.01	.1943
.04	-.00	.0111
.09	-.01	.1753
.14	-.01	.1342
.19	-.01	.1353
.24	-.01	.0844
.29	-.01	.0642
.34	-.01	.0488
.39	-.01	.0434
.44	-.01	.0360
.49	-.01	.0460
.54	-.01	.0586
.59	-.01	.0678
.64	-.00	.0689
.69	-.00	.0828
.74	.00	.0989
.79	.00	.1132
.84	.00	.1238

X/C	Z/C	CP
0.00	-.01	.1414
.11	.03	.0130
.20	.05	.0007
.31	.06	.0075
.40	.07	.0091
.51	.06	-.0015
.61	.06	.0041
.71	.05	.0051
0.00	-.01	.0013
.11	-.02	.0061
.21	-.02	.0023
.31	-.02	.0049
.40	-.02	.0043
.51	-.01	.0056
.61	-.01	.0037
.71	-.00	.0048

X/C	Z/C	CP
.11	.01	.0020
.21	.00	.0074
.31	.00	.0035
.41	.01	.0050
.51	.01	.0031
.62	.01	.0075
.71	.00	.1553
.11	-.05	.0018
.22	-.04	.0070
.32	-.03	.0031
.42	-.03	.0047
.51	-.02	.0027
.62	-.01	.0071
.72	-.00	.0031

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17042

MACH .603

Q 20396.6

ALPW

5.97

BETA

0.00

P1 80224.37

PT1 102540.81

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.0337
.05	.05	-.9763
.10	.06	-.8714
.15	.06	-.7984
.20	.07	-.7669
.25	.07	-.7410
.30	.07	-.7242
.35	.07	-.7020
.40	.07	-.6807
.45	.07	-.6457
.50	.07	-.5886
.55	.06	-.5363
.60	.06	-.4766
.65	.05	-.4273
.70	.05	-.3606
.75	.04	-.3041
.80	.03	-.2536
.85	.03	-.1890
.90	.02	-.1220
0.00	.03	-.3729
.05	.01	.2952
.10	.01	.2015
.15	.00	.1458
.20	-.00	.1068
.25	-.00	.0762
.30	-.01	.0788
.35	-.01	.0760
.40	-.01	.0730
.45	-.01	.0083
.50	-.01	.0118
.55	-.01	.0136
.60	-.01	.0151
.65	-.01	.0229
.70	-.00	.0333
.75	-.00	.0756
.80	-.00	.0729
.85	.00	.0840
.90	.00	.0960

X/C	Z/C	CP
0.00	.01	.0032
.05	.03	-1.2185
.10	.04	-1.0810
.15	.05	-.9894
.20	.06	-.9211
.25	.06	-.8773
.30	.07	-.8428
.35	.07	-.8022
.40	.07	-.7715
.45	.07	-.7049
.50	.07	-.6417
.55	.06	-.5706
.60	.06	-.5005
.65	.05	-.4262
.70	.05	-.3564
.75	.04	-.2911
.80	.04	-.2281
.85	.03	-.1676
0.00	.01	-.4388
.04	-.00	.0007
.09	-.01	.2851
.14	-.01	.2304
.19	-.01	.1964
.24	-.01	.1557
.29	-.01	.1298
.34	-.01	.1077
.39	-.01	.0895
.44	-.01	.0826
.49	-.01	.0855
.54	-.01	.0841
.59	-.01	.0917
.64	-.00	.0909
.69	-.00	.1024
.74	.00	.1109
.79	.00	.1233
.84	.00	.1319

X/C	Z/C	CP
0.00	-.01	.1403
.11	.03	.0048
.20	.05	-.0034
.31	.06	.0035
.40	.07	-.0004
.51	.06	-.0076
.61	.06	.0032
.71	.05	.0032
0.00	-.01	.0014
.11	-.02	.0027
.21	-.02	-.0001
.31	-.02	.0033
.40	-.02	.0038
.51	-.01	.0003
.61	-.01	.0029
.71	-.00	.0030

X/C	Z/C	CP
.11	.01	.0033
.21	.00	.0021
.31	.00	.0010
.41	.01	.0023
.51	.01	.0012
.62	.01	.0012
.71	.00	-.3773
.11	-.05	.0032
.22	-.04	.0022
.32	-.03	.0010
.42	-.03	.0024
.51	-.02	.0015
.62	-.01	.0010
.72	-.00	.0004

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 13

TP 17043

MACH .603

Q 20407.3

ALPW

-.03

BETA

0.00

P1 80203.46

PT1 102533.15

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5107
.05	.05	-.1328
.10	.06	-.2505
.15	.06	-.2903
.20	.07	-.3289
.25	.07	-.3640
.30	.07	-.3863
.35	.07	-.3993
.40	.07	-.4110
.45	.07	-.4015
.50	.07	-.3906
.55	.06	-.3669
.60	.06	-.3344
.65	.05	-.3075
.70	.05	-.2649
.75	.04	-.2318
.80	.03	-.1967
.85	.03	-.1559
.90	.02	-.1035
0.00	.03	.5909
.05	.01	-.2509
.10	.01	-.1983
.15	.00	-.1822
.20	-.00	-.1779
.25	-.00	-.1822
.30	-.01	-.1786
.35	-.01	-.1779
.40	-.01	-.1798
.45	-.01	-.1796
.50	-.01	-.1790
.55	-.01	-.1652
.60	-.01	-.1421
.65	-.01	-.1144
.70	-.00	-.0899
.75	-.00	-.0439
.80	-.00	-.0258
.85	.00	.0005
.90	.00	.0737

X/C	Z/C	CP
0.00	.01	.0052
.05	.03	-.1041
.10	.04	-.2619
.15	.05	-.3275
.20	.06	-.3678
.25	.06	-.4058
.30	.07	-.4352
.35	.07	-.4528
.40	.07	-.4625
.45	.07	-.4605
.50	.07	-.4350
.55	.06	-.4055
.60	.06	-.3806
.65	.05	-.3755
.70	.05	-.3013
.75	.04	-.2624
.80	.04	-.2185
.85	.03	-.1781
0.00	.01	.5633
.04	-.00	.0175
.09	-.01	-.1652
.14	-.01	-.1512
.19	-.01	-.1538
.24	-.01	-.1360
.29	-.01	-.1240
.34	-.01	-.1185
.39	-.01	-.1128
.44	-.01	-.0965
.49	-.01	-.0738
.54	-.01	-.0457
.59	-.01	-.0236
.64	-.00	-.0178
.69	-.00	-.0012
.74	.00	.0208
.79	.00	.0490
.84	.00	.0766

X/C	Z/C	CP
0.00	-.01	.0981
.11	.03	.0184
.20	.05	.0042
.31	.06	.0041
.40	.07	.0095
.51	.06	-.0027
.61	.06	.0060
.71	.05	.0078
0.00	-.01	.0047
.11	-.02	.0055
.21	-.02	.0054
.31	-.02	.0049
.40	-.02	.0053
.51	-.01	.0076
.61	-.01	.0055
.71	-.00	.0075

X/C	Z/C	CP
.11	.01	.0055
.21	.00	.0086
.31	.00	.0036
.41	.01	.0072
.51	.01	.0051
.62	.01	.0059
.71	.00	.6123
.11	-.05	.0051
.22	-.04	.0083
.32	-.03	.0034
.42	-.03	.0068
.51	-.02	.0048
.62	-.01	.0056
.72	-.00	.0057

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 14

TP 17060

MACH .827

0

31269.9

ALPW

.01

BETA

0.00

P1 65352.50

PT1 102335.64

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5155
.05	.05	-.0972
.10	.06	-.2295
.15	.06	-.2913
.20	.07	-.3452
.25	.07	-.3966
.30	.07	-.4305
.35	.07	-.4929
.40	.07	-.5455
.45	.07	-.5904
.50	.07	-.6097
.55	.06	-.6162
.60	.06	-.5683
.65	.05	-.4641
.70	.05	-.3500
.75	.04	-.2993
.80	.03	-.2400
.85	.03	-.1813
.90	.02	-.1039
0.00	.03	.6107
.05	.01	-.3245
.10	.01	-.2567
.15	.00	-.2324
.20	-.00	-.2309
.25	-.00	-.2354
.30	-.01	-.2404
.35	-.01	-.2379
.40	-.01	-.2400
.45	-.01	-.2349
.50	-.01	-.2214
.55	-.01	-.1572
.60	-.01	-.1196
.65	-.01	-.0820
.70	-.00	-.0822
.75	-.00	-.0034
.80	-.00	.0445
.85	.00	.0635
.90	.00	.1127

X/C	Z/C	CP
0.00	.01	.0187
.05	.03	-.1024
.10	.04	-.2963
.15	.05	-.3826
.20	.06	-.4568
.25	.06	-.5096
.30	.07	-.5809
.35	.07	-.6174
.40	.07	-.7413
.45	.07	-.7843
.50	.07	-.6800
.55	.06	-.5324
.60	.06	-.4815
.65	.05	-.4745
.70	.05	-.4041
.75	.04	-.3511
.80	.04	-.2341
.85	.03	-.2321
0.00	.01	.6181
.04	-.00	.0288
.09	-.01	-.2530
.14	-.01	-.2116
.19	-.01	-.1843
.24	-.01	-.1718
.29	-.01	-.1629
.34	-.01	-.1460
.39	-.01	-.1415
.44	-.01	-.1180
.49	-.01	-.1145
.54	-.01	-.0487
.59	-.01	-.0208
.64	-.00	-.0225
.69	-.00	.0061
.74	.00	.0342
.79	.00	.0699
.84	.00	.0987

X/C	Z/C	CP
0.00	-.01	.1267
.11	.03	.0223
.20	.05	.0201
.31	.06	.0186
.40	.07	.0241
.51	.06	.0161
.61	.06	.0145
.71	.05	.0209
0.00	-.01	.0150
.11	-.02	.0189
.21	-.02	.0220
.31	-.02	.0217
.40	-.02	.0138
.51	-.01	.0156
.61	-.01	.0138
.71	-.00	.0202

X/C	Z/C	CP
.11	.01	.0188
.21	.00	.0155
.31	.00	.0148
.41	.01	.0127
.51	.01	.0175
.62	.01	.0164
.71	.00	.6159
.11	-.05	.0182
.22	-.04	.0149
.32	-.03	.0143
.42	-.03	.0122
.51	-.02	.0169
.62	-.01	.0159
.72	-.00	.0143

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 14

TP 17061

MACH .826

Q 31250.1

ALPW

1.05

BETA

0.00

P1 65382.10

PT1 102335.30

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5932	0.00	.01	.0183	0.00	-.01	.1462	.11	.01	.0182
.05	.05	-.2141	.05	.03	-.2601	.11	.03	.0138	.21	.00	.0142
.10	.06	-.3285	.10	.04	-.4378	.20	.05	.0148	.31	.00	.0185
.15	.06	-.3790	.15	.05	-.5155	.31	.06	.0151	.41	.01	.0181
.20	.07	-.4299	.20	.06	-.5833	.40	.07	.0159	.51	.01	.0159
.25	.07	-.4736	.25	.06	-.6383	.51	.06	.0172	.62	.01	.0168
.30	.07	-.5035	.30	.07	-.6958	.61	.06	.0169	.71	.00	.6504
.35	.07	-.5611	.35	.07	-.7532	.71	.05	.0246	.11	-.05	.0176
.40	.07	-.5964	.40	.07	-.8212	0.00	-.01	.0119	.22	-.04	.0138
.45	.07	-.6542	.45	.07	-.8573	.11	-.02	.0162	.32	-.03	.0179
.50	.07	-.6666	.50	.07	-.8959	.21	-.02	.0173	.42	-.03	.0177
.55	.06	-.6787	.55	.06	-.8925	.31	-.02	.0176	.51	-.02	.0155
.60	.06	-.6760	.60	.06	-.6012	.40	-.02	.0183	.62	-.01	.0164
.65	.05	-.6480	.65	.05	-.5006	.51	-.01	.0162	.72	-.00	.0163
.70	.05	-.4293	.70	.05	-.4217	.61	-.01	.0135			
.75	.04	-.3014	.75	.04	-.3614	.71	-.00	.0165			
.80	.03	-.2381	.80	.04	-.2247						
.85	.03	-.1790	.85	.03	-.2219						
.90	.02	-.1066	0.00	.01	.6407						
0.00	.03	.6253	.04	-.00	.0223						
.05	.01	-.1827	.09	-.01	-.1306						
.10	.01	-.1669	.14	-.01	-.1086						
.15	.00	-.1662	.19	-.01	-.1039						
.20	-.00	-.1718	.24	-.01	-.0999						
.25	-.00	-.1839	.29	-.01	-.0901						
.30	-.01	-.1948	.34	-.01	-.0892						
.35	-.01	-.2011	.39	-.01	-.0884						
.40	-.01	-.2028	.44	-.01	-.0696						
.45	-.01	-.1902	.49	-.01	-.0582						
.50	-.01	-.1907	.54	-.01	-.0272						
.55	-.01	-.1755	.59	-.01	.0001						
.60	-.01	-.1115	.64	-.00	.0148						
.65	-.01	-.0984	.69	-.00	.0411						
.70	-.00	-.0839	.74	.00	.0608						
.75	-.00	.0080	.79	.00	.1014						
.80	-.00	.0292	.84	.00	.1230						
.85	.00	.0390									
.90	.00	.1259									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 14

TP 17062

MACH .827

Q 31287.4

ALPW

1.44

BETA

0.00

P1 65326.32

PT1 102336.08

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6126
.05	.05	-.2514
.10	.06	-.3626
.15	.06	-.4149
.20	.07	-.4584
.25	.07	-.4968
.30	.07	-.5318
.35	.07	-.5701
.40	.07	-.6161
.45	.07	-.6656
.50	.07	-.6900
.55	.06	-.7056
.60	.06	-.7083
.65	.05	-.6898
.70	.05	-.5055
.75	.04	-.3140
.80	.03	-.2371
.85	.03	-.1766
.90	.02	-.1013
0.00	.03	.6208
.05	.01	-.1454
.10	.01	-.1325
.15	.00	-.1431
.20	-.00	-.1485
.25	-.00	-.1676
.30	-.01	-.1681
.35	-.01	-.1693
.40	-.01	-.1805
.45	-.01	-.1745
.50	-.01	-.1660
.55	-.01	-.1547
.60	-.01	-.1384
.65	-.01	-.1115
.70	-.00	-.0757
.75	-.00	.0111
.80	-.00	.0112
.85	.00	.0377
.90	.00	.1207

X/C	Z/C	CP
0.00	.01	.0156
.05	.03	-.3180
.10	.04	-.4904
.15	.05	-.5698
.20	.06	-.6252
.25	.06	-.6826
.30	.07	-.7435
.35	.07	-.7889
.40	.07	-.8566
.45	.07	-.9044
.50	.07	-.9287
.55	.06	-.9501
.60	.06	-.7845
.65	.05	-.5740
.70	.05	-.4196
.75	.04	-.3707
.80	.04	-.2141
.85	.03	-.2074
0.00	.01	.6409
.04	-.00	.0230
.09	-.01	-.0844
.14	-.01	-.0855
.19	-.01	-.0807
.24	-.01	-.0827
.29	-.01	-.0792
.34	-.01	-.0750
.39	-.01	-.0755
.44	-.01	-.0585
.49	-.01	-.0628
.54	-.01	-.0161
.59	-.01	.0195
.64	-.00	.0221
.69	-.00	.0487
.74	.00	.0703
.79	.00	.1118
.84	.00	.1355

X/C	Z/C	CP
0.00	-.01	.1619
.11	.03	.0119
.20	.05	.0203
.31	.06	.0295
.40	.07	.0181
.51	.06	.0083
.61	.06	.0161
.71	.05	.0183
0.00	-.01	.0135
.11	-.02	.0180
.21	-.02	.0177
.31	-.02	.0182
.40	-.02	.0174
.51	-.01	.0022
.61	-.01	.0255
.71	-.00	.0170

X/C	Z/C	CP
.11	.01	.0157
.21	.00	.0172
.31	.00	.0178
.41	.01	.0161
.51	.01	.0147
.62	.01	.0119
.71	.00	.6487
.11	-.05	.0152
.22	-.04	.0167
.32	-.03	.0171
.42	-.03	.0156
.51	-.02	.0143
.62	-.01	.0115
.72	-.00	.0141

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 14

TP 17063

MACH .826

Q 31259.1

ALPW

2.04

BETA

0.00

P1 65370.38

PT1 102337.06

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6212	0.00	.01	.0167	0.00	-.01	.1634	.11	.01	.0168
.05	.05	-.3277	.05	.03	-.4171	.11	.03	.0182	.21	.00	.0157
.10	.06	-.4279	.10	.04	-.5911	.20	.05	.0169	.31	.00	.0212
.15	.06	-.4607	.15	.05	-.6408	.31	.06	.0273	.41	.01	.0137
.20	.07	-.4981	.20	.06	-.6893	.40	.07	.0136	.51	.01	.0159
.25	.07	-.5520	.25	.06	-.7378	.51	.06	.0219	.62	.01	.0181
.30	.07	-.5841	.30	.07	-.8027	.61	.06	.0300	.71	.00	.6342
.35	.07	-.6034	.35	.07	-.8506	.71	.05	.0119	.11	-.05	.0164
.40	.07	-.6459	.40	.07	-.9109	0.00	-.01	.0118	.22	-.04	.0154
.45	.07	-.7060	.45	.07	-.9731	.11	-.02	.0134	.32	-.03	.0210
.50	.07	-.7172	.50	.07	-.9998	.21	-.02	.0204	.42	-.03	.0134
.55	.06	-.7365	.55	.06	-1.0194	.31	-.02	.0230	.51	-.02	.0154
.60	.06	-.7500	.60	.06	-.9442	.40	-.02	.0135	.62	-.01	.0178
.65	.05	-.7514	.65	.05	-.5852	.51	-.01	.0198	.72	-.00	.0111
.70	.05	-.6873	.70	.05	-.4196	.61	-.01	.0245			
.75	.04	-.3713	.75	.04	-.3362	.71	-.00	.0114			
.80	.03	-.2504	.80	.04	-.2102						
.85	.03	-.1735	.85	.03	-.2012						
.90	.02	-.1047	0.00	.01	.6238						
0.00	.03	.5975	.04	-.00	.0179						
.05	.01	-.0709	.09	-.01	-.0288						
.10	.01	-.0902	.14	-.01	-.0423						
.15	.00	-.1029	.19	-.01	-.0449						
.20	-.00	-.1135	.24	-.01	-.0402						
.25	-.00	-.1309	.29	-.01	-.0482						
.30	-.01	-.1495	.34	-.01	-.0560						
.35	-.01	-.1644	.39	-.01	-.0510						
.40	-.01	-.1681	.44	-.01	-.0395						
.45	-.01	-.1579	.49	-.01	-.0406						
.50	-.01	-.1596	.54	-.01	-.0008						
.55	-.01	-.1459	.59	-.01	.0289						
.60	-.01	-.1259	.64	-.00	.0314						
.65	-.01	-.1015	.69	-.00	.0586						
.70	-.00	-.0612	.74	.00	.0784						
.75	-.00	.0222	.79	.00	.1149						
.80	-.00	.0245	.84	.00	.1288						
.85	.00	.0434									
.90	.00	.1137									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 14

TP 17064

MACH .827

Q 31290.9

ALPW

2.53

BETA

0.00

P1 65327.22

PT1 102341.57

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6221
.05	.05	-.3711
.10	.06	-.4810
.15	.06	-.5191
.20	.07	-.5330
.25	.07	-.5780
.30	.07	-.6084
.35	.07	-.6517
.40	.07	-.6608
.45	.07	-.7236
.50	.07	-.7272
.55	.06	-.7559
.60	.06	-.7675
.65	.05	-.7691
.70	.05	-.7597
.75	.04	-.4484
.80	.03	-.2515
.85	.03	-.1783
.90	.02	-.1038
0.00	.03	.5797
.05	.01	-.0275
.10	.01	-.0521
.15	.00	-.0745
.20	-.00	-.0849
.25	-.00	-.1045
.30	-.01	-.1091
.35	-.01	-.1197
.40	-.01	-.1285
.45	-.01	-.1332
.50	-.01	-.1292
.55	-.01	-.1202
.60	-.01	-.1085
.65	-.01	-.0927
.70	-.00	-.0613
.75	-.00	-.0026
.80	-.00	.0126
.85	.00	.0414
.90	.00	.1190

X/C	Z/C	CP
0.00	.01	.0176
.05	.03	-.4935
.10	.04	-.6504
.15	.05	-.7236
.20	.06	-.7371
.25	.06	-.7827
.30	.07	-.8459
.35	.07	-.8948
.40	.07	-.9433
.45	.07	-1.0138
.50	.07	-1.0393
.55	.06	-1.0431
.60	.06	-.7967
.65	.05	-.6566
.70	.05	-.5048
.75	.04	-.4637
.80	.04	-.2189
.85	.03	-.2090
0.00	.01	.5907
.04	-.00	.0205
.09	-.01	.0186
.14	-.01	-.0015
.19	-.01	.0073
.24	-.01	-.0133
.29	-.01	-.0272
.34	-.01	-.0316
.39	-.01	-.0294
.44	-.01	-.0263
.49	-.01	-.0303
.54	-.01	-.0053
.59	-.01	.0380
.64	-.00	.0371
.69	-.00	.0647
.74	.00	.0839
.79	.00	.1221
.84	.00	.1416

X/C	Z/C	CP
0.00	-.01	.1607
.11	.03	.0084
.20	.05	.0102
.31	.06	.0114
.40	.07	.0122
.51	.06	.0216
.61	.06	.0177
.71	.05	.0120
0.00	-.01	.0109
.11	-.02	.0147
.21	-.02	.0046
.31	-.02	.0062
.40	-.02	.0095
.51	-.01	.0177
.61	-.01	.0171
.71	-.00	.0117

X/C	Z/C	CP
.11	.01	.0167
.21	.00	.0145
.31	.00	.0110
.41	.01	.0151
.51	.01	.0165
.62	.01	.0137
.71	.00	.6179
.11	-.05	.0154
.22	-.04	.0142
.32	-.03	.0107
.42	-.03	.0149
.51	-.02	.0162
.62	-.01	.0134
.72	-.00	.0095

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 14

TP 17065

MACH .826

0

31259.7

ALPW

-.05

BETA

0.00

P1 65374.34

PT1 102341.47

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5059	0.00	.01	.0120	0.00	-.01	.1335	.11	.01	.0122
.05	.05	-.0917	.05	.03	-.0874	.11	.03	.0128	.21	.00	.0173
.10	.06	-.2223	.10	.04	-.2796	.20	.05	.0189	.31	.00	.0121
.15	.06	-.2911	.15	.05	-.3760	.31	.06	.0146	.41	.01	.0115
.20	.07	-.3383	.20	.06	-.4363	.40	.07	.0178	.51	.01	.0175
.25	.07	-.3958	.25	.06	-.5059	.51	.06	.0177	.62	.01	.0166
.30	.07	-.4331	.30	.07	-.5813	.61	.06	.0067	.71	.00	.6110
.35	.07	-.4951	.35	.07	-.6205	.71	.05	.0120	.11	-.05	.0167
.40	.07	-.5352	.40	.07	-.7379	0.00	-.01	.0139	.22	-.04	.0173
.45	.07	-.5866	.45	.07	-.7351	.11	-.02	.0171	.32	-.03	.0122
.50	.07	-.5928	.50	.07	-.6696	.21	-.02	.0119	.42	-.03	.0115
.55	.06	-.6026	.55	.06	-.5611	.31	-.02	.0119	.51	-.02	.0176
.60	.06	-.5662	.60	.06	-.4901	.40	-.02	.0175	.62	-.01	.0167
.65	.05	-.4536	.65	.05	-.4818	.51	-.01	.0106	.72	-.00	.0115
.70	.05	-.3562	.70	.05	-.3749	.61	-.01	.0103			
.75	.04	-.2950	.75	.04	-.3167	.71	-.00	.0158			
.80	.03	-.2421	.80	.04	-.2362						
.85	.03	-.1812	.85	.03	-.1726						
.90	.02	-.1083	0.00	.01	.5796						
0.00	.03	.6087	.04	-.00	.0210						
.05	.01	-.3311	.09	-.01	-.2187						
.10	.01	-.2516	.14	-.01	-.2168						
.15	.00	-.2402	.19	-.01	-.1866						
.20	-.00	-.2318	.24	-.01	-.1751						
.25	-.00	-.2442	.29	-.01	-.1612						
.30	-.01	-.2367	.34	-.01	-.1541						
.35	-.01	-.2354	.39	-.01	-.1421						
.40	-.01	-.2361	.44	-.01	-.1212						
.45	-.01	-.2419	.49	-.01	-.1108						
.50	-.01	-.2359	.54	-.01	-.0726						
.55	-.01	-.2188	.59	-.01	-.0277						
.60	-.01	-.1946	.64	-.00	-.0222						
.65	-.01	-.1589	.69	-.00	-.0027						
.70	-.00	-.1229	.74	.00	.0288						
.75	-.00	-.0255	.79	.00	.0762						
.80	-.00	-.0196	.84	.00	.0977						
.85	.00	.0107									
.90	.00	.0938									

7 X 10 HIGH SPEED TUNNEL

TP 17082

PT1 101981.28

$$Y/B/2 = 1.011$$

X/C	Z/C	CP
.11	.01	-.1201
.21	.00	-.1458
.31	.00	-.6208
.41	.01	-.7653
.51	.01	-.7667
.62	.01	-.6315
.71	.00	-.3905
.11	-.05	-.6163
.22	-.04	-.5340
.32	-.03	-.4562
.42	-.03	-.3149
.51	-.02	-.1578
.62	-.01	-.0030
.72	-.00	.1217

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17083

MACH .805

Q

30209.4

ALPW

-1.53

BETA

0.00

P1 66540.75

PT1 101969.87

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.2760	0.00	.01	.4472	0.00	-.01	.0934	.11	.01	-.1751
.05	.05	.0573	.05	.03	.1161	.11	.03	.0522	.21	.00	-.1196
.10	.06	-.0963	.10	.04	-.0882	.20	.05	-.0741	.31	.00	-.6675
.15	.06	-.1799	.15	.05	-.1948	.31	.06	-.2187	.41	.01	-.8270
.20	.07	-.2348	.20	.06	-.2676	.40	.07	-.5361	.51	.01	-.8876
.25	.07	-.2989	.25	.06	-.3336	.51	.06	-.6617	.62	.01	-.6463
.30	.07	-.3298	.30	.07	-.3945	.61	.06	-.5807	.71	.00	-.3860
.35	.07	-.3794	.35	.07	-.4426	.71	.05	-.3806	.11	-.05	-.5451
.40	.07	-.4302	.40	.07	-.4862	0.00	-.01	.0909	.22	-.04	-.4626
.45	.07	-.4371	.45	.07	-.4959	.11	-.02	-.3911	.32	-.03	-.3093
.50	.07	-.4487	.50	.07	-.5083	.21	-.02	.4693	.42	-.03	-.1526
.55	.06	-.4268	.55	.06	-.4560	.31	-.02	.5162	.51	-.02	-.0527
.60	.06	-.3986	.60	.06	-.4160	.40	-.02	-.2615	.62	-.01	.0558
.65	.05	-.3489	.65	.05	-.4081	.51	-.01	-.2702	.72	-.00	.1312
.70	.05	-.3076	.70	.05	-.3866	.61	-.01	-.0581			
.75	.04	-.2696	.75	.04	-.3457	.71	-.00	.0381			
.80	.03	-.2203	.80	.04	-.2148						
.85	.03	-.1692	.85	.03	-.2157						
.90	.02	-.1061	0.00	.01	.0658						
0.00	.03	.4301	.04	-.00	.2329						
.05	.01	-.5000	.09	-.01	-.5236						
.10	.01	-.3721	.14	-.01	-.4302						
.15	.00	-.3583	.19	-.01	-.3979						
.20	-.00	-.3456	.24	-.01	-.2988						
.25	-.00	-.3401	.29	-.01	-.2494						
.30	-.01	-.3272	.34	-.01	-.2228						
.35	-.01	-.3256	.39	-.01	-.2012						
.40	-.01	-.3088	.44	-.01	-.1655						
.45	-.01	-.3039	.49	-.01	-.1281						
.50	-.01	-.2844	.54	-.01	-.0901						
.55	-.01	-.2612	.59	-.01	-.0557						
.60	-.01	-.2213	.64	-.00	-.0549						
.65	-.01	-.1857	.69	-.00	.0157						
.70	-.00	-.1462	.74	.00	.0209						
.75	-.00	-.1038	.79	.00	.0436						
.80	-.00	-.0594	.84	.00	.0720						
.85	.00	-.0232									
.90	.00	.0174									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17084

MACH .806

Q 30255.9

ALPW

-1.05

BETA

0.00

P1 66462.90

PT1 101961.63

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$
[illegible]

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17085

MACH .806

Q 30216.2

ALPW

-.58

BETA

0.00

P1 66520.70

PT1 101960.79

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4359
.05	.05	-.0486
.10	.06	-.1830
.15	.06	-.2548
.20	.07	-.3036
.25	.07	-.3569
.30	.07	-.4135
.35	.07	-.4587
.40	.07	-.4915
.45	.07	-.5230
.50	.07	-.5244
.55	.06	-.4833
.60	.06	-.4443
.65	.05	-.3888
.70	.05	-.3305
.75	.04	-.2842
.80	.03	-.2398
.85	.03	-.1723
.90	.02	-.1125
0.00	.03	.5805
.05	.01	-.3854
.10	.01	-.2841
.15	.00	-.2579
.20	-.00	-.2582
.25	-.00	-.2678
.30	-.01	-.2672
.35	-.01	-.2644
.40	-.01	-.2599
.45	-.01	-.2563
.50	-.01	-.2483
.55	-.01	-.2379
.60	-.01	-.2041
.65	-.01	-.1611
.70	-.00	-.1192
.75	-.00	-.0777
.80	-.00	-.0363
.85	.00	-.0041
.90	.00	.0453

X/C	Z/C	CP
0.00	.01	.5678
.05	.03	-.0053
.10	.04	-.2013
.15	.05	-.3086
.20	.06	-.3743
.25	.06	-.4292
.30	.07	-.4932
.35	.07	-.5309
.40	.07	-.5672
.45	.07	-.5896
.50	.07	-.5595
.55	.06	-.5000
.60	.06	-.4533
.65	.05	-.4528
.70	.05	-.4233
.75	.04	-.3812
.80	.04	-.2384
.85	.03	-.2295
0.00	.01	.0795
.04	-.00	.4285
.09	-.01	-.2001
.14	-.01	-.2681
.19	-.01	-.2764
.24	-.01	-.2059
.29	-.01	-.1904
.34	-.01	-.1753
.39	-.01	-.1631
.44	-.01	-.1363
.49	-.01	-.1008
.54	-.01	-.0689
.59	-.01	-.0345
.64	-.00	-.0360
.69	-.00	.0349
.74	.00	.0350
.79	.00	.0639
.84	.00	.0879

X/C	Z/C	CP
0.00	-.01	.1063
.11	.03	.0741
.20	.05	-.1627
.31	.06	-.2940
.40	.07	-.5454
.51	.06	-.8136
.61	.06	-.6346
.71	.05	-.3979
0.00	-.01	.0955
.11	-.02	-.2921
.21	-.02	.1350
.31	-.02	.1755
.40	-.02	-.0769
.51	-.01	-.0698
.61	-.01	.0005
.71	-.00	.0588

X/C	Z/C	CP
.11	.01	-.2998
.21	.00	-.1418
.31	.00	-.7737
.41	.01	-.9251
.51	.01	-1.0314
.62	.01	-.7106
.71	.00	-.3838
.11	-.05	-.3095
.22	-.04	-.0985
.32	-.03	-.0451
.42	-.03	-.0166
.51	-.02	.0170
.62	-.01	.0629
.72	-.00	.1183

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17086

MACH .806

Q 30247.8

ALPW

.09

BETA

0.00

P1 66472.13

PT1 101959.18

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5217
.05	.05	-.1123
.10	.06	-.2452
.15	.06	-.3102
.20	.07	-.3563
.25	.07	-.4101
.30	.07	-.4506
.35	.07	-.5089
.40	.07	-.5338
.45	.07	-.5753
.50	.07	-.5536
.55	.06	-.5227
.60	.06	-.4751
.65	.05	-.4054
.70	.05	-.3506
.75	.04	-.2983
.80	.03	-.2502
.85	.03	-.1867
.90	.02	-.1116
0.00	.03	.6100
.05	.01	-.2986
.10	.01	-.2407
.15	.00	-.2260
.20	-.00	-.2226
.25	-.00	-.2281
.30	-.01	-.2252
.35	-.01	-.2187
.40	-.01	-.2174
.45	-.01	-.2229
.50	-.01	-.2127
.55	-.01	-.2014
.60	-.01	-.1715
.65	-.01	-.1428
.70	-.00	-.1108
.75	-.00	-.0664
.80	-.00	-.0251
.85	.00	.0132
.90	.00	.0478

X/C	Z/C	CP
0.00	.01	.6180
.05	.03	-.1136
.10	.04	-.2928
.15	.05	-.3944
.20	.06	-.4490
.25	.06	-.5244
.30	.07	-.5801
.35	.07	-.6120
.40	.07	-.6617
.45	.07	-.6441
.50	.07	-.6274
.55	.06	-.5668
.60	.06	-.4845
.65	.05	-.4882
.70	.05	-.4449
.75	.04	-.3992
.80	.04	-.2468
.85	.03	-.2444
0.00	.01	.0883
.04	-.00	.3874
.09	-.01	-.1301
.14	-.01	-.1972
.19	-.01	-.1945
.24	-.01	-.1693
.29	-.01	-.1515
.34	-.01	-.1404
.39	-.01	-.1354
.44	-.01	-.1112
.49	-.01	-.0800
.54	-.01	-.0516
.59	-.01	-.0219
.64	-.00	-.0205
.69	-.00	.0533
.74	.00	.0490
.79	.00	.0720
.84	.00	.0969

X/C	Z/C	CP
0.00	-.01	.1187
.11	.03	.0826
.20	.05	-.2221
.31	.06	-.3614
.40	.07	-.6247
.51	.06	-.9240
.61	.06	-.7918
.71	.05	-.4030
0.00	-.01	.0770
.11	-.02	-.1960
.21	-.02	.0613
.31	-.02	.0912
.40	-.02	-.0513
.51	-.01	-.0469
.61	-.01	.0047
.71	-.00	.0652

X/C	Z/C	CP
.11	.01	-.3855
.21	.00	-.1774
.31	.00	-.8799
.41	.01	-.9972
.51	.01	-1.0900
.62	.01	-.7787
.71	.00	-.4112
.11	-.05	.0067
.22	-.04	-.0327
.32	-.03	-.0072
.42	-.03	.0079
.51	-.02	.0398
.62	-.01	.0741
.72	-.00	.1309

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17087

MACH .806

Q 30236.3

ALPW

.52

BETA

0.00

P1 66487.39

PT1 101957.60

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5608	0.00	.01	.6406	0.00	-.01	.1285	.11	.01	-.4520
.05	.05	-.1610	.05	.03	-.1836	.11	.03	.0816	.21	.00	-.2300
.10	.06	-.2828	.10	.04	-.3596	.20	.05	-.3001	.31	.00	-.9635
.15	.06	-.3468	.15	.05	-.4423	.31	.06	-.4401	.41	.01	-1.0449
.20	.07	-.3907	.20	.06	-.5106	.40	.07	-.6238	.51	.01	-1.0738
.25	.07	-.4395	.25	.06	-.5619	.51	.06	-.9563	.62	.01	-.6812
.30	.07	-.4827	.30	.07	-.6121	.61	.06	-.8714	.71	.00	-.4056
.35	.07	-.5292	.35	.07	-.6716	.71	.05	-.4308	.11	-.05	.0361
.40	.07	-.5704	.40	.07	-.7499	0.00	-.01	.0597	.22	-.04	-.0106
.45	.07	-.5978	.45	.07	-.6790	.11	-.02	-.1234	.32	-.03	.0085
.50	.07	-.5834	.50	.07	-.6475	.21	-.02	.0589	.42	-.03	.0228
.55	.06	-.5512	.55	.06	-.5999	.31	-.02	.0588	.51	-.02	.0479
.60	.06	-.5090	.60	.06	-.4992	.40	-.02	-.0374	.62	-.01	.0864
.65	.05	-.4316	.65	.05	-.5054	.51	-.01	-.0314	.72	-.00	.1375
.70	.05	-.3650	.70	.05	-.4421	.61	-.01	.0212			
.75	.04	-.3068	.75	.04	-.4001	.71	-.00	.0638			
.80	.03	-.2499	.80	.04	-.2469						
.85	.03	-.1894	.85	.03	-.2129						
.90	.02	-.1185	0.00	.01	.0898						
0.00	.03	.6191	.04	-.00	.1230						
.05	.01	-.2486	.09	-.01	-.0734						
.10	.01	-.2037	.14	-.01	-.1407						
.15	.00	-.2046	.19	-.01	-.1339						
.20	-.00	-.1929	.24	-.01	-.1240						
.25	-.00	-.1946	.29	-.01	-.1181						
.30	-.01	-.2071	.34	-.01	-.1239						
.35	-.01	-.2139	.39	-.01	-.1150						
.40	-.01	-.2035	.44	-.01	-.0925						
.45	-.01	-.2175	.49	-.01	-.0666						
.50	-.01	-.2039	.54	-.01	-.0345						
.55	-.01	-.1800	.59	-.01	-.0074						
.60	-.01	-.1614	.64	-.00	-.0123						
.65	-.01	-.1234	.69	-.00	.0480						
.70	-.00	-.0918	.74	.00	.0597						
.75	-.00	-.0566	.79	.00	.0730						
.80	-.00	-.0226	.84	.00	.1002						
.85	.00	.0199									
.90	.00	.0501									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17088

MACH .806

Q 30220.8

ALPW

.96

BETA

0.00

P1 66509.10

PT1 101956.44

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5874
.05	.05	-.2123
.10	.06	-.3290
.15	.06	-.3856
.20	.07	-.4294
.25	.07	-.4807
.30	.07	-.5104
.35	.07	-.5503
.40	.07	-.6000
.45	.07	-.6491
.50	.07	-.6340
.55	.06	-.6241
.60	.06	-.5194
.65	.05	-.4492
.70	.05	-.3632
.75	.04	-.3170
.80	.03	-.2525
.85	.03	-.1926
.90	.02	-.1137
0.00	.03	.6239
.05	.01	-.1761
.10	.01	-.1669
.15	.00	-.1681
.20	-.00	-.1607
.25	-.00	-.1677
.30	-.01	-.1785
.35	-.01	-.1795
.40	-.01	-.1818
.45	-.01	-.1922
.50	-.01	-.1911
.55	-.01	-.1682
.60	-.01	-.1508
.65	-.01	-.1212
.70	-.00	-.0850
.75	-.00	-.0400
.80	-.00	-.0054
.85	.00	.0354
.90	.00	.0624

X/C	Z/C	CP
0.00	.01	.6446
.05	.03	-.2643
.10	.04	-.4196
.15	.05	-.5151
.20	.06	-.5648
.25	.06	-.6206
.30	.07	-.6804
.35	.07	-.7178
.40	.07	-.7932
.45	.07	-.7980
.50	.07	-.7228
.55	.06	-.5936
.60	.06	-.5138
.65	.05	-.5138
.70	.05	-.4724
.75	.04	-.4171
.80	.04	-.2565
.85	.03	-.2070
0.00	.01	.0970
.04	-.00	.1324
.09	-.01	-.0192
.14	-.01	-.1125
.19	-.01	-.1116
.24	-.01	-.0994
.29	-.01	-.0911
.34	-.01	-.0908
.39	-.01	-.0849
.44	-.01	-.0745
.49	-.01	-.0489
.54	-.01	-.0217
.59	-.01	.0038
.64	-.00	.0022
.69	-.00	.0615
.74	.00	.0696
.79	.00	.0856
.84	.00	.1083

X/C	Z/C	CP
0.00	-.01	.1371
.11	.03	.0620
.20	.05	-.3924
.31	.06	-.5724
.40	.07	-.6509
.51	.06	-.9639
.61	.06	-.9597
.71	.05	-.4504
0.00	-.01	.0162
.11	-.02	-.0482
.21	-.02	.0381
.31	-.02	.0398
.40	-.02	-.0267
.51	-.01	-.0186
.61	-.01	.0257
.71	-.00	.0708

X/C	Z/C	CP
.11	.01	-.5083
.21	.00	-.6504
.31	.00	-1.0347
.41	.01	-1.1311
.51	.01	-1.0680
.62	.01	-.6373
.71	.00	-.4169
.11	-.05	.0729
.22	-.04	.0182
.32	-.03	.0298
.42	-.03	.0364
.51	-.02	.0588
.62	-.01	.0856
.72	-.00	.1392

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

PUJN 15

TP 17089

MACH .807

Q

30271.8

ALPW

1.48

BETA

0.00

P1 66430.39

PT1 101953.59

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6063
.05	.05	-.2747
.10	.06	-.3866
.15	.06	-.4406
.20	.07	-.4650
.25	.07	-.5150
.30	.07	-.5381
.35	.07	-.5877
.40	.07	-.6388
.45	.07	-.6818
.50	.07	-.6875
.55	.06	-.6923
.60	.06	-.6099
.65	.05	-.4785
.70	.05	-.3767
.75	.04	-.3198
.80	.03	-.2633
.85	.03	-.1948
.90	.02	-.1179
0.00	.03	.6134
.05	.01	-.1267
.10	.01	-.1198
.15	.00	-.1206
.20	-.00	-.1236
.25	-.00	-.1566
.30	-.01	-.1561
.35	-.01	-.1607
.40	-.01	-.1679
.45	-.01	-.1778
.50	-.01	-.1715
.55	-.01	-.1547
.60	-.01	-.1341
.65	-.01	-.1108
.70	-.00	-.0717
.75	-.00	-.0398
.80	-.00	-.0019
.85	.00	.0278
.90	.00	.0625

X/C	Z/C	CP
0.00	.01	.6392
.05	.03	-.3486
.10	.04	-.5116
.15	.05	-.5848
.20	.06	-.6324
.25	.06	-.6931
.30	.07	-.7519
.35	.07	-.7830
.40	.07	-.8338
.45	.07	-.8921
.50	.07	-.9089
.55	.06	-.7271
.60	.06	-.4892
.65	.05	-.4884
.70	.05	-.4621
.75	.04	-.4160
.80	.04	-.2531
.85	.03	-.1978
0.00	.01	.0915
.04	-.00	.1160
.09	-.01	.0220
.14	-.01	-.0718
.19	-.01	-.0756
.24	-.01	-.0685
.29	-.01	-.0727
.34	-.01	-.0687
.39	-.01	-.0714
.44	-.01	-.0609
.49	-.01	-.0400
.54	-.01	-.0096
.59	-.01	.0185
.64	-.00	.0183
.69	-.00	.0735
.74	.00	.0750
.79	.00	.0903
.84	.00	.1144

X/C	Z/C	CP
0.00	-.01	.1410
.11	.03	.0164
.20	.05	-.4458
.31	.06	-.6142
.40	.07	-.8441
.51	.06	-.8788
.61	.06	-.9757
.71	.05	-.4986
0.00	-.01	-.0384
.11	-.02	-.0450
.21	-.02	.0326
.31	-.02	.0367
.40	-.02	-.0025
.51	-.01	.0039
.61	-.01	.0327
.71	-.00	.0717

X/C	Z/C	CP
.11	.01	-.6089
.21	.00	-.6784
.31	.00	-1.1026
.41	.01	-1.1615
.51	.01	-.9593
.62	.01	-.6172
.71	.00	-.4584
.11	-.05	.0677
.22	-.04	.0341
.32	-.03	.0376
.42	-.03	.0382
.51	-.02	.0545
.62	-.01	.0874
.72	-.00	.1366

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17090

MACH .806

Q 30223.7

ALPW

1.92

BETA

0.00

P1 66502.43

PT1 101954.27

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6139
.05	.05	-.3368
.10	.06	-.4343
.15	.06	-.4713
.20	.07	-.5107
.25	.07	-.5488
.30	.07	-.5722
.35	.07	-.6175
.40	.07	-.6594
.45	.07	-.7126
.50	.07	-.7270
.55	.06	-.7126
.60	.06	-.7023
.65	.05	-.4912
.70	.05	-.3794
.75	.04	-.3235
.80	.03	-.2687
.85	.03	-.1911
.90	.02	-.1192
0.00	.03	.6023
.05	.01	-.0887
.10	.01	-.0810
.15	.00	-.0792
.20	-.00	-.0809
.25	-.00	-.1265
.30	-.01	-.1335
.35	-.01	-.1381
.40	-.01	-.1377
.45	-.01	-.1482
.50	-.01	-.1535
.55	-.01	-.1448
.60	-.01	-.1260
.65	-.01	-.0949
.70	-.00	-.0722
.75	-.00	-.0346
.80	-.00	.0003
.85	.00	.0400
.90	.00	.0707

X/C	Z/C	CP
0.00	.01	.6313
.05	.03	-.4334
.10	.04	-.5788
.15	.05	-.6507
.20	.06	-.6898
.25	.06	-.7394
.30	.07	-.8070
.35	.07	-.8537
.40	.07	-.9122
.45	.07	-.9477
.50	.07	-.9412
.55	.06	-.8705
.60	.06	-.4973
.65	.05	-.5173
.70	.05	-.4650
.75	.04	-.4096
.80	.04	-.2504
.85	.03	-.1855
0.00	.01	.0977
.04	-.00	.1254
.09	-.01	.0526
.14	-.01	-.0321
.19	-.01	-.0341
.24	-.01	-.0408
.29	-.01	-.0492
.34	-.01	-.0535
.39	-.01	-.0561
.44	-.01	-.0373
.49	-.01	-.0234
.54	-.01	-.0000
.59	-.01	.0270
.64	-.00	.0193
.69	-.00	.0819
.74	.00	.0918
.79	.00	.1054
.84	.00	.1203

X/C	Z/C	CP
0.00	-.01	.1413
.11	.03	-.0213
.20	.05	-.5081
.31	.06	-.6872
.40	.07	-.8927
.51	.06	-.9100
.61	.06	-.9582
.71	.05	-.4761
0.00	-.01	-.0941
.11	-.02	-.0391
.21	-.02	.0202
.31	-.02	.0172
.40	-.02	.0058
.51	-.01	.0171
.61	-.01	.0396
.71	-.00	.0715

X/C	Z/C	CP
.11	.01	-.7384
.21	.00	-.7224
.31	.00	-1.1013
.41	.01	-1.0300
.51	.01	-.7441
.62	.01	-.5992
.71	.00	-.4844
.11	-.05	.0739
.22	-.04	.0744
.32	-.03	.0542
.42	-.03	.0474
.51	-.02	.0622
.62	-.01	.0835
.72	-.00	.1243

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17091

MACH .805

Q 30170.1

ALPW

2.51

BETA

0.00

P1 66573.27

PT1 101946.48

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6180
.05	.05	-.4170
.10	.06	-.4972
.15	.06	-.5209
.20	.07	-.5586
.25	.07	-.6032
.30	.07	-.6193
.35	.07	-.6530
.40	.07	-.6889
.45	.07	-.7417
.50	.07	-.7504
.55	.06	-.7587
.60	.06	-.7542
.65	.05	-.5404
.70	.05	-.3947
.75	.04	-.3240
.80	.03	-.2671
.85	.03	-.1914
.90	.02	-.1163
0.00	.03	.5742
.05	.01	-.0204
.10	.01	-.0349
.15	.00	-.0404
.20	-.00	-.0406
.25	-.00	-.1043
.30	-.01	-.1003
.35	-.01	-.1054
.40	-.01	-.1135
.45	-.01	-.1285
.50	-.01	-.1338
.55	-.01	-.1229
.60	-.01	-.1013
.65	-.01	-.0889
.70	-.00	-.0559
.75	-.00	-.0199
.80	-.00	.0073
.85	.00	.0367
.90	.00	.0735

X/C	Z/C	CP
0.00	.01	.6095
.05	.03	-.5569
.10	.04	-.6989
.15	.05	-.7386
.20	.06	-.7655
.25	.06	-.8284
.30	.07	-.8806
.35	.07	-.9117
.40	.07	-.9733
.45	.07	-1.0246
.50	.07	-1.0324
.55	.06	-1.0205
.60	.06	-.6356
.65	.05	-.5951
.70	.05	-.4865
.75	.04	-.4164
.80	.04	-.2400
.85	.03	-.1832
0.00	.01	.1040
.04	-.00	.1075
.09	-.01	.0544
.14	-.01	.0109
.19	-.01	.0137
.24	-.01	-.0174
.29	-.01	-.0185
.34	-.01	-.0241
.39	-.01	-.0270
.44	-.01	-.0163
.49	-.01	-.0024
.54	-.01	.0144
.59	-.01	.0384
.64	-.00	.0410
.69	-.00	.0936
.74	.00	.0960
.79	.00	.1056
.84	.00	.1200

X/C	Z/C	CP
0.00	-.01	.1441
.11	.03	-.0951
.20	.05	-.6500
.31	.06	-.7496
.40	.07	-1.0147
.51	.06	-1.0436
.61	.06	-.8668
.71	.05	-.4930
0.00	-.01	-.2583
.11	-.02	-.0247
.21	-.02	.0105
.31	-.02	.0123
.40	-.02	.0134
.51	-.01	.0145
.61	-.01	.0434
.71	-.00	.0657

X/C	Z/C	CP
.11	.01	-.8556
.21	.00	-.7493
.31	.00	-1.1755
.41	.01	-1.1024
.51	.01	-.8690
.62	.01	-.6463
.71	.00	-.4882
.11	-.05	.1142
.22	-.04	.1007
.32	-.03	.0650
.42	-.03	.0586
.51	-.02	.0706
.62	-.01	.0720
.72	-.00	.1149

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17092

MACH .806

Q

30252.6

ALPW

2.96

BETA

0.00

P1 66450.17

PT1 101945.51

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6083
.05	.05	-.4653
.10	.06	-.5417
.15	.06	-.5620
.20	.07	-.5918
.25	.07	-.6349
.30	.07	-.6568
.35	.07	-.6673
.40	.07	-.7139
.45	.07	-.7606
.50	.07	-.7858
.55	.06	-.7992
.60	.06	-.7924
.65	.05	-.7481
.70	.05	-.4562
.75	.04	-.3269
.80	.03	-.2623
.85	.03	-.1920
.90	.02	-.1169
0.00	.03	.5382
.05	.01	.0172
.10	.01	-.0129
.15	.00	-.0201
.20	-.00	-.0322
.25	-.00	-.0873
.30	-.01	-.0936
.35	-.01	-.0956
.40	-.01	-.1035
.45	-.01	-.1213
.50	-.01	-.1222
.55	-.01	-.1061
.60	-.01	-.0965
.65	-.01	-.0743
.70	-.00	-.0475
.75	-.00	-.0210
.80	-.00	.0094
.85	.00	.0456
.90	.00	.0728

X/C	Z/C	CP
0.00	.01	.5751
.05	.03	-.6381
.10	.04	-.7409
.15	.05	-.8167
.20	.06	-.8401
.25	.06	-.8658
.30	.07	-.9192
.35	.07	-.9506
.40	.07	-1.0068
.45	.07	-1.0669
.50	.07	-1.0842
.55	.06	-1.0664
.60	.06	-.7163
.65	.05	-.7471
.70	.05	-.5491
.75	.04	-.4391
.80	.04	-.2329
.85	.03	-.1867
0.00	.01	.1003
.04	-.00	.0990
.09	-.01	.0508
.14	-.01	.0493
.19	-.01	.0403
.24	-.01	.0114
.29	-.01	.0015
.34	-.01	-.0037
.39	-.01	-.0139
.44	-.01	-.0062
.49	-.01	.0113
.54	-.01	.0294
.59	-.01	.0453
.64	-.00	.0386
.69	-.00	.0946
.74	.00	.0968
.79	.00	.1044
.84	.00	.1255

X/C	Z/C	CP
0.00	-.01	.1518
.11	.03	-.2594
.20	.05	-.7531
.31	.06	-.8162
.40	.07	-1.0719
.51	.06	-1.0590
.61	.06	-.7447
.71	.05	-.5462
0.00	-.01	-.4206
.11	-.02	-.0199
.21	-.02	.0133
.31	-.02	.0147
.40	-.02	.0151
.51	-.01	.0211
.61	-.01	.0361
.71	-.00	.0564

X/C	Z/C	CP
.11	.01	-.9322
.21	.00	-.7783
.31	.00	-1.0803
.41	.01	-.9001
.51	.01	-.6548
.62	.01	-.5510
.71	.00	-.4723
.11	-.05	.1434
.22	-.04	.1039
.32	-.03	.0775
.42	-.03	.0545
.51	-.02	.0601
.62	-.01	.0659
.72	-.00	.0910

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17093

MACH .805

Q 30208.1

ALPW

3.94

BETA

0.00

P1 66512.63

PT1 101942.36

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5695	0.00	.01	.4512	0.00	-.01	.1504	.11	.01	-1.0553
.05	.05	-.6066	.05	.03	-.8098	.11	.03	-.4994	.21	.00	-.8381
.10	.06	-.6648	.10	.04	-.9113	.20	.05	-.8966	.31	.00	-1.0600
.15	.06	-.6631	.15	.05	-.9845	.31	.06	-.9387	.41	.01	-.7904
.20	.07	-.6669	.20	.06	-1.0003	.40	.07	-1.0630	.51	.01	-.6524
.25	.07	-.7052	.25	.06	-1.0271	.51	.06	-1.0404	.62	.01	-.5616
.30	.07	-.7371	.30	.07	-1.0345	.61	.06	-.7577	.71	.00	-.4781
.35	.07	-.7643	.35	.07	-1.0361	.71	.05	-.5262	.11	-.05	.1898
.40	.07	-.7985	.40	.07	-1.0936	0.00	-.01	-.7294	.22	-.04	.1293
.45	.07	-.8139	.45	.07	-1.1408	.11	-.02	-.0231	.32	-.03	.0908
.50	.07	-.8229	.50	.07	-1.1172	.21	-.02	.0071	.42	-.03	.0693
.55	.06	-.8430	.55	.06	-.8719	.31	-.02	.0083	.51	-.02	.0699
.60	.06	-.8472	.60	.06	-.6757	.40	-.02	.0161	.62	-.01	.0654
.65	.05	-.8615	.65	.05	-.6651	.51	-.01	.0168	.72	-.00	.0860
.70	.05	-.5808	.70	.05	-.5810	.61	-.01	.0348			
.75	.04	-.3446	.75	.04	-.4850	.71	-.00	.0468			
.80	.03	-.2632	.80	.04	-.2886						
.85	.03	-.1914	.85	.03	-.2035						
.90	.02	-.1134	0.00	.01	.1132						
0.00	.03	.4336	.04	-.00	.0997						
.05	.01	.1062	.09	-.01	.1343						
.10	.01	.0555	.14	-.01	.1003						
.15	.00	.0241	.19	-.01	.1024						
.20	-.00	.0233	.24	-.01	.0573						
.25	-.00	-.0269	.29	-.01	.0425						
.30	-.01	-.0260	.34	-.01	.0365						
.35	-.01	-.0397	.39	-.01	.0205						
.40	-.01	-.0528	.44	-.01	.0258						
.45	-.01	-.0720	.49	-.01	.0385						
.50	-.01	-.0697	.54	-.01	.0466						
.55	-.01	-.0708	.59	-.01	.0718						
.60	-.01	-.0683	.64	-.00	.0712						
.65	-.01	-.0494	.69	-.00	.1098						
.70	-.00	-.0291	.74	.00	.1124						
.75	-.00	-.0033	.79	.00	.1167						
.80	-.00	.0281	.84	.00	.1415						
.85	.00	.0596									
.90	.00	.0857									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17094

MACH .807

Q

30257.8

ALPW

5.88

BETA

0.00

P1 66436.56

PT1 101939.88

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4283
.05	.05	-.9017
.10	.06	-.8783
.15	.06	-.9050
.20	.07	-.7639
.25	.07	-.8194
.30	.07	-.8805
.35	.07	-.9051
.40	.07	-.9183
.45	.07	-.9613
.50	.07	-.9780
.55	.06	-.9334
.60	.06	-.9190
.65	.05	-.9212
.70	.05	-.6147
.75	.04	-.4167
.80	.03	-.3155
.85	.03	-.2224
.90	.02	-.1562
0.00	.03	.1769
.05	.01	.2347
.10	.01	.1641
.15	.00	.1175
.20	-.00	.0932
.25	-.00	.0408
.30	-.01	.0399
.35	-.01	.0330
.40	-.01	.0145
.45	-.01	-.0119
.50	-.01	-.0212
.55	-.01	-.0198
.60	-.01	-.0158
.65	-.01	-.0096
.70	-.00	.0103
.75	-.00	.0341
.80	-.00	.0425
.85	.00	.0652
.90	.00	.0883

X/C	Z/C	CP
0.00	.01	.2243
.05	.03	-1.2712
.10	.04	-1.2483
.15	.05	-1.2546
.20	.06	-1.2639
.25	.06	-1.2458
.30	.07	-1.2207
.35	.07	-1.1583
.40	.07	-1.0558
.45	.07	-.8834
.50	.07	-.6657
.55	.06	-.5684
.60	.06	-.4884
.65	.05	-.5412
.70	.05	-.4713
.75	.04	-.4207
.80	.04	-.2968
.85	.03	-.2561
0.00	.01	.0979
.04	-.00	.0611
.09	-.01	.2343
.14	-.01	.1853
.19	-.01	.1834
.24	-.01	.1167
.29	-.01	.0941
.34	-.01	.0682
.39	-.01	.0540
.44	-.01	.0551
.49	-.01	.0494
.54	-.01	.0615
.59	-.01	.0692
.64	-.00	.0706
.69	-.00	.0942
.74	.00	.0900
.79	.00	.1121
.84	.00	.1174

X/C	Z/C	CP
0.00	-.01	.1248
.11	.03	-.6497
.20	.05	-.7272
.31	.06	-.8518
.40	.07	-.8003
.51	.06	-.7115
.61	.06	-.5365
.71	.05	-.4948
0.00	-.01	-1.0832
.11	-.02	-.0413
.21	-.02	-.0039
.31	-.02	-.0036
.40	-.02	-.0224
.51	-.01	-.0104
.61	-.01	.0125
.71	-.00	.0177

X/C	Z/C	CP
.11	.01	-1.0887
.21	.00	-.8840
.31	.00	-1.2144
.41	.01	-1.0869
.51	.01	-.7451
.62	.01	-.5375
.71	.00	-.3902
.11	-.05	.1861
.22	-.04	.1122
.32	-.03	.0897
.42	-.03	.0645
.51	-.02	.0622
.62	-.01	.0616
.72	-.00	.0856

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 15

TP 17095

MACH .806

Q 30243.8

ALPH

-.00

BETA

0.00

P1 66440.03

PT1 101924.35

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5108	0.00	.01	.6084	0.00	-.01	.1117	.11	.01	-.3736
.05	.05	-.1105	.05	.03	-.0878	.11	.03	.0827	.21	.00	-.7578
.10	.06	-.2315	.10	.04	-.2809	.20	.05	-.1949	.31	.00	-.8360
.15	.06	-.3010	.15	.05	-.3797	.31	.06	-.3185	.41	.01	-.9780
.20	.07	-.3610	.20	.06	-.4378	.40	.07	-.5980	.51	.01	-1.0346
.25	.07	-.4043	.25	.06	-.4940	.51	.06	-.9018	.62	.01	-.7780
.30	.07	-.4482	.30	.07	-.5656	.61	.06	-.7723	.71	.00	-.4076
.35	.07	-.4915	.35	.07	-.5982	.71	.05	-.3991	.11	-.05	-.0492
.40	.07	-.5230	.40	.07	-.6527	0.00	-.01	.0870	.22	-.04	-.0348
.45	.07	-.5798	.45	.07	-.6279	.11	-.02	-.2159	.32	-.03	-.0120
.50	.07	-.5544	.50	.07	-.6254	.21	-.02	-.0489	.42	-.03	.0096
.55	.06	-.5212	.55	.06	-.5727	.31	-.02	-.0485	.51	-.02	.0321
.60	.06	-.4769	.60	.06	-.4733	.40	-.02	-.0532	.62	-.01	.0809
.65	.05	-.4147	.65	.05	-.4723	.51	-.01	-.0344	.72	-.00	.1303
.70	.05	-.3524	.70	.05	-.4391	.61	-.01	.0151			
.75	.04	-.3094	.75	.04	-.4024	.71	-.00	.0666			
.80	.03	-.2508	.80	.04	-.2498						
.85	.03	-.1860	.85	.03	-.1969						
.90	.02	-.1133	0.00	.01	.3786						
0.00	.03	.6075	.04	-.00	.0635						
.05	.01	-.3131	.09	-.01	-.2315						
.10	.01	-.2436	.14	-.01	-.1961						
.15	.00	-.2311	.19	-.01	-.2027						
.20	-.00	-.2294	.24	-.01	-.1629						
.25	-.00	-.2273	.29	-.01	-.1569						
.30	-.01	-.2284	.34	-.01	-.1450						
.35	-.01	-.2269	.39	-.01	-.1373						
.40	-.01	-.2293	.44	-.01	-.1124						
.45	-.01	-.2268	.49	-.01	-.0896						
.50	-.01	-.2264	.54	-.01	-.0595						
.55	-.01	-.2075	.59	-.01	-.0197						
.60	-.01	-.1854	.64	-.00	-.0179						
.65	-.01	-.1577	.69	-.00	.0309						
.70	-.00	-.1192	.74	.00	.0344						
.75	-.00	-.0836	.79	.00	.0668						
.80	-.00	-.0432	.84	.00	.0846						
.85	.00	-.0039									
.90	.00	.0492									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17112

MACH .754

Q 27775.0

ALPW

-1.96

BETA

0.00

P1 69716.99

PT1 101671.55

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/8/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.1882
.05	.05	.0832
.10	.06	-.0750
.15	.06	-.1458
.20	.07	-.2096
.25	.07	-.2720
.30	.07	-.3035
.35	.07	-.3343
.40	.07	-.3798
.45	.07	-.3902
.50	.07	-.3844
.55	.06	-.3605
.60	.06	-.3360
.65	.05	-.3120
.70	.05	-.2706
.75	.04	-.2354
.80	.03	-.2029
.85	.03	-.1571
.90	.02	-.1012
0.00	.03	.4557
.05	.01	-.5020
.10	.01	-.3879
.15	.00	-.3388
.20	-.00	-.3219
.25	-.00	-.3204
.30	-.01	-.3201
.35	-.01	-.3116
.40	-.01	-.2993
.45	-.01	-.2744
.50	-.01	-.2739
.55	-.01	-.2574
.60	-.01	-.2287
.65	-.01	-.1874
.70	-.00	-.1470
.75	-.00	-.0382
.80	-.00	-.0369
.85	.00	-.0095
.90	.00	.0850

X/C	Z/C	CP
0.00	.01	.3709
.05	.03	.1499
.10	.04	-.0423
.15	.05	-.1488
.20	.06	-.2217
.25	.06	-.2779
.30	.07	-.3331
.35	.07	-.3807
.40	.07	-.4211
.45	.07	-.4299
.50	.07	-.4177
.55	.06	-.3916
.60	.06	-.3719
.65	.05	-.3794
.70	.05	-.3507
.75	.04	-.3192
.80	.04	-.2127
.85	.03	-.2142
0.00	.01	.3978
.04	-.00	.0303
.09	-.01	-.6265
.14	-.01	-.4787
.19	-.01	-.3659
.24	-.01	-.3062
.29	-.01	-.2575
.34	-.01	-.2353
.39	-.01	-.2129
.44	-.01	-.1807
.49	-.01	-.1386
.54	-.01	-.1075
.59	-.01	-.0733
.64	-.00	-.0779
.69	-.00	.0011
.74	.00	.0129
.79	.00	.0284
.84	.00	.0504

X/C	Z/C	CP
0.00	-.01	.0757
.11	.03	.0115
.20	.05	-.2521
.31	.06	-.3776
.40	.07	-.5492
.51	.06	-.5775
.61	.06	-.4874
.71	.05	-.3585
0.00	-.01	.1103
.11	-.02	-.4377
.21	-.02	.7429
.31	-.02	.7471
.40	-.02	-.3170
.51	-.01	-.1679
.61	-.01	-.0449
.71	-.00	.0417

X/C	Z/C	CP
.11	.01	-.1411
.21	.00	-.2533
.31	.00	-.6000
.41	.01	-.6662
.51	.01	-.6463
.62	.01	-.5395
.71	.00	-.3939
.11	-.05	-.6800
.22	-.04	-.5191
.32	-.03	-.3495
.42	-.03	-.1408
.51	-.02	-.0308
.62	-.01	.0669
.72	-.00	.1292

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17113

MACH .753

Q 27725.7

ALPW

-1.45

BETA

0.00

P1 69783.06

PT1 101668.94

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.2872	0.00	.01	.4359	0.00	-.01	.0904	.11	.01	-.2033
.05	.05	.0361	.05	.03	.0960	.11	.03	.0491	.21	.00	-.3018
.10	.06	-.1198	.10	.04	-.0995	.20	.05	-.1623	.31	.00	-.6563
.15	.06	-.1963	.15	.05	-.1956	.31	.06	-.3304	.41	.01	-.7057
.20	.07	-.2429	.20	.06	-.2657	.40	.07	-.5961	.51	.01	-.6697
.25	.07	-.3041	.25	.06	-.3215	.51	.06	-.6225	.62	.01	-.5464
.30	.07	-.3505	.30	.07	-.3708	.61	.06	-.5095	.71	.00	-.3971
.35	.07	-.3636	.35	.07	-.4204	.71	.05	-.3684	.11	-.05	-.6121
.40	.07	-.4088	.40	.07	-.4554	0.00	-.01	.1181	.22	-.04	-.3882
.45	.07	-.4088	.45	.07	-.4562	.11	-.02	-.3851	.32	-.03	-.2038
.50	.07	-.4022	.50	.07	-.4478	.21	-.02	.4596	.42	-.03	-.0613
.55	.06	-.3862	.55	.06	-.4416	.31	-.02	.4710	.51	-.02	-.0075
.60	.06	-.3517	.60	.06	-.3902	.40	-.02	-.1962	.62	-.01	.0592
.65	.05	-.3266	.65	.05	-.3907	.51	-.01	-.1075	.72	-.00	.1255
.70	.05	-.2849	.70	.05	-.3694	.61	-.01	-.0056			
.75	.04	-.2494	.75	.04	-.3390	.71	-.00	.0576			
.80	.03	-.2061	.80	.04	-.2169						
.85	.03	-.1661	.85	.03	-.2165						
.90	.02	-.1043	0.00	.01	.4406						
0.00	.03	.5185	.04	-.00	.0296						
.05	.01	-.4620	.09	-.01	-.4584						
.10	.01	-.3278	.14	-.01	-.3506						
.15	.00	-.3050	.19	-.01	-.2895						
.20	-.00	-.2964	.24	-.01	-.2573						
.25	-.00	-.2990	.29	-.01	-.2174						
.30	-.01	-.2947	.34	-.01	-.2030						
.35	-.01	-.2871	.39	-.01	-.1892						
.40	-.01	-.2872	.44	-.01	-.1564						
.45	-.01	-.2816	.49	-.01	-.1260						
.50	-.01	-.2657	.54	-.01	-.0917						
.55	-.01	-.2430	.59	-.01	-.0577						
.60	-.01	-.2181	.64	-.00	-.0562						
.65	-.01	-.1779	.69	-.00	.0157						
.70	-.00	-.1361	.74	.00	.0078						
.75	-.00	-.0978	.79	.00	.0383						
.80	-.00	-.0562	.84	.00	.0667						
.85	.00	-.0193									
.90	.00	.0756									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17114

MACH .753

Q 27711.4

ALPW

-.92

BETA

0.00

P1 69795.55

PT1 101661.88

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.3872
.05	.05	-.0148
.10	.06	-.1692
.15	.06	-.2274
.20	.07	-.2824
.25	.07	-.3346
.30	.07	-.3757
.35	.07	-.4058
.40	.07	-.4372
.45	.07	-.4444
.50	.07	-.4297
.55	.06	-.4055
.60	.06	-.3773
.65	.05	-.3394
.70	.05	-.2940
.75	.04	-.2618
.80	.03	-.2160
.85	.03	-.1696
.90	.02	-.1081
0.00	.03	.5619
.05	.01	-.4040
.10	.01	-.2887
.15	.00	-.2612
.20	-.00	-.2564
.25	-.00	-.2474
.30	-.01	-.2446
.35	-.01	-.2452
.40	-.01	-.2458
.45	-.01	-.2503
.50	-.01	-.2382
.55	-.01	-.2176
.60	-.01	-.1867
.65	-.01	-.1564
.70	-.00	-.1222
.75	-.00	-.0828
.80	-.00	-.0454
.85	.00	.0004
.90	.00	.0696

X/C	Z/C	CP
0.00	.01	.5204
.05	.03	.0301
.10	.04	-.1605
.15	.05	-.2527
.20	.06	-.3188
.25	.06	-.3741
.30	.07	-.4253
.35	.07	-.4680
.40	.07	-.4896
.45	.07	-.5003
.50	.07	-.4694
.55	.06	-.4402
.60	.06	-.4087
.65	.05	-.4085
.70	.05	-.3827
.75	.04	-.3443
.80	.04	-.2301
.85	.03	-.2272
0.00	.01	.5147
.04	-.00	.0241
.09	-.01	-.3161
.14	-.01	-.2739
.19	-.01	-.2454
.24	-.01	-.2164
.29	-.01	-.1961
.34	-.01	-.1822
.39	-.01	-.1663
.44	-.01	-.1451
.49	-.01	-.1065
.54	-.01	-.0767
.59	-.01	-.0418
.64	-.00	-.0416
.69	-.00	.0210
.74	.00	.0273
.79	.00	.0468
.84	.00	.0731

X/C	Z/C	CP
0.00	-.01	.0997
.11	.03	.0713
.20	.05	-.1246
.31	.06	-.3588
.40	.07	-.6227
.51	.06	-.6803
.61	.06	-.5331
.71	.05	-.3800
0.00	-.01	.1240
.11	-.02	-.3431
.21	-.02	.2386
.31	-.02	.2679
.40	-.02	-.0825
.51	-.01	-.0872
.61	-.01	.0077
.71	-.00	.0609

X/C	Z/C	CP
.11	.01	-.2882
.21	.00	-.3586
.31	.00	-.7199
.41	.01	-.7587
.51	.01	-.7175
.62	.01	-.5614
.71	.00	-.4108
.11	-.05	-.5025
.22	-.04	-.1714
.32	-.03	-.0687
.42	-.03	-.0222
.51	-.02	.0095
.62	-.01	.0601
.72	-.00	.1156

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17115

MACH .755

Q 27778.9

ALPW

-.52

BETA

0.00

P1 69702.80

PT1 101663.34

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4469
.05	.05	-.0600
.10	.06	-.2061
.15	.06	-.2732
.20	.07	-.3134
.25	.07	-.3568
.30	.07	-.3993
.35	.07	-.4315
.40	.07	-.4552
.45	.07	-.4605
.50	.07	-.4456
.55	.06	-.4235
.60	.06	-.3908
.65	.05	-.3567
.70	.05	-.3064
.75	.04	-.2734
.80	.03	-.2202
.85	.03	-.1697
.90	.02	-.1147
0.00	.03	.5859
.05	.01	-.3447
.10	.01	-.2626
.15	.00	-.2335
.20	-.00	-.2341
.25	-.00	-.2329
.30	-.01	-.2318
.35	-.01	-.2337
.40	-.01	-.2309
.45	-.01	-.2280
.50	-.01	-.2324
.55	-.01	-.2056
.60	-.01	-.1843
.65	-.01	-.1445
.70	-.00	-.1101
.75	-.00	-.0651
.80	-.00	-.0356
.85	.00	.0017
.90	.00	.0484

X/C	Z/C	CP
0.00	.01	.5678
.05	.03	-.0239
.10	.04	-.2199
.15	.05	-.2999
.20	.06	-.3599
.25	.06	-.4173
.30	.07	-.4614
.35	.07	-.5041
.40	.07	-.5211
.45	.07	-.5287
.50	.07	-.5058
.55	.06	-.4648
.60	.06	-.4249
.65	.05	-.4241
.70	.05	-.3964
.75	.04	-.3594
.80	.04	-.2343
.85	.03	-.2339
0.00	.01	.5270
.04	-.00	.0464
.09	-.01	-.2544
.14	-.01	-.2289
.19	-.01	-.2059
.24	-.01	-.1936
.29	-.01	-.1709
.34	-.01	-.1608
.39	-.01	-.1474
.44	-.01	-.1297
.49	-.01	-.0985
.54	-.01	-.0627
.59	-.01	-.0318
.64	-.00	-.0305
.69	-.00	.0301
.74	.00	.0341
.79	.00	.0579
.84	.00	.0780

X/C	Z/C	CP
0.00	-.01	.1075
.11	.03	.0836
.20	.05	-.1406
.31	.06	-.3895
.40	.07	-.6791
.51	.06	-.7202
.61	.06	-.5465
.71	.05	-.3922
0.00	-.01	.1208
.11	-.02	-.2790
.21	-.02	.1254
.31	-.02	.1423
.40	-.02	-.0622
.51	-.01	-.0633
.61	-.01	.0100
.71	-.00	.0578

X/C	Z/C	CP
.11	.01	-.3461
.21	.00	-.4063
.31	.00	-.7901
.41	.01	-.7942
.51	.01	-.7395
.62	.01	-.5690
.71	.00	-.4171
.11	-.05	-.2600
.22	-.04	-.0666
.32	-.03	-.0374
.42	-.03	-.0071
.51	-.02	.0184
.62	-.01	.0594
.72	-.00	.1164

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17117

MACH .754

Q

27764.9

ALPW

-.06

BETA

0.00

P1 69728.02

PT1 101668.63

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5001
.05	.05	-.1219
.10	.06	-.2480
.15	.06	-.3028
.20	.07	-.3485
.25	.07	-.3959
.30	.07	-.4345
.35	.07	-.4542
.40	.07	-.4843
.45	.07	-.4889
.50	.07	-.4689
.55	.06	-.4392
.60	.06	-.4058
.65	.05	-.3655
.70	.05	-.3223
.75	.04	-.2783
.80	.03	-.2291
.85	.03	-.1751
.90	.02	-.1130
0.00	.03	.6028
.05	.01	-.2979
.10	.01	-.2310
.15	.00	-.2355
.20	-.00	-.2137
.25	-.00	-.2046
.30	-.01	-.2049
.35	-.01	-.2048
.40	-.01	-.2063
.45	-.01	-.2038
.50	-.01	-.2032
.55	-.01	-.1806
.60	-.01	-.1583
.65	-.01	-.1297
.70	-.00	-.1044
.75	-.00	-.0692
.80	-.00	-.0302
.85	.00	.0103
.90	.00	.0689

X/C	Z/C	CP
0.00	.01	.6104
.05	.03	-.1023
.10	.04	-.2758
.15	.05	-.3625
.20	.06	-.4095
.25	.06	-.4581
.30	.07	-.5087
.35	.07	-.5404
.40	.07	-.5719
.45	.07	-.5564
.50	.07	-.5256
.55	.06	-.4956
.60	.06	-.4487
.65	.05	-.4530
.70	.05	-.4184
.75	.04	-.3748
.80	.04	-.2425
.85	.03	-.2243
0.00	.01	.4329
.04	-.00	.0942
.09	-.01	-.1491
.14	-.01	-.1930
.19	-.01	-.1840
.24	-.01	-.1537
.29	-.01	-.1470
.34	-.01	-.1410
.39	-.01	-.1322
.44	-.01	-.1102
.49	-.01	-.0810
.54	-.01	-.0560
.59	-.01	-.0243
.64	-.00	-.0260
.69	-.00	.0372
.74	.00	.0407
.79	.00	.0628
.84	.00	.0848

X/C	Z/C	CP
0.00	-.01	.1147
.11	.03	.0930
.20	.05	-.2019
.31	.06	-.4445
.40	.07	-.7076
.51	.06	-.7795
.61	.06	-.5649
.71	.05	-.3979
0.00	-.01	.1127
.11	-.02	-.2188
.21	-.02	-.0001
.31	-.02	.0003
.40	-.02	-.0520
.51	-.01	-.0503
.61	-.01	.0131
.71	-.00	.0628

X/C	Z/C	CP
.11	.01	-.4229
.21	.00	-.4799
.31	.00	-.8575
.41	.01	-.8984
.51	.01	-.8007
.62	.01	-.5314
.71	.00	-.4263
.11	-.05	-.0616
.22	-.04	-.0436
.32	-.03	-.0177
.42	-.03	.0058
.51	-.02	.0334
.62	-.01	.0737
.72	-.00	.1248

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP * 17118

MACH .755

Q 27805.0

ALPW

.50

BETA

0.00

P1 69668.40

PT1 101665.24

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5589
.05	.05	-.1792
.10	.06	-.3085
.15	.06	-.3501
.20	.07	-.3924
.25	.07	-.4427
.30	.07	-.4692
.35	.07	-.5021
.40	.07	-.5208
.45	.07	-.5155
.50	.07	-.4971
.55	.06	-.4657
.60	.06	-.4338
.65	.05	-.3866
.70	.05	-.3321
.75	.04	-.2957
.80	.03	-.2394
.85	.03	-.1842
.90	.02	-.1217
0.00	.03	.6154
.05	.01	-.2219
.10	.01	-.1846
.15	.00	-.1865
.20	-.00	-.1777
.25	-.00	-.1787
.30	-.01	-.1807
.35	-.01	-.1849
.40	-.01	-.1828
.45	-.01	-.1961
.50	-.01	-.1886
.55	-.01	-.1671
.60	-.01	-.1432
.65	-.01	-.1193
.70	-.00	-.0780
.75	-.00	-.0471
.80	-.00	-.0128
.85	.00	.0215
.90	.00	.0520

X/C	Z/C	CP
0.00	.01	.6363
.05	.03	-.1914
.10	.04	-.3544
.15	.05	-.4291
.20	.06	-.4724
.25	.06	-.5245
.30	.07	-.5690
.35	.07	-.5989
.40	.07	-.6216
.45	.07	-.6129
.50	.07	-.5643
.55	.06	-.5244
.60	.06	-.4776
.65	.05	-.4720
.70	.05	-.4382
.75	.04	-.3885
.80	.04	-.2496
.85	.03	-.2429
0.00	.01	.4323
.04	-.00	.0810
.09	-.01	-.1112
.14	-.01	-.1321
.19	-.01	-.1353
.24	-.01	-.1185
.29	-.01	-.1135
.34	-.01	-.1109
.39	-.01	-.1028
.44	-.01	-.0882
.49	-.01	-.0602
.54	-.01	-.0364
.59	-.01	-.0096
.64	-.00	-.0074
.69	-.00	.0519
.74	.00	.0597
.79	.00	.0695
.84	.00	.0942

X/C	Z/C	CP
0.00	-.01	.1214
.11	.03	.0904
.20	.05	-.2559
.31	.06	-.5038
.40	.07	-.8421
.51	.06	-.8767
.61	.06	-.5916
.71	.05	-.4140
0.00	-.01	.0824
.11	-.02	-.1326
.21	-.02	-.0246
.31	-.02	-.0205
.40	-.02	-.0441
.51	-.01	-.0330
.61	-.01	.0179
.71	-.00	.0641

X/C	Z/C	CP
.11	.01	-.5274
.21	.00	-.6495
.31	.00	-.9405
.41	.01	-1.0049
.51	.01	-.8355
.62	.01	-.5909
.71	.00	-.4317
.11	-.05	-.0151
.22	-.04	-.0087
.32	-.03	.0069
.42	-.03	.0240
.51	-.02	.0436
.62	-.01	.0828
.72	-.00	.1337

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17119

MACH .755

Q 27802.5

ALPW

1.11

BETA

0.00

P1 69678.72

PT1 101671.74

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5936
.05	.05	-.2640
.10	.06	-.3654
.15	.06	-.4106
.20	.07	-.4444
.25	.07	-.4901
.30	.07	-.5141
.35	.07	-.5407
.40	.07	-.5622
.45	.07	-.5665
.50	.07	-.5255
.55	.06	-.4976
.60	.06	-.4536
.65	.05	-.3992
.70	.05	-.3510
.75	.04	-.3045
.80	.03	-.2491
.85	.03	-.1859
.90	.02	-.1206
0.00	.03	.6148
.05	.01	-.1386
.10	.01	-.1515
.15	.00	-.1426
.20	-.00	-.1399
.25	-.00	-.1498
.30	-.01	-.1596
.35	-.01	-.1604
.40	-.01	-.1666
.45	-.01	-.1675
.50	-.01	-.1684
.55	-.01	-.1487
.60	-.01	-.1232
.65	-.01	-.0993
.70	-.00	-.0713
.75	-.00	-.0434
.80	-.00	-.0090
.85	.00	.0279
.90	.00	.0606

X/C	Z/C	CP
0.00	.01	.6419
.05	.03	-.3124
.10	.04	-.4509
.15	.05	-.5150
.20	.06	-.5495
.25	.06	-.5949
.30	.07	-.6294
.35	.07	-.6564
.40	.07	-.6780
.45	.07	-.6575
.50	.07	-.6061
.55	.06	-.5573
.60	.06	-.5009
.65	.05	-.5056
.70	.05	-.4660
.75	.04	-.4183
.80	.04	-.2637
.85	.03	-.2588
0.00	.01	.0923
.04	-.00	.1280
.09	-.01	-.0136
.14	-.01	-.0825
.19	-.01	-.0919
.24	-.01	-.0854
.29	-.01	-.0784
.34	-.01	-.0791
.39	-.01	-.0777
.44	-.01	-.0636
.49	-.01	-.0379
.54	-.01	-.0154
.59	-.01	.0069
.64	-.00	.0013
.69	-.00	.0610
.74	.00	.0622
.79	.00	.0857
.84	.00	.0998

X/C	Z/C	CP
0.00	-.01	.1283
.11	.03	.0710
.20	.05	-.3229
.31	.06	-.5821
.40	.07	-.8292
.51	.06	-1.0604
.61	.06	-.6119
.71	.05	-.4192
0.00	-.01	.0370
.11	-.02	-.0467
.21	-.02	-.0218
.31	-.02	-.0206
.40	-.02	-.0187
.51	-.01	-.0192
.61	-.01	-.0056
.71	-.00	.0714

X/C	Z/C	CP
.11	.01	-.6153
.21	.00	-.7694
.31	.00	-1.1088
.41	.01	-1.1186
.51	.01	-.8330
.62	.01	-.5749
.71	.00	-.4247
.11	-.05	.0543
.22	-.04	.0290
.32	-.03	.0376
.42	-.03	.0429
.51	-.02	.0609
.62	-.01	.0928
.72	-.00	.1445

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17120

MACH .754

Q 27765.3

ALPW

1.53

BETA

0.00

P1 69725.93

PT1 101667.16

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6132	0.00	.01	.6332	0.00	-.01	.1344	.11	.01	-.6867
.05	.05	-.3093	.05	.03	-.3847	.11	.03	.0394	.21	.00	-.8347
.10	.06	-.4124	.10	.04	-.5250	.20	.05	-.3699	.31	.00	-1.1986
.15	.06	-.4460	.15	.05	-.5849	.31	.06	-.6336	.41	.01	-1.1968
.20	.07	-.4797	.20	.06	-.6020	.40	.07	-.8801	.51	.01	-.8796
.25	.07	-.5144	.25	.06	-.6425	.51	.06	-1.1175	.62	.01	-.5631
.30	.07	-.5467	.30	.07	-.6881	.61	.06	-.6452	.71	.00	-.4150
.35	.07	-.5657	.35	.07	-.6877	.71	.05	-.4245	.11	-.05	.0591
.40	.07	-.5885	.40	.07	-.7117	0.00	-.01	-.0158	.22	-.04	.0380
.45	.07	-.5921	.45	.07	-.6915	.11	-.02	-.0387	.32	-.03	.0408
.50	.07	-.5559	.50	.07	-.6283	.21	-.02	-.0194	.42	-.03	.0441
.55	.06	-.5127	.55	.06	-.5667	.31	-.02	-.0163	.51	-.02	.0632
.60	.06	-.4598	.60	.06	-.5113	.40	-.02	-.0048	.62	-.01	.0963
.65	.05	-.4131	.65	.05	-.5057	.51	-.01	-.0003	.72	-.00	.1487
.70	.05	-.3508	.70	.05	-.4713	.61	-.01	.0324			
.75	.04	-.3057	.75	.04	-.4267	.71	-.00	.0742			
.80	.03	-.2512	.80	.04	-.2659						
.85	.03	-.1928	.85	.03	-.2584						
.90	.02	-.1200	0.00	.01	.3431						
0.00	.03	.6082	.04	-.00	.0827						
.05	.01	-.1071	.09	-.01	-.0034						
.10	.01	-.0889	.14	-.01	-.0554						
.15	.00	-.0892	.19	-.01	-.0492						
.20	-.00	-.0976	.24	-.01	-.0516						
.25	-.00	-.1319	.29	-.01	-.0654						
.30	-.01	-.1277	.34	-.01	-.0622						
.35	-.01	-.1330	.39	-.01	-.0636						
.40	-.01	-.1466	.44	-.01	-.0501						
.45	-.01	-.1445	.49	-.01	-.0308						
.50	-.01	-.1467	.54	-.01	-.0082						
.55	-.01	-.1334	.59	-.01	.0153						
.60	-.01	-.1158	.64	-.00	.0183						
.65	-.01	-.0870	.69	-.00	.0750						
.70	-.00	-.0537	.74	.00	.0732						
.75	-.00	-.0337	.79	.00	.0970						
.80	-.00	-.0021	.84	.00	.1084						
.85	.00	.0349									
.90	.00	.0605									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17121

MACH .753

Q 27723.1

ALPW

2.02

BETA

0.00

P1 69782.56

PT1 101664.99

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6138
.05	.05	-.3819
.10	.06	-.4721
.15	.06	-.5029
.20	.07	-.5187
.25	.07	-.5568
.30	.07	-.5817
.35	.07	-.6003
.40	.07	-.6268
.45	.07	-.6137
.50	.07	-.5794
.55	.06	-.5390
.60	.06	-.4801
.65	.05	-.4286
.70	.05	-.3694
.75	.04	-.3135
.80	.03	-.2529
.85	.03	-.1976
.90	.02	-.1276
0.00	.03	.5819
.05	.01	-.0540
.10	.01	-.0471
.15	.00	-.0570
.20	-.00	-.0728
.25	-.00	-.1024
.30	-.01	-.1005
.35	-.01	-.1097
.40	-.01	-.1175
.45	-.01	-.1309
.50	-.01	-.1294
.55	-.01	-.1202
.60	-.01	-.0972
.65	-.01	-.0801
.70	-.00	-.0522
.75	-.00	-.0183
.80	-.00	.0123
.85	.00	.0373
.90	.00	.0671

X/C	Z/C	CP
0.00	.01	.6241
.05	.03	-.5093
.10	.04	-.6171
.15	.05	-.6522
.20	.06	-.6760
.25	.06	-.7039
.30	.07	-.7406
.35	.07	-.7356
.40	.07	-.7659
.45	.07	-.7432
.50	.07	-.6707
.55	.06	-.5854
.60	.06	-.5294
.65	.05	-.5274
.70	.05	-.4881
.75	.04	-.4324
.80	.04	-.2650
.85	.03	-.2573
0.00	.01	.0957
.04	-.00	.0717
.09	-.01	.0504
.14	-.01	-.0120
.19	-.01	-.0156
.24	-.01	-.0311
.29	-.01	-.0397
.34	-.01	-.0396
.39	-.01	-.0455
.44	-.01	-.0345
.49	-.01	-.0180
.54	-.01	.0067
.59	-.01	.0262
.64	-.00	.0308
.69	-.00	.0913
.74	.00	.0911
.79	.00	.1021
.84	.00	.1178

X/C	Z/C	CP
0.00	-.01	.1378
.11	.03	.0050
.20	.05	-.4426
.31	.06	-.7038
.40	.07	-.9010
.51	.06	-1.1859
.61	.06	-.6766
.71	.05	-.4483
0.00	-.01	-.0940
.11	-.02	-.0256
.21	-.02	-.0177
.31	-.02	-.0153
.40	-.02	.0073
.51	-.01	.0060
.61	-.01	.0380
.71	-.00	.0710

X/C	Z/C	CP
.11	.01	-.7602
.21	.00	-.9000
.31	.00	-1.2762
.41	.01	-1.2573
.51	.01	-.9507
.62	.01	-.5790
.71	.00	-.4047
.11	-.05	.0723
.22	-.04	.0689
.32	-.03	.0622
.42	-.03	.0588
.51	-.02	.0733
.62	-.01	.1009
.72	-.00	.1505

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17122

MACH .755

Q 27795.7

ALPW

2.52

BETA

0.00

P1 69676.97

PT1 101661.10

Y/B/2 = .21

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6067	0.00	.01	.5734	0.00	-.01	.1427	.11	.01	-.9061
.05	.05	-.4473	.05	.03	-.5905	.11	.03	-.0669	.21	.00	-.9507
.10	.06	-.5245	.10	.04	-.7158	.20	.05	-.5001	.31	.00	-1.3359
.15	.06	-.5416	.15	.05	-.7370	.31	.06	-.7860	.41	.01	-1.2535
.20	.07	-.5676	.20	.06	-.7556	.40	.07	-.9060	.51	.01	-.9494
.25	.07	-.5947	.25	.06	-.7740	.51	.06	-1.2433	.62	.01	-.6213
.30	.07	-.6118	.30	.07	-.7966	.61	.06	-.7430	.71	.00	-.4197
.35	.07	-.6406	.35	.07	-.8041	.71	.05	-.4653	.11	-.05	.1165
.40	.07	-.6616	.40	.07	-.8127	0.00	-.01	-.2118	.22	-.04	.0889
.45	.07	-.6610	.45	.07	-.7837	.11	-.02	-.0131	.32	-.03	.0782
.50	.07	-.6095	.50	.07	-.7109	.21	-.02	-.0065	.42	-.03	.0715
.55	.06	-.5624	.55	.06	-.6048	.31	-.02	-.0047	.51	-.02	.0812
.60	.06	-.4973	.60	.06	-.5448	.40	-.02	.0106	.62	-.01	.1061
.65	.05	-.4467	.65	.05	-.5466	.51	-.01	.0103	.72	-.00	.1519
.70	.05	-.3725	.70	.05	-.5093	.61	-.01	.0443			
.75	.04	-.3298	.75	.04	-.4514	.71	-.00	.0746			
.80	.03	-.2600	.80	.04	-.2742						
.85	.03	-.2016	.85	.03	-.2563						
.90	.02	-.1247	0.00	.01	.5184						
0.00	.03	.5497	.04	-.00	.0628						
.05	.01	-.0025	.09	-.01	.0626						
.10	.01	-.0295	.14	-.01	.0225						
.15	.00	-.0371	.19	-.01	.0167						
.20	-.00	-.0469	.24	-.01	.0009						
.25	-.00	-.0843	.29	-.01	-.0047						
.30	-.01	-.0823	.34	-.01	-.0192						
.35	-.01	-.0932	.39	-.01	-.0222						
.40	-.01	-.1025	.44	-.01	-.0186						
.45	-.01	-.1086	.49	-.01	.0036						
.50	-.01	-.1145	.54	-.01	.0152						
.55	-.01	-.1011	.59	-.01	.0388						
.60	-.01	-.0833	.64	-.00	.0398						
.65	-.01	-.0594	.69	-.00	.0895						
.70	-.00	-.0416	.74	.00	.0913						
.75	-.00	-.0199	.79	.00	.1065						
.80	-.00	.0108	.84	.00	.1191						
.85	.00	.0462									
.90	.00	.0788									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17123

MACH .754

Q 27751.5

ALPW

2.98

BETA

0.00

P1 69728.43

PT1 101651.53

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5949
.05	.05	-.5146
.10	.06	-.5724
.15	.06	-.5979
.20	.07	-.6027
.25	.07	-.6365
.30	.07	-.6459
.35	.07	-.6781
.40	.07	-.6916
.45	.07	-.7050
.50	.07	-.6492
.55	.06	-.5783
.60	.06	-.5183
.65	.05	-.4494
.70	.05	-.3865
.75	.04	-.3344
.80	.03	-.2625
.85	.03	-.2023
.90	.02	-.1255
0.00	.03	.5014
.05	.01	.0408
.10	.01	.0042
.15	.00	.0029
.20	-.00	-.0133
.25	-.00	-.0658
.30	-.01	-.0649
.35	-.01	-.0755
.40	-.01	-.0808
.45	-.01	-.0944
.50	-.01	-.0954
.55	-.01	-.0839
.60	-.01	-.0666
.65	-.01	-.0496
.70	-.00	-.0326
.75	-.00	-.0059
.80	-.00	.0178
.85	.00	.0515
.90	.00	.0799

X/C	Z/C	CP
0.00	.01	.5204
.05	.03	-.7075
.10	.04	-.7941
.15	.05	-.8004
.20	.06	-.8165
.25	.06	-.8445
.30	.07	-.8681
.35	.07	-.8630
.40	.07	-.8585
.45	.07	-.8090
.50	.07	-.7434
.55	.06	-.6110
.60	.06	-.5613
.65	.05	-.5618
.70	.05	-.5173
.75	.04	-.4610
.80	.04	-.2790
.85	.03	-.2627
0.00	.01	.1042
.04	-.00	.0736
.09	-.01	.0417
.14	-.01	.0660
.19	-.01	.0653
.24	-.01	.0251
.29	-.01	.0157
.34	-.01	.0030
.39	-.01	-.0011
.44	-.01	.0007
.49	-.01	.0154
.54	-.01	.0341
.59	-.01	.0470
.64	-.00	.0471
.69	-.00	.0969
.74	.00	.0997
.79	.00	.1118
.84	.00	.1255

X/C	Z/C	CP
0.00	-.01	.1485
.11	.03	-.1509
.20	.05	-.5709
.31	.06	-.8964
.40	.07	-.9730
.51	.06	-1.2742
.61	.06	-.7432
.71	.05	-.5048
0.00	-.01	-.3365
.11	-.02	-.0083
.21	-.02	-.0030
.31	-.02	-.0040
.40	-.02	.0162
.51	-.01	.0257
.61	-.01	.0467
.71	-.00	.0726

X/C	Z/C	CP
.11	.01	-1.0051
.21	.00	-.9983
.31	.00	-1.3330
.41	.01	-1.1806
.51	.01	-.8433
.62	.01	-.6070
.71	.00	-.4452
.11	-.05	.1493
.22	-.04	.1092
.32	-.03	.0907
.42	-.03	.0805
.51	-.02	.0863
.62	-.01	.1056
.72	-.00	.1434

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17124

MACH .754

Q . 27760.4

ALPW

4.03

BETA

0.00

P1 69709.67

PT1 101645.54

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5034
.05	.05	-.6769
.10	.06	-.7141
.15	.06	-.6989
.20	.07	-.6900
.25	.07	-.6990
.30	.07	-.7368
.35	.07	-.7537
.40	.07	-.7840
.45	.07	-.7750
.50	.07	-.7064
.55	.06	-.6220
.60	.06	-.5531
.65	.05	-.4793
.70	.05	-.4011
.75	.04	-.3419
.80	.03	-.2806
.85	.03	-.1997
.90	.02	-.1281
0.00	.03	.3257
.05	.01	.1313
.10	.01	.0767
.15	.00	.0513
.20	-.00	.0412
.25	-.00	-.0123
.30	-.01	-.0079
.35	-.01	-.0188
.40	-.01	-.0295
.45	-.01	-.0518
.50	-.01	-.0588
.55	-.01	-.0499
.60	-.01	-.0426
.65	-.01	-.0250
.70	-.00	-.0060
.75	-.00	.0208
.80	-.00	.0438
.85	.00	.0682
.90	.00	.0873

X/C	Z/C	CP
0.00	.01	.3364
.05	.03	-.9631
.10	.04	-.9995
.15	.05	-1.0573
.20	.06	-1.0097
.25	.06	-1.0109
.30	.07	-1.0144
.35	.07	-1.0479
.40	.07	-1.0353
.45	.07	-.9048
.50	.07	-.7009
.55	.06	-.6313
.60	.06	-.5674
.65	.05	-.5674
.70	.05	-.5226
.75	.04	-.4624
.80	.04	-.2737
.85	.03	-.2436
0.00	.01	.2348
.04	-.00	.0527
.09	-.01	.1735
.14	-.01	.1312
.19	-.01	.1341
.24	-.01	.0825
.29	-.01	.0618
.34	-.01	.0498
.39	-.01	.0357
.44	-.01	.0396
.49	-.01	.0449
.54	-.01	.0634
.59	-.01	.0740
.64	-.00	.0753
.69	-.00	.1133
.74	.00	.1158
.79	.00	.1221
.84	.00	.1351

X/C	Z/C	CP
0.00	-.01	.1502
.11	.03	-.4547
.20	.05	-.7616
.31	.06	-1.0561
.40	.07	-1.1427
.51	.06	-1.3377
.61	.06	-.7477
.71	.05	-.6028
0.00	-.01	-.7080
.11	-.02	-.0030
.21	-.02	-.0001
.31	-.02	-.0010
.40	-.02	.0176
.51	-.01	.0220
.61	-.01	.0493
.71	-.00	.0556

X/C	Z/C	CP
.11	.01	-1.1286
.21	.00	-1.0802
.31	.00	-1.0071
.41	.01	-.7942
.51	.01	-.6790
.62	.01	-.5780
.71	.00	-.4860
.11	-.05	.1979
.22	-.04	.1334
.32	-.03	.1073
.42	-.03	.0777
.51	-.02	.0770
.62	-.01	.0734
.72	-.00	.1019

7 X 10 HIGH SPEED TUNNEL

TP 17125

PT1 101645.89

$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.01	.0488
.05	.03	-1.5785
.10	.04	-1.5294
.15	.05	-1.4956
.20	.06	-1.4811
.25	.06	-1.4356
.30	.07	-1.4418
.35	.07	-1.3632
.40	.07	-1.3496
.45	.07	-1.2136
.50	.07	-.7537
.55	.06	-.4991
.60	.06	-.4392
.65	.05	-.4410
.70	.05	-.4067
.75	.04	-.3675
.80	.04	-.2211
.85	.03	-.1934
0.00	.01	.1178
.04	-.00	.0551
.09	-.01	.2757
.14	-.01	.2192
.19	-.01	.2209
.24	-.01	.1524
.29	-.01	.1287
.34	-.01	.1037
.39	-.01	.0879
.44	-.01	.0838
.49	-.01	.0916
.54	-.01	.0939
.59	-.01	.1013
.64	-.00	.1011
.69	-.00	.1286
.74	.00	.1234
.79	.00	.1355
.84	.00	.1476

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 16

TP 17126

MACH .754

Q 27734.4

ALPW

.07

BETA

0.00

P1 69742.72

PT1 101642.50

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5299
.05	.05	-.1322
.10	.06	-.2625
.15	.06	-.3169
.20	.07	-.3537
.25	.07	-.4069
.30	.07	-.4386
.35	.07	-.4677
.40	.07	-.4940
.45	.07	-.5000
.50	.07	-.4779
.55	.06	-.4484
.60	.06	-.4105
.65	.05	-.3742
.70	.05	-.3244
.75	.04	-.2889
.80	.03	-.2326
.85	.03	-.1767
.90	.02	-.1174
0.00	.03	.6127
.05	.01	-.2809
.10	.01	-.2184
.15	.00	-.2158
.20	-.00	-.2127
.25	-.00	-.2078
.30	-.01	-.2041
.35	-.01	-.2040
.40	-.01	-.2047
.45	-.01	-.2030
.50	-.01	-.2019
.55	-.01	-.1869
.60	-.01	-.1657
.65	-.01	-.1318
.70	-.00	-.1072
.75	-.00	-.0676
.80	-.00	-.0353
.85	.00	.0004
.90	.00	.0408

X/C	Z/C	CP
0.00	.01	.6203
.05	.03	-.1223
.10	.04	-.2902
.15	.05	-.3747
.20	.06	-.4291
.25	.06	-.4825
.30	.07	-.5236
.35	.07	-.5509
.40	.07	-.5776
.45	.07	-.5660
.50	.07	-.5363
.55	.06	-.4921
.60	.06	-.4542
.65	.05	-.4565
.70	.05	-.3758
.75	.04	-.3616
.80	.04	-.2462
.85	.03	-.1868
0.00	.01	.4313
.04	-.00	.0718
.09	-.01	-.1740
.14	-.01	-.1752
.19	-.01	-.1843
.24	-.01	-.1513
.29	-.01	-.1385
.34	-.01	-.1294
.39	-.01	-.1245
.44	-.01	-.1037
.49	-.01	-.0783
.54	-.01	-.0481
.59	-.01	-.0229
.64	-.00	-.0238
.69	-.00	.0395
.74	.00	.0406
.79	.00	.0611
.84	.00	.0854

X/C	Z/C	CP
0.00	-.01	.1082
.11	.03	.1053
.20	.05	-.1654
.31	.06	-.4247
.40	.07	-.7594
.51	.06	-.7861
.61	.06	-.5679
.71	.05	-.4051
0.00	-.01	.1080
.11	-.02	-.2071
.21	-.02	-.0509
.31	-.02	-.0521
.40	-.02	-.0522
.51	-.01	-.0352
.61	-.01	.0162
.71	-.00	.0627

X/C	Z/C	CP
.11	.01	-.4412
.21	.00	-.5146
.31	.00	-.8576
.41	.01	-.9215
.51	.01	-.7712
.62	.01	-.5846
.71	.00	-.4252
.11	-.05	-.0495
.22	-.04	-.0349
.32	-.03	-.0129
.42	-.03	.0085
.51	-.02	.0338
.62	-.01	.0749
.72	-.00	.1300

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN

17

TP 17131

MACH .703

Q

25301.1

ALPW

-2.00

BETA

0.00

P1 73054.98

PT1 101641.96

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.1547
.05	.05	.0803
.10	.06	-.0760
.15	.06	-.1510
.20	.07	-.2081
.25	.07	-.2541
.30	.07	-.2947
.35	.07	-.3202
.40	.07	-.3502
.45	.07	-.3641
.50	.07	-.3501
.55	.06	-.3359
.60	.06	-.3166
.65	.05	-.2847
.70	.05	-.2484
.75	.04	-.2297
.80	.03	-.1896
.85	.03	-.1495
.90	.02	-.0995
0.00	.03	.4367
.05	.01	-.4948
.10	.01	-.3694
.15	.00	-.3272
.20	-.00	-.3066
.25	-.00	-.2962
.30	-.01	-.2933
.35	-.01	-.2855
.40	-.01	-.2869
.45	-.01	-.2855
.50	-.01	-.2712
.55	-.01	-.2499
.60	-.01	-.2238
.65	-.01	-.1914
.70	-.00	-.1522
.75	-.00	-.1135
.80	-.00	-.0723
.85	.00	-.0357
.90	.00	.0518

X/C	Z/C	CP
0.00	.01	.3283
.05	.03	.1532
.10	.04	-.0358
.15	.05	-.1438
.20	.06	-.2112
.25	.06	-.2598
.30	.07	-.3216
.35	.07	-.3578
.40	.07	-.3887
.45	.07	-.3939
.50	.07	-.3870
.55	.06	-.3636
.60	.06	-.3401
.65	.05	-.3410
.70	.05	-.2940
.75	.04	-.2874
.80	.04	-.2045
.85	.03	-.1646
0.00	.01	.2271
.04	-.00	.0352
.09	-.01	-.5608
.14	-.01	-.4093
.19	-.01	-.3774
.24	-.01	-.2845
.29	-.01	-.2527
.34	-.01	-.2252
.39	-.01	-.2032
.44	-.01	-.1730
.49	-.01	-.1409
.54	-.01	-.1043
.59	-.01	-.0694
.64	-.00	-.0543
.69	-.00	.0001
.74	.00	.0008
.79	.00	.0194
.84	.00	.0424

X/C	Z/C	CP
0.00	-.01	.0678
.11	.03	.0017
.20	.05	-.0970
.31	.06	-.2404
.40	.07	-.5254
.51	.06	-.5331
.61	.06	-.4477
.71	.05	-.3444
0.00	-.01	.1109
.11	-.02	-.4460
.21	-.02	.4011
.31	-.02	.3994
.40	-.02	-.2849
.51	-.01	-.1213
.61	-.01	-.0124
.71	-.00	.0544

X/C	Z/C	CP
.11	.01	-.1445
.21	.00	-.2666
.31	.00	-.5555
.41	.01	-.6069
.51	.01	-.5853
.62	.01	-.5025
.71	.00	-.3871
.11	-.05	-.6398
.22	-.04	-.5115
.32	-.03	-.3419
.42	-.03	-.1574
.51	-.02	-.0446
.62	-.01	.0583
.72	-.00	.1167

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17132

MACH .703

Q 25286.9

ALPW

-1.48

BETA

0.00

P1 73068.85

PT1 101637.21

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.2837	0.00	.01	.4213	0.00	-.01	.0804	.11	.01	-.1984
.05	.05	.0330	.05	.03	.0968	.11	.03	.0411	.21	.00	-.3134
.10	.06	-.1185	.10	.04	-.0874	.20	.05	-.0614	.31	.00	-.5953
.15	.06	-.1926	.15	.05	-.1972	.31	.06	-.2550	.41	.01	-.6416
.20	.07	-.2415	.20	.06	-.2556	.40	.07	-.4653	.51	.01	-.6108
.25	.07	-.2949	.25	.06	-.3106	.51	.06	-.5610	.62	.01	-.5169
.30	.07	-.3299	.30	.07	-.3497	.61	.06	-.4673	.71	.00	-.3894
.35	.07	-.3529	.35	.07	-.3936	.71	.05	-.3529	.11	-.05	-.5781
.40	.07	-.3834	.40	.07	-.4182	0.00	-.01	.1227	.22	-.04	-.3927
.45	.07	-.3827	.45	.07	-.4239	.11	-.02	-.4094	.32	-.03	-.2114
.50	.07	-.3694	.50	.07	-.4106	.21	-.02	.2022	.42	-.03	-.0714
.55	.06	-.3534	.55	.06	-.3854	.31	-.02	.2018	.51	-.02	-.0150
.60	.06	-.3315	.60	.06	-.3749	.40	-.02	-.1306	.62	-.01	.0538
.65	.05	-.2976	.65	.05	-.3673	.51	-.01	-.0544	.72	-.00	.1166
.70	.05	-.2647	.70	.05	-.2991	.61	-.01	.0022			
.75	.04	-.2354	.75	.04	-.2897	.71	-.00	.0582			
.80	.03	-.1925	.80	.04	-.2104						
.85	.03	-.1572	.85	.03	-.1663						
.90	.02	-.1025	0.00	.01	.2171						
0.00	.03	.5006	.04	-.00	.0486						
.05	.01	-.4433	.09	-.01	-.4296						
.10	.01	-.3216	.14	-.01	-.3269						
.15	.00	-.2884	.19	-.01	-.2797						
.20	-.00	-.2722	.24	-.01	-.2490						
.25	-.00	-.2680	.29	-.01	-.2168						
.30	-.01	-.2621	.34	-.01	-.2019						
.35	-.01	-.2604	.39	-.01	-.1804						
.40	-.01	-.2589	.44	-.01	-.1572						
.45	-.01	-.2363	.49	-.01	-.1238						
.50	-.01	-.2352	.54	-.01	-.0883						
.55	-.01	-.2203	.59	-.01	-.0573						
.60	-.01	-.1943	.64	-.00	-.0482						
.65	-.01	-.1622	.69	-.00	.0094						
.70	-.00	-.1289	.74	.00	.0148						
.75	-.00	-.0930	.79	.00	.0336						
.80	-.00	-.0572	.84	.00	.0561						
.85	.00	-.0223									
.90	.00	.0256									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17133

MACH .704

Q 25322.4

ALPW

- 83

BETA

0.00

P1 73019.59

PT1 101635.34

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$
[illegible]

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17134

MACH .703

Q 25298.1

ALPW

-.52

BETA

0.00

P1 73051.24

PT1 101634.64

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.4494	0.00	.01	.5642	0.00	-.01	.0999	.11	.01	-.3453
.05	.05	-.0688	.05	.03	-.0296	.11	.03	.0979	.21	.00	-.4295
.10	.06	-.2080	.10	.04	-.2088	.20	.05	-.1066	.31	.00	-.7023
.15	.06	-.2636	.15	.05	-.2894	.31	.06	-.3419	.41	.01	-.7132
.20	.07	-.3072	.20	.06	-.3497	.40	.07	-.5812	.51	.01	-.6660
.25	.07	-.3510	.25	.06	-.3905	.51	.06	-.6372	.62	.01	-.5491
.30	.07	-.3872	.30	.07	-.4351	.61	.06	-.5039	.71	.00	-.4125
.35	.07	-.4124	.35	.07	-.4590	.71	.05	-.3809	.11	-.05	-.2291
.40	.07	-.4346	.40	.07	-.4896	0.00	-.01	.1236	.22	-.04	-.0728
.45	.07	-.4337	.45	.07	-.4846	.11	-.02	-.2846	.32	-.03	-.0429
.50	.07	-.4117	.50	.07	-.4588	.21	-.02	-.0140	.42	-.03	-.0137
.55	.06	-.3935	.55	.06	-.4283	.31	-.02	-.0120	.51	-.02	.0135
.60	.06	-.3644	.60	.06	-.4123	.40	-.02	-.0610	.62	-.01	.0613
.65	.05	-.3305	.65	.05	-.4011	.51	-.01	-.0468	.72	-.00	.1120
.70	.05	-.2879	.70	.05	-.3220	.61	-.01	.0086			
.75	.04	-.2555	.75	.04	-.2721	.71	-.00	.0558			
.80	.03	-.2131	.80	.04	-.2312						
.85	.03	-.1607	.85	.03	-.1787						
.90	.02	-.1114	0.00	.01	.4625						
0.00	.03	.5830	.04	-.00	.0481						
.05	.01	-.3377	.09	-.01	-.2759						
.10	.01	-.2498	.14	-.01	-.2186						
.15	.00	-.2200	.19	-.01	-.2167						
.20	-.00	-.2081	.24	-.01	-.1761						
.25	-.00	-.2137	.29	-.01	-.1634						
.30	-.01	-.2056	.34	-.01	-.1478						
.35	-.01	-.2052	.39	-.01	-.1460						
.40	-.01	-.2068	.44	-.01	-.1231						
.45	-.01	-.2094	.49	-.01	-.0899						
.50	-.01	-.2125	.54	-.01	-.0627						
.55	-.01	-.1903	.59	-.01	-.0330						
.60	-.01	-.1657	.64	-.00	-.0219						
.65	-.01	-.1440	.69	-.00	.0280						
.70	-.00	-.1112	.74	.00	.0280						
.75	-.00	-.0820	.79	.00	.0484						
.80	-.00	-.0464	.84	.00	.0701						
.85	.00	-.0091									
.90	.00	.0579									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17135

MACH .703

0

25279.9

ALPW

.04

BETA

0.00

P1 73071.66

PT1 101631.09

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5244
.05	.05	-.1371
.10	.06	-.2549
.15	.06	-.3116
.20	.07	-.3557
.25	.07	-.3877
.30	.07	-.4189
.35	.07	-.4382
.40	.07	-.4547
.45	.07	-.4563
.50	.07	-.4381
.55	.06	-.4110
.60	.06	-.3797
.65	.05	-.3427
.70	.05	-.3002
.75	.04	-.2657
.80	.03	-.2210
.85	.03	-.1663
.90	.02	-.1107
0.00	.03	.6042
.05	.01	-.2583
.10	.01	-.2161
.15	.00	-.1962
.20	-.00	-.1950
.25	-.00	-.1945
.30	-.01	-.1946
.35	-.01	-.1952
.40	-.01	-.1976
.45	-.01	-.1943
.50	-.01	-.1931
.55	-.01	-.1718
.60	-.01	-.1474
.65	-.01	-.1257
.70	-.00	-.0922
.75	-.00	-.0532
.80	-.00	-.0219
.85	.00	.0070
.90	.00	.0760

X/C	Z/C	CP
0.00	.01	.6185
.05	.03	-.1129
.10	.04	-.2833
.15	.05	-.3601
.20	.06	-.4002
.25	.06	-.4437
.30	.07	-.4805
.35	.07	-.5122
.40	.07	-.5266
.45	.07	-.5212
.50	.07	-.4944
.55	.06	-.4660
.60	.06	-.4342
.65	.05	-.4315
.70	.05	-.3321
.75	.04	-.3365
.80	.04	-.2397
.85	.03	-.1892
0.00	.01	.5565
.04	-.00	.0434
.09	-.01	-.1993
.14	-.01	-.1667
.19	-.01	-.1715
.24	-.01	-.1388
.29	-.01	-.1277
.34	-.01	-.1245
.39	-.01	-.1170
.44	-.01	-.1047
.49	-.01	-.0732
.54	-.01	-.0524
.59	-.01	-.0199
.64	-.00	-.0150
.69	-.00	.0398
.74	.00	.0373
.79	.00	.0558
.84	.00	.0791

X/C	Z/C	CP
0.00	-.01	.1038
.11	.03	.1014
.20	.05	-.1478
.31	.06	-.3966
.40	.07	-.6147
.51	.06	-.6830
.61	.06	-.5310
.71	.05	-.3925
0.00	-.01	.1166
.11	-.02	-.2031
.21	-.02	-.0615
.31	-.02	-.0595
.40	-.02	-.0513
.51	-.01	-.0395
.61	-.01	.0146
.71	-.00	.0623

X/C	Z/C	CP
.11	.01	-.4350
.21	.00	-.5103
.31	.00	-.7665
.41	.01	-.7709
.51	.01	-.6890
.62	.01	-.5671
.71	.00	-.4217
.11	-.05	-.0561
.22	-.04	-.0383
.32	-.03	-.0175
.42	-.03	.0032
.51	-.02	.0285
.62	-.01	.0696
.72	-.00	.1242

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17136

MACH .704

Q 25305.7

ALPW

.60

BETA

0.00

P1 73034.10

PT1 101627.92

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5638
.05	.05	-.2080
.10	.06	-.3195
.15	.06	-.3602
.20	.07	-.3933
.25	.07	-.4270
.30	.07	-.4637
.35	.07	-.4751
.40	.07	-.4910
.45	.07	-.4808
.50	.07	-.4598
.55	.06	-.4318
.60	.06	-.3992
.65	.05	-.3625
.70	.05	-.3106
.75	.04	-.2756
.80	.03	-.2270
.85	.03	-.1752
.90	.02	-.1120
0.00	.03	.6113
.05	.01	-.1952
.10	.01	-.1648
.15	.00	-.1627
.20	-.00	-.1645
.25	-.00	-.1634
.30	-.01	-.1722
.35	-.01	-.1714
.40	-.01	-.1697
.45	-.01	-.1710
.50	-.01	-.1687
.55	-.01	-.1536
.60	-.01	-.1337
.65	-.01	-.1124
.70	-.00	-.0841
.75	-.00	-.0553
.80	-.00	-.0214
.85	.00	.0090
.90	.00	.0635

X/C	Z/C	CP
0.00	.01	.6380
.05	.03	-.2152
.10	.04	-.3662
.15	.05	-.4191
.20	.06	-.4605
.25	.06	-.4972
.30	.07	-.5346
.35	.07	-.5534
.40	.07	-.5737
.45	.07	-.5596
.50	.07	-.5276
.55	.06	-.4888
.60	.06	-.4543
.65	.05	-.3937
.70	.05	-.3487
.75	.04	-.3033
.80	.04	-.2461
.85	.03	-.1955
0.00	.01	.5655
.04	-.00	.0235
.09	-.01	-.1296
.14	-.01	-.1218
.19	-.01	-.1087
.24	-.01	-.1042
.29	-.01	-.0947
.34	-.01	-.0946
.39	-.01	-.0922
.44	-.01	-.0801
.49	-.01	-.0565
.54	-.01	-.0326
.59	-.01	-.0025
.64	-.00	.0019
.69	-.00	.0460
.74	.00	.0564
.79	.00	.0715
.84	.00	.0926

X/C	Z/C	CP
0.00	-.01	.1154
.11	.03	.0975
.20	.05	-.1952
.31	.06	-.4625
.40	.07	-.7213
.51	.06	-.7344
.61	.06	-.5666
.71	.05	-.4100
0.00	-.01	.0940
.11	-.02	-.1078
.21	-.02	-.0641
.31	-.02	-.0646
.40	-.02	-.0398
.51	-.01	-.0315
.61	-.01	.0195
.71	-.00	.0677

X/C	Z/C	CP
.11	.01	-.5388
.21	.00	-.5906
.31	.00	-.8469
.41	.01	-.8147
.51	.01	-.7325
.62	.01	-.5880
.71	.00	-.4388
.11	-.05	-.0174
.22	-.04	-.0035
.32	-.03	.0069
.42	-.03	.0246
.51	-.02	.0422
.62	-.01	.0791
.72	-.00	.1294

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17137

MACH .703

Q 25300.1 ALPW

1.11

BETA

0.00

P1 73033.84

PT1 101620.60

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5965
.05	.05	-.2726
.10	.06	-.3688
.15	.06	-.4046
.20	.07	-.4295
.25	.07	-.4658
.30	.07	-.4903
.35	.07	-.5069
.40	.07	-.5208
.45	.07	-.5130
.50	.07	-.4766
.55	.06	-.4522
.60	.06	-.4165
.65	.05	-.3735
.70	.05	-.3223
.75	.04	-.2869
.80	.03	-.2372
.85	.03	-.1849
.90	.02	-.1180
0.00	.03	.6080
.05	.01	-.1320
.10	.01	-.1217
.15	.00	-.1252
.20	-.00	-.1318
.25	-.00	-.1424
.30	-.01	-.1306
.35	-.01	-.1396
.40	-.01	-.1417
.45	-.01	-.1510
.50	-.01	-.1503
.55	-.01	-.1387
.60	-.01	-.1193
.65	-.01	-.0962
.70	-.00	-.0705
.75	-.00	-.0217
.80	-.00	-.0021
.85	.00	.0260
.90	.00	.0927

X/C	Z/C	CP
0.00	.01	.6420
.05	.03	-.3080
.10	.04	-.4335
.15	.05	-.4911
.20	.06	-.5256
.25	.06	-.5527
.30	.07	-.5851
.35	.07	-.6000
.40	.07	-.6102
.45	.07	-.5941
.50	.07	-.5533
.55	.06	-.5108
.60	.06	-.4770
.65	.05	-.4119
.70	.05	-.3641
.75	.04	-.3125
.80	.04	-.2574
.85	.03	-.1955
0.00	.01	.5769
.04	-.00	.0681
.09	-.01	-.0937
.14	-.01	-.0783
.19	-.01	-.0859
.24	-.01	-.0752
.29	-.01	-.0747
.34	-.01	-.0706
.39	-.01	-.0717
.44	-.01	-.0599
.49	-.01	-.0357
.54	-.01	-.0150
.59	-.01	.0083
.64	-.00	.0224
.69	-.00	.0640
.74	.00	.0681
.79	.00	.0777
.84	.00	.0969

X/C	Z/C	CP
0.00	-.01	.1209
.11	.03	.0688
.20	.05	-.2462
.31	.06	-.5078
.40	.07	-.7945
.51	.06	-.7811
.61	.06	-.5953
.71	.05	-.4276
0.00	-.01	.0529
.11	-.02	-.0475
.21	-.02	-.0586
.31	-.02	-.0369
.40	-.02	-.0229
.51	-.01	-.0158
.61	-.01	.0232
.71	-.00	.0687

X/C	Z/C	CP
.11	.01	-.6457
.21	.00	-.6705
.31	.00	-.9081
.41	.01	-.8623
.51	.01	-.7568
.62	.01	-.5997
.71	.00	-.4462
.11	-.05	.0281
.22	-.04	.0237
.32	-.03	.0345
.42	-.03	.0400
.51	-.02	.0543
.62	-.01	.0891
.72	-.00	.1352

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17138

MACH

.70+

Q

25324.2

ALPW

1.55

BETA

0.00

P1 72991.55

PT1 101610.91

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6056	0.00	.01	.6373	0.00	-.01	.1288	.11	.01	-.7272
.05	.05	-.3339	.05	.03	-.3816	.11	.03	.0354	.21	.00	-.7449
.10	.06	-.4150	.10	.04	-.5074	.20	.05	-.2966	.31	.00	-.9748
.15	.06	-.4447	.15	.05	-.5540	.31	.06	-.5617	.41	.01	-.9031
.20	.07	-.4695	.20	.06	-.5816	.40	.07	-.8771	.51	.01	-.7771
.25	.07	-.4996	.25	.06	-.5968	.51	.06	-.8082	.62	.01	-.6107
.30	.07	-.5190	.30	.07	-.6231	.61	.06	-.6067	.71	.00	-.4505
.35	.07	-.5292	.35	.07	-.6455	.71	.05	-.4404	.11	-.05	.0396
.40	.07	-.5463	.40	.07	-.6490	0.00	-.01	.0093	.22	-.04	.0359
.45	.07	-.5350	.45	.07	-.6226	.11	-.02	-.0377	.32	-.03	.0405
.50	.07	-.5029	.50	.07	-.5777	.21	-.02	-.0498	.42	-.03	.0403
.55	.06	-.4618	.55	.06	-.5342	.31	-.02	-.0291	.51	-.02	.0582
.60	.06	-.4277	.60	.06	-.4919	.40	-.02	-.0086	.62	-.01	.0928
.65	.05	-.3822	.65	.05	-.4888	.51	-.01	.0014	.72	-.00	.1430
.70	.05	-.3329	.70	.05	-.3737	.61	-.01	.0290			
.75	.04	-.2942	.75	.04	-.3208	.71	-.00	.0683			
.80	.03	-.2365	.80	.04	-.2643						
.85	.03	-.1868	.85	.03	-.2043						
.90	.02	-.1230	0.00	.01	.6143						
0.00	.03	.5898	.04	-.00	.0223						
.05	.01	-.0843	.09	-.01	-.0555						
.10	.01	-.0914	.14	-.01	-.0546						
.15	.00	-.0980	.19	-.01	-.0517						
.20	-.00	-.1093	.24	-.01	-.0514						
.25	-.00	-.1175	.29	-.01	-.0548						
.30	-.01	-.1174	.34	-.01	-.0597						
.35	-.01	-.1247	.39	-.01	-.0592						
.40	-.01	-.1250	.44	-.01	-.0497						
.45	-.01	-.1358	.49	-.01	-.0298						
.50	-.01	-.1279	.54	-.01	-.0089						
.55	-.01	-.1204	.59	-.01	.0161						
.60	-.01	-.1026	.64	-.00	.0232						
.65	-.01	-.0820	.69	-.00	.0744						
.70	-.00	-.0579	.74	.00	.0780						
.75	-.00	-.0273	.79	.00	.0898						
.80	-.00	-.0048	.84	.00	.1093						
.85	.00	.0292									
.90	.00	.0887									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17139

MACH .702

Q 25231.7

ALPW

2.06

BETA

0.00

P1 73106.73

PT1 101603.51

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6051
.05	.05	-.4019
.10	.06	-.4793
.15	.06	-.4922
.20	.07	-.5100
.25	.07	-.5327
.30	.07	-.5568
.35	.07	-.5579
.40	.07	-.5781
.45	.07	-.5521
.50	.07	-.5235
.55	.06	-.4867
.60	.06	-.4448
.65	.05	-.3958
.70	.05	-.3445
.75	.04	-.3026
.80	.03	-.2477
.85	.03	-.1896
.90	.02	-.1233
0.00	.03	.5555
.05	.01	-.0327
.10	.01	-.0538
.15	.00	-.0690
.20	-.00	-.0801
.25	-.00	-.0963
.30	-.01	-.0938
.35	-.01	-.0953
.40	-.01	-.1024
.45	-.01	-.1135
.50	-.01	-.1232
.55	-.01	-.1122
.60	-.01	-.0925
.65	-.01	-.0701
.70	-.00	-.0504
.75	-.00	.0023
.80	-.00	.0148
.85	.00	.0410
.90	.00	.0835

X/C	Z/C	CP
0.00	.01	.6130
.05	.03	-.4970
.10	.04	-.5864
.15	.05	-.6090
.20	.06	-.6434
.25	.06	-.6574
.30	.07	-.6756
.35	.07	-.6805
.40	.07	-.6893
.45	.07	-.6633
.50	.07	-.6106
.55	.06	-.5487
.60	.06	-.5106
.65	.05	-.4468
.70	.05	-.3815
.75	.04	-.3314
.80	.04	-.2646
.85	.03	-.2065
0.00	.01	.5797
.04	-.00	.0589
.09	-.01	.0067
.14	-.01	-.0018
.19	-.01	-.0047
.24	-.01	-.0241
.29	-.01	-.0307
.34	-.01	-.0355
.39	-.01	-.0349
.44	-.01	-.0334
.49	-.01	-.0151
.54	-.01	.0075
.59	-.01	.0263
.64	-.00	.0386
.69	-.00	.0877
.74	.00	.0877
.79	.00	.0977
.84	.00	.1086

X/C	Z/C	CP
0.00	-.01	.1303
.11	.03	-.0083
.20	.05	-.3677
.31	.06	-.6279
.40	.07	-.9592
.51	.06	-.8587
.61	.06	-.6200
.71	.05	-.4469
0.00	-.01	-.0692
.11	-.02	-.0239
.21	-.02	-.0441
.31	-.02	-.0314
.40	-.02	.0009
.51	-.01	.0082
.61	-.01	.0375
.71	-.00	.0720

X/C	Z/C	CP
.11	.01	-.8374
.21	.00	-.9474
.31	.00	-1.0108
.41	.01	-.9278
.51	.01	-.7791
.62	.01	-.6206
.71	.00	-.4554
.11	-.05	.0797
.22	-.04	.0638
.32	-.03	.0597
.42	-.03	.0580
.51	-.02	.0688
.62	-.01	.0754
.72	-.00	.1436

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17140

MACH .704

Q 25308.0

ALPW

2.55

BETA

0.00

P1 72995.70

PT1 101594.25

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5997
.05	.05	-.4796
.10	.06	-.5345
.15	.06	-.5402
.20	.07	-.5524
.25	.07	-.5689
.30	.07	-.5886
.35	.07	-.5986
.40	.07	-.5993
.45	.07	-.5866
.50	.07	-.5463
.55	.06	-.5070
.60	.06	-.4615
.65	.05	-.4086
.70	.05	-.3566
.75	.04	-.3098
.80	.03	-.2518
.85	.03	-.1927
.90	.02	-.1253
0.00	.03	.5091
.05	.01	.0153
.10	.01	-.0141
.15	.00	-.0331
.20	-.00	-.0567
.25	-.00	-.0710
.30	-.01	-.0749
.35	-.01	-.0755
.40	-.01	-.0894
.45	-.01	-.1020
.50	-.01	-.0976
.55	-.01	-.0886
.60	-.01	-.0768
.65	-.01	-.0603
.70	-.00	-.0339
.75	-.00	.0130
.80	-.00	.0272
.85	.00	.0472
.90	.00	.1228

X/C	Z/C	CP
0.00	.01	.5626
.05	.03	-.6095
.10	.04	-.6762
.15	.05	-.7044
.20	.06	-.6951
.25	.06	-.7132
.30	.07	-.7260
.35	.07	-.7276
.40	.07	-.7330
.45	.07	-.6935
.50	.07	-.6363
.55	.06	-.5728
.60	.06	-.5277
.65	.05	-.4630
.70	.05	-.3983
.75	.04	-.3352
.80	.04	-.2754
.85	.03	-.2096
0.00	.01	.6101
.04	-.00	.0167
.09	-.01	.0221
.14	-.01	.0248
.19	-.01	.0221
.24	-.01	.0051
.29	-.01	-.0054
.34	-.01	-.0120
.39	-.01	-.0184
.44	-.01	-.0143
.49	-.01	.0058
.54	-.01	.0187
.59	-.01	.0395
.64	-.00	.0454
.69	-.00	.0905
.74	.00	.0901
.79	.00	.1003
.84	.00	.1174

X/C	Z/C	CP
0.00	-.01	.1385
.11	.03	-.0592
.20	.05	-.4706
.31	.06	-.7056
.40	.07	-1.0460
.51	.06	-.8834
.61	.06	-.6320
.71	.05	-.4548
0.00	-.01	-.1766
.11	-.02	-.0111
.21	-.02	-.0304
.31	-.02	-.0248
.40	-.02	.0103
.51	-.01	.0163
.61	-.01	.0432
.71	-.00	.0716

X/C	Z/C	CP
.11	.01	-.9173
.21	.00	-1.0808
.31	.00	-1.1550
.41	.01	-.9032
.51	.01	-.7806
.62	.01	-.6251
.71	.00	-.4543
.11	-.05	.1207
.22	-.04	.0846
.32	-.03	.0815
.42	-.03	.0666
.51	-.02	.0778
.62	-.01	.1005
.72	-.00	.1449

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17141

MACH .704

Q

25326.0

ALPW

3.06

BETA

0.00

P1 72961.92

PT1 101584.95

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5727
.05	.05	-.5473
.10	.06	-.5908
.15	.06	-.5970
.20	.07	-.6031
.25	.07	-.6027
.30	.07	-.6214
.35	.07	-.6221
.40	.07	-.6291
.45	.07	-.6138
.50	.07	-.5617
.55	.06	-.5259
.60	.06	-.4726
.65	.05	-.4203
.70	.05	-.3659
.75	.04	-.3151
.80	.03	-.2565
.85	.03	-.1986
.90	.02	-.1245
0.00	.03	.4526
.05	.01	.0631
.10	.01	.0187
.15	.00	-.0106
.20	-.00	-.0297
.25	-.00	-.0471
.30	-.01	-.0494
.35	-.01	-.0518
.40	-.01	-.0640
.45	-.01	-.0879
.50	-.01	-.0849
.55	-.01	-.0770
.60	-.01	-.0612
.65	-.01	-.0437
.70	-.00	-.0237
.75	-.00	.0420
.80	-.00	.0450
.85	.00	.0589
.90	.00	.1233

X/C	Z/C	CP
0.00	.01	.4661
.05	.03	-.7187
.10	.04	-.7787
.15	.05	-.7705
.20	.06	-.7671
.25	.06	-.7684
.30	.07	-.7885
.35	.07	-.7778
.40	.07	-.7718
.45	.07	-.7187
.50	.07	-.6714
.55	.06	-.5957
.60	.06	-.5421
.65	.05	-.5399
.70	.05	-.4065
.75	.04	-.3417
.80	.04	-.2808
.85	.03	-.2095
0.00	.01	.4676
.04	-.00	.0405
.09	-.01	.0894
.14	-.01	.0681
.19	-.01	.0526
.24	-.01	.0325
.29	-.01	.0193
.34	-.01	.0073
.39	-.01	.0050
.44	-.01	.0033
.49	-.01	.0162
.54	-.01	.0321
.59	-.01	.0531
.64	-.00	.0639
.69	-.00	.1001
.74	.00	.1033
.79	.00	.1125
.84	.00	.1239

X/C	Z/C	CP
0.00	-.01	.1421
.11	.03	-.1298
.20	.05	-.4879
.31	.06	-.7411
.40	.07	-1.1372
.51	.06	-.9651
.61	.06	-.6511
.71	.05	-.4638
0.00	-.01	-.2989
.11	-.02	-.0018
.21	-.02	-.0209
.31	-.02	-.0141
.40	-.02	.0166
.51	-.01	.0228
.61	-.01	.0453
.71	-.00	.0743

X/C	Z/C	CP
.11	.01	-1.0360
.21	.00	-1.1457
.31	.00	-1.3053
.41	.01	-.9789
.51	.01	-.7603
.62	.01	-.6124
.71	.00	-.4482
.11	-.05	.1516
.22	-.04	.1128
.32	-.03	.0908
.42	-.03	.0826
.51	-.02	.0870
.62	-.01	.1055
.72	-.00	.1439

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17142

MACH .704

Q 25312.2

ALPM

4.05

BETA

0.00

P1 72975.38

PY1 101580.21

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4809
.05	.05	-.7102
.10	.06	-.7116
.15	.06	-.6874
.20	.07	-.6746
.25	.07	-.6744
.30	.07	-.6862
.35	.07	-.6727
.40	.07	-.6996
.45	.07	-.6528
.50	.07	-.6175
.55	.06	-.5579
.60	.06	-.5006
.65	.05	-.4456
.70	.05	-.3812
.75	.04	-.3284
.80	.03	-.2674
.85	.03	-.2011
.90	.02	-.1287
0.00	.03	.2822
.05	.01	.1488
.10	.01	.0840
.15	.00	.0468
.20	-.00	.0188
.25	-.00	-.0079
.30	-.01	-.0025
.35	-.01	-.0027
.40	-.01	-.0198
.45	-.01	-.0484
.50	-.01	-.0530
.55	-.01	-.0474
.60	-.01	-.0308
.65	-.01	-.0209
.70	-.00	-.0003
.75	-.00	.0409
.80	-.00	.0404
.85	.00	.0661
.90	.00	.1135

X/C	Z/C	CP
0.00	.01	.2799
.05	.03	-.9575
.10	.04	-.9680
.15	.05	-.9023
.20	.06	-.8908
.25	.06	-.8579
.30	.07	-.8580
.35	.07	-.8418
.40	.07	-.8256
.45	.07	-.7757
.50	.07	-.6981
.55	.06	-.6282
.60	.06	-.5627
.65	.05	-.4893
.70	.05	-.4079
.75	.04	-.3460
.80	.04	-.2679
.85	.03	-.2042
0.00	.01	.3041
.04	-.00	.0162
.09	-.01	.1720
.14	-.01	.1346
.19	-.01	.1043
.24	-.01	.0823
.29	-.01	.0646
.34	-.01	.0496
.39	-.01	.0412
.44	-.01	.0365
.49	-.01	.0479
.54	-.01	.0583
.59	-.01	.0711
.64	-.00	.0823
.69	-.00	.1128
.74	.00	.1156
.79	.00	.1178
.84	.00	.1298

X/C	Z/C	CP
0.00	-.01	.1411
.11	.03	-.2838
.20	.05	-.6237
.31	.06	-.8726
.40	.07	-1.1813
.51	.06	-.9834
.61	.06	-.6810
.71	.05	-.5131
0.00	-.01	-.6158
.11	-.02	-.0010
.21	-.02	-.0145
.31	-.02	-.0142
.40	-.02	.0201
.51	-.01	.0264
.61	-.01	.0519
.71	-.00	.0683

X/C	Z/C	CP
.11	.01	-1.2766
.21	.00	-1.2224
.31	.00	-1.3875
.41	.01	-.9878
.51	.01	-.7301
.62	.01	-.5742
.71	.00	-.4178
.11	-.05	.2051
.22	-.04	.1431
.32	-.03	.1179
.42	-.03	.1017
.51	-.02	.1021
.62	-.01	.1118
.72	-.00	.1430

7 X 10 HIGH SPEED TUNNEL

RUN

17

TP 17143

Q 25307.2

ALPW

6.07

BETA

0.00

P1 72981.05

PT1 101579.38

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.2154
.05	.05	-.9412
.10	.06	-.9778
.15	.06	-.8778
.20	.07	-.8539
.25	.07	-.8303
.30	.07	-.8174
.35	.07	-.8180
.40	.07	-.8003
.45	.07	-.7510
.50	.07	-.6791
.55	.06	-.6093
.60	.06	-.5393
.65	.05	-.4686
.70	.05	-.3979
.75	.04	-.3385
.80	.03	-.2714
.85	.03	-.1984
.90	.02	-.1287
0.00	.03	-.1321
.05	.01	.2898
.10	.01	.1969
.15	.00	.1418
.20	-.00	.1055
.25	-.00	.0767
.30	-.01	.0515
.35	-.01	.0528
.40	-.01	.0513
.45	-.01	.0004
.50	-.01	-.0043
.55	-.01	.0018
.60	-.01	.0026
.65	-.01	.0137
.70	-.00	.0292
.75	-.00	.0792
.80	-.00	.0770
.85	.00	.0909
.90	.00	.1013

X/C	Z/C	CP
0.00	.01	-.1273
.05	.03	-1.8352
.10	.04	-1.6664
.15	.05	-1.5952
.20	.06	-.9055
.25	.06	-.8746
.30	.07	-.8851
.35	.07	-.8952
.40	.07	-.8523
.45	.07	-.7868
.50	.07	-.6966
.55	.06	-.6159
.60	.06	-.5306
.65	.05	-.4610
.70	.05	-.3734
.75	.04	-.2917
.80	.04	-.2264
.85	.03	-.1683
0.00	.01	-.1381
.04	-.00	-.0171
.09	-.01	.2694
.14	-.01	.2302
.19	-.01	.2147
.24	-.01	.1554
.29	-.01	.1294
.34	-.01	.1064
.39	-.01	.0902
.44	-.01	.0789
.49	-.01	.0826
.54	-.01	.0836
.59	-.01	.0981
.64	-.00	.0982
.69	-.00	.1161
.74	.00	.1195
.79	.00	.1202
.84	.00	.1244

X/C	Z/C	CP
0.00	-.01	.1362
.11	.03	-.5312
.20	.05	-.8294
.31	.06	-1.1027
.40	.07	-1.0974
.51	.06	-.9840
.61	.06	-.8228
.71	.05	-.6950
0.00	-.01	-1.2814
.11	-.02	-.0300
.21	-.02	-.0226
.31	-.02	-.0193
.40	-.02	-.0000
.51	-.01	.0096
.61	-.01	.0371
.71	-.00	.0397

X/C	Z/C	CP
.11	.01	-1.3746
.21	.00	-1.2348
.31	.00	-1.0583
.41	.01	-.6749
.51	.01	-.5332
.62	.01	-.4492
.71	.00	-.4077
.11	-.05	.2442
.22	-.04	.1650
.32	-.03	.1229
.42	-.03	.0913
.51	-.02	.0826
.62	-.01	.0718
.72	-.00	.0822

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 17

TP 17144

MACH .704

Q

25292.5

ALPW

.05

BETA

0.00

P1 72993.62

PT1 101572.67

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5194
.05	.05	-.1363
.10	.06	-.2580
.15	.06	-.3063
.20	.07	-.3464
.25	.07	-.3884
.30	.07	-.4239
.35	.07	-.4401
.40	.07	-.4608
.45	.07	-.4635
.50	.07	-.4356
.55	.06	-.4171
.60	.06	-.3815
.65	.05	-.3421
.70	.05	-.3008
.75	.04	-.2699
.80	.03	-.2182
.85	.03	-.1725
.90	.02	-.1131
0.00	.03	.6031
.05	.01	-.2576
.10	.01	-.2127
.15	.00	-.1929
.20	-.00	-.1932
.25	-.00	-.1934
.30	-.01	-.2006
.35	-.01	-.1971
.40	-.01	-.1985
.45	-.01	-.1981
.50	-.01	-.1968
.55	-.01	-.1746
.60	-.01	-.1514
.65	-.01	-.1221
.70	-.00	-.0965
.75	-.00	-.0618
.80	-.00	-.0359
.85	.00	.0034
.90	.00	.0645

X/C	Z/C	CP
0.00	.01	.6204
.05	.03	-.1313
.10	.04	-.2808
.15	.05	-.3634
.20	.06	-.4122
.25	.06	-.4476
.30	.07	-.4907
.35	.07	-.5105
.40	.07	-.5326
.45	.07	-.5225
.50	.07	-.4878
.55	.06	-.4584
.60	.06	-.4346
.65	.05	-.4017
.70	.05	-.3308
.75	.04	-.3372
.80	.04	-.2422
.85	.03	-.1863
0.00	.01	.5687
.04	-.00	.0010
.09	-.01	-.1686
.14	-.01	-.1679
.19	-.01	-.1671
.24	-.01	-.1398
.29	-.01	-.1351
.34	-.01	-.1235
.39	-.01	-.1186
.44	-.01	-.1029
.49	-.01	-.0706
.54	-.01	-.0493
.59	-.01	-.0191
.64	-.00	-.0070
.69	-.00	.0433
.74	.00	.0392
.79	.00	.0543
.84	.00	.0762

X/C	Z/C	CP
0.00	-.01	.1032
.11	.03	.1035
.20	.05	-.1354
.31	.06	-.3790
.40	.07	-.6456
.51	.06	-.6748
.61	.06	-.5404
.71	.05	-.3953
0.00	-.01	.1124
.11	-.02	-.1997
.21	-.02	-.0607
.31	-.02	-.0636
.40	-.02	-.0540
.51	-.01	-.0347
.61	-.01	.0109
.71	-.00	.0610

X/C	Z/C	CP
.11	.01	-.4304
.21	.00	-.5128
.31	.00	-.7586
.41	.01	-.7727
.51	.01	-.7022
.62	.01	-.5699
.71	.00	-.4278
.11	-.05	-.0508
.22	-.04	-.0390
.32	-.03	-.0137
.42	-.03	.0024
.51	-.02	.0312
.62	-.01	.0740
.72	-.00	.1215

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17161

MACH .602

Q 20168.2

ALPW

-1.88

BETA

0.00

P1 79370.53

PT1 101435.97

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.1525
.05	.05	.0577
.10	.06	-.0799
.15	.06	-.1621
.20	.07	-.2023
.25	.07	-.2537
.30	.07	-.2833
.35	.07	-.3110
.40	.07	-.3242
.45	.07	-.3277
.50	.07	-.3235
.55	.06	-.3086
.60	.06	-.2890
.65	.05	-.2581
.70	.05	-.2313
.75	.04	-.2105
.80	.03	-.1744
.85	.03	-.1354
.90	.02	-.0926
0.00	.03	.4249
.05	.01	-.4644
.10	.01	-.3323
.15	.00	-.2953
.20	-.00	-.2670
.25	-.00	-.2630
.30	-.01	-.2621
.35	-.01	-.2605
.40	-.01	-.2607
.45	-.01	-.2190
.50	-.01	-.2156
.55	-.01	-.2134
.60	-.01	-.1869
.65	-.01	-.1599
.70	-.00	-.1310
.75	-.00	-.0979
.80	-.00	-.0607
.85	.00	-.0278
.90	.00	.0310

X/C	Z/C	CP
0.00	.01	.2948
.05	.03	.1343
.10	.04	-.0537
.15	.05	-.1425
.20	.06	-.2038
.25	.06	-.2531
.30	.07	-.3019
.35	.07	-.3296
.40	.07	-.3621
.45	.07	-.3576
.50	.07	-.3591
.55	.06	-.3286
.60	.06	-.3234
.65	.05	-.3202
.70	.05	-.2554
.75	.04	-.2554
.80	.04	-.1905
.85	.03	-.1555
0.00	.01	.2354
.04	-.00	.0709
.09	-.01	-.4245
.14	-.01	-.3282
.19	-.01	-.2802
.24	-.01	-.2528
.29	-.01	-.2245
.34	-.01	-.2013
.39	-.01	-.1892
.44	-.01	-.1578
.49	-.01	-.1311
.54	-.01	-.0937
.59	-.01	-.0643
.64	-.00	-.0464
.69	-.00	.0026
.74	.00	.0144
.79	.00	.0270
.84	.00	.0491

X/C	Z/C	CP
0.00	-.01	.0729
.11	.03	.0682
.20	.05	-.1783
.31	.06	-.2767
.40	.07	-.4985
.51	.06	-.4944
.61	.06	-.4116
.71	.05	-.3214
0.00	-.01	.1211
.11	-.02	-.4748
.21	-.02	.2127
.31	-.02	.0914
.40	-.02	-.0835
.51	-.01	-.0378
.61	-.01	.0051
.71	-.00	.0539

X/C	Z/C	CP
.11	.01	-.1585
.21	.00	-.2774
.31	.00	-.5100
.41	.01	-.5446
.51	.01	-.5219
.62	.01	-.4577
.71	.00	-.3588
.11	-.05	-.6174
.22	-.04	-.4380
.32	-.03	-.2089
.42	-.03	-.0517
.51	-.02	.0183
.62	-.01	.0540
.72	-.00	.1036

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17162

MACH .602

Q

20165.6

ALPW

-1.43

BETA

0.00

P1 79373.08

PT1 101435.42

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.2555
.05	.05	.0216
.10	.06	-.1224
.15	.06	-.1893
.20	.07	-.2351
.25	.07	-.2792
.30	.07	-.3123
.35	.07	-.3316
.40	.07	-.3523
.45	.07	-.3483
.50	.07	-.3369
.55	.06	-.3215
.60	.06	-.2946
.65	.05	-.2741
.70	.05	-.2368
.75	.04	-.2192
.80	.03	-.1813
.85	.03	-.1407
.90	.02	-.0954
0.00	.03	.4841
.05	.01	-.4182
.10	.01	-.2878
.15	.00	-.2603
.20	-.00	-.2467
.25	-.00	-.2408
.30	-.01	-.2470
.35	-.01	-.2399
.40	-.01	-.2368
.45	-.01	-.2149
.50	-.01	-.2157
.55	-.01	-.1967
.60	-.01	-.1840
.65	-.01	-.1510
.70	-.00	-.1246
.75	-.00	-.0894
.80	-.00	-.0523
.85	.00	-.0204
.90	.00	.0351

X/C	Z/C	CP
0.00	.01	.4050
.05	.03	.0791
.10	.04	-.0977
.15	.05	-.1898
.20	.06	-.2411
.25	.06	-.2909
.30	.07	-.3285
.35	.07	-.3615
.40	.07	-.3875
.45	.07	-.3859
.50	.07	-.3730
.55	.06	-.3554
.60	.06	-.3395
.65	.05	-.3431
.70	.05	-.2697
.75	.04	-.2738
.80	.04	-.1979
.85	.03	-.1598
0.00	.01	.2465
.04	-.00	.0471
.09	-.01	-.3502
.14	-.01	-.2866
.19	-.01	-.2860
.24	-.01	-.2232
.29	-.01	-.1974
.34	-.01	-.1823
.39	-.01	-.1719
.44	-.01	-.1460
.49	-.01	-.1126
.54	-.01	-.0866
.59	-.01	-.0533
.64	-.00	-.0466
.69	-.00	.0128
.74	.00	.0133
.79	.00	.0364
.84	.00	.0540

X/C	Z/C	CP
0.00	-.01	.0844
.11	.03	.0803
.20	.05	-.1158
.31	.06	-.2854
.40	.07	-.5200
.51	.06	-.5198
.61	.06	-.4304
.71	.05	-.3330
0.00	-.01	.1333
.11	-.02	-.4063
.21	-.02	.0688
.31	-.02	.0694
.40	-.02	-.0591
.51	-.01	-.0433
.61	-.01	.0021
.71	-.00	.0524

X/C	Z/C	CP
.11	.01	-.2059
.21	.00	-.3154
.31	.00	-.5405
.41	.01	-.5727
.51	.01	-.5419
.62	.01	-.4725
.71	.00	-.3661
.11	-.05	-.5611
.22	-.04	-.3011
.32	-.03	-.1072
.42	-.03	-.0232
.51	-.02	.0120
.62	-.01	.0534
.72	-.00	.1087

7 X 10 HIGH SPEED TUNNEL

TEST 107

R J N 18

TP 17163

MACH .602

Q 20152.0

ALPW

-93

BETA

0.00

P1 79389.99

PT1 101435.72

Y/B/2 - .31

$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.3710
.05	.05	-.0335
.10	.06	-.1642
.15	.06	-.2261
.20	.07	-.2634
.25	.07	-.3057
.30	.07	-.3401
.35	.07	-.3525
.40	.07	-.3714
.45	.07	-.3719
.50	.07	-.3505
.55	.06	-.3391
.60	.06	-.3088
.65	.05	-.2862
.70	.05	-.2486
.75	.04	-.2267
.80	.03	-.1885
.85	.03	-.1429
.90	.02	-.0992
0.00	.03	.5454
.05	.01	-.3582
.10	.01	-.2572
.15	.00	-.2232
.20	-.00	-.2141
.25	-.00	-.2153
.30	-.01	-.2104
.35	-.01	-.2116
.40	-.01	-.2100
.45	-.01	-.1992
.50	-.01	-.1985
.55	-.01	-.1797
.60	-.01	-.1601
.65	-.01	-.1340
.70	-.00	-.1049
.75	-.00	-.0781
.80	-.00	-.0448
.85	.00	-.0123
.90	.00	.0403

X/C	Z/C	CP
0.00	.01	.5052
.05	.03	.0154
.10	.04	-.1524
.15	.05	-.2361
.20	.06	-.2900
.25	.06	-.3282
.30	.07	-.3685
.35	.07	-.3951
.40	.07	-.4201
.45	.07	-.4146
.50	.07	-.3985
.55	.06	-.3694
.60	.06	-.3549
.65	.05	-.3528
.70	.05	-.3332
.75	.04	-.2731
.80	.04	-.2101
.85	.03	-.1692
0.00	.01	.4221
.04	-.00	.0427
.09	-.01	-.2978
.14	-.01	-.2340
.19	-.01	-.2082
.24	-.01	-.1906
.29	-.01	-.1712
.34	-.01	-.1587
.39	-.01	-.1523
.44	-.01	-.1276
.49	-.01	-.0989
.54	-.01	-.0689
.59	-.01	-.0412
.64	-.00	-.0292
.69	-.00	.0171
.74	.00	.0250
.79	.00	.0415
.84	.00	.0591

X/C	Z/C	CP
0.00	-.01	.0876
.11	.03	.0876
.20	.05	-.1806
.31	.06	-.3442
.40	.07	-.5747
.51	.06	-.5502
.61	.06	-.4528
.71	.05	-.3457
0.00	-.01	.1380
.11	-.02	-.3355
.21	-.02	-.0259
.31	-.02	-.0242
.40	-.02	-.0508
.51	-.01	-.0445
.61	-.01	.0014
.71	-.00	.0534

X/C	Z/C	CP
.11	.01	-.2779
.21	.00	-.3674
.31	.00	-.5854
.41	.01	-.6025
.51	.01	-.5689
.62	.01	-.4868
.71	.00	-.3793
.11	-.05	-.4086
.22	-.04	-.1196
.32	-.03	-.0566
.42	-.03	-.0235
.51	-.02	.0032
.62	-.01	.0474
.72	-.00	.1002

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17164

MACH .603

Q 20176.4

ALPW

-.40

BETA

0.00

P1 79363.57

PT1 101438.93

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4641
.05	.05	-.0908
.10	.06	-.2123
.15	.06	-.2650
.20	.07	-.3064
.25	.07	-.3427
.30	.07	-.3698
.35	.07	-.3785
.40	.07	-.3968
.45	.07	-.3900
.50	.07	-.3697
.55	.06	-.3536
.60	.06	-.3260
.65	.05	-.2995
.70	.05	-.2590
.75	.04	-.2353
.80	.03	-.1926
.85	.03	-.1526
.90	.02	-.1031
0.00	.03	.5804
.05	.01	-.2914
.10	.01	-.2162
.15	.00	-.1991
.20	-.00	-.1924
.25	-.00	-.1900
.30	-.01	-.1863
.35	-.01	-.1883
.40	-.01	-.1874
.45	-.01	-.1883
.50	-.01	-.1863
.55	-.01	-.1715
.60	-.01	-.1530
.65	-.01	-.1191
.70	-.00	-.0930
.75	-.00	-.0629
.80	-.00	-.0306
.85	.00	.0017
.90	.00	.0516

X/C	Z/C	CP
0.00	.01	.5792
.05	.03	-.0604
.10	.04	-.2238
.15	.05	-.2882
.20	.06	-.3418
.25	.06	-.3746
.30	.07	-.4110
.35	.07	-.4293
.40	.07	-.4473
.45	.07	-.4412
.50	.07	-.4255
.55	.06	-.4001
.60	.06	-.3781
.65	.05	-.3758
.70	.05	-.3527
.75	.04	-.3210
.80	.04	-.2178
.85	.03	-.1741
0.00	.01	.4812
.04	-.00	.0328
.09	-.01	-.2363
.14	-.01	-.1868
.19	-.01	-.1851
.24	-.01	-.1598
.29	-.01	-.1459
.34	-.01	-.1342
.39	-.01	-.1265
.44	-.01	-.1093
.49	-.01	-.0833
.54	-.01	-.0596
.59	-.01	-.0299
.64	-.00	-.0165
.69	-.00	.0277
.74	.00	.0326
.79	.00	.0475
.84	.00	.0704

X/C	Z/C	CP
0.00	-.01	.0918
.11	.03	.0921
.20	.05	-.2136
.31	.06	-.3992
.40	.07	-.6177
.51	.06	-.5808
.61	.06	-.4756
.71	.05	-.3635
0.00	-.01	.1355
.11	-.02	-.2663
.21	-.02	-.0751
.31	-.02	-.0752
.40	-.02	-.0557
.51	-.01	-.0435
.61	-.01	.0053
.71	-.00	.0550

X/C	Z/C	CP
.11	.01	-.3549
.21	.00	-.4215
.31	.00	-.6357
.41	.01	-.6389
.51	.01	-.5986
.62	.01	-.5078
.71	.00	-.3961
.11	-.05	-.1474
.22	-.04	-.0594
.32	-.03	-.0359
.42	-.03	-.0097
.51	-.02	.0154
.62	-.01	.0549
.72	-.00	.1053

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17165

MACH .602

Q 20163.7

ALPW

.06

BETA

0.00

P1 79374.64

PT1 101434.68

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5259
.05	.05	-.1492
.10	.06	-.2623
.15	.06	-.3037
.20	.07	-.3308
.25	.07	-.3710
.30	.07	-.3924
.35	.07	-.4026
.40	.07	-.4175
.45	.07	-.4104
.50	.07	-.3900
.55	.06	-.3696
.60	.06	-.3381
.65	.05	-.3071
.70	.05	-.2689
.75	.04	-.2433
.80	.03	-.1990
.85	.03	-.1568
.90	.02	-.1087
0.00	.03	.5968
.05	.01	-.2304
.10	.01	-.1893
.15	.00	-.1764
.20	-.00	-.1684
.25	-.00	-.1795
.30	-.01	-.1746
.35	-.01	-.1742
.40	-.01	-.1754
.45	-.01	-.1650
.50	-.01	-.1633
.55	-.01	-.1513
.60	-.01	-.1289
.65	-.01	-.1058
.70	-.00	-.0800
.75	-.00	-.0525
.80	-.00	-.0213
.85	.00	.0092
.90	.00	.0367

X/C	Z/C	CP
0.00	.01	.6118
.05	.03	-.1326
.10	.04	-.2749
.15	.05	-.3432
.20	.06	-.3769
.25	.06	-.4152
.30	.07	-.4463
.35	.07	-.4620
.40	.07	-.4759
.45	.07	-.4685
.50	.07	-.4461
.55	.06	-.4113
.60	.06	-.3966
.65	.05	-.3941
.70	.05	-.3677
.75	.04	-.3363
.80	.04	-.2267
.85	.03	-.1826
0.00	.01	.2956
.04	-.00	.0689
.09	-.01	-.1810
.14	-.01	-.1479
.19	-.01	-.1345
.24	-.01	-.1285
.29	-.01	-.1198
.34	-.01	-.1100
.39	-.01	-.1080
.44	-.01	-.0922
.49	-.01	-.0682
.54	-.01	-.0419
.59	-.01	-.0223
.64	-.00	-.0057
.69	-.00	.0368
.74	.00	.0374
.79	.00	.0515
.84	.00	.0742

X/C	Z/C	CP
0.00	-.01	.0964
.11	.03	.0982
.20	.05	-.1606
.31	.06	-.4095
.40	.07	-.6622
.51	.06	-.6130
.61	.06	-.4984
.71	.05	-.3803
0.00	-.01	.1260
.11	-.02	-.1693
.21	-.02	-.0951
.31	-.02	-.0947
.40	-.02	-.0556
.51	-.01	-.0421
.61	-.01	.0097
.71	-.00	.0552

X/C	Z/C	CP
.11	.01	-.4153
.21	.00	-.4793
.31	.00	-.6690
.41	.01	-.6778
.51	.01	-.6184
.62	.01	-.5262
.71	.00	-.4092
.11	-.05	-.0463
.22	-.04	-.0380
.32	-.03	-.0153
.42	-.03	.0005
.51	-.02	.0265
.62	-.01	.0646
.72	-.00	.1132

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17166

MACH .602

Q 20151.4

ALPW

.57

BETA

0.00

P1 79387.17

PT1 101432.19

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5709	0.00	.01	.6293	0.00	-.01	.1078	.11	.01	-.5102
.05	.05	-.2099	.05	.03	-.2217	.11	.03	.1064	.21	.00	-.5504
.10	.06	-.3105	.10	.04	-.3426	.20	.05	-.2779	.31	.00	-.7281
.15	.06	-.3447	.15	.05	-.3897	.31	.06	-.4899	.41	.01	-.7083
.20	.07	-.3669	.20	.06	-.4247	.40	.07	-.7072	.51	.01	-.6444
.25	.07	-.4018	.25	.06	-.4564	.51	.06	-.6526	.62	.01	-.5450
.30	.07	-.4218	.30	.07	-.4892	.61	.06	-.5213	.71	.00	-.4228
.35	.07	-.4334	.35	.07	-.4965	.71	.05	-.3969	.11	-.05	-.0111
.40	.07	-.4400	.40	.07	-.5061	0.00	-.01	.1088	.22	-.04	-.0087
.45	.07	-.4321	.45	.07	-.4989	.11	-.02	-.0928	.32	-.03	.0061
.50	.07	-.4092	.50	.07	-.4713	.21	-.02	-.0898	.42	-.03	.0192
.55	.06	-.3885	.55	.06	-.4327	.31	-.02	-.0906	.51	-.02	.0382
.60	.06	-.3510	.60	.06	-.4124	.40	-.02	-.0416	.62	-.01	.0721
.65	.05	-.3193	.65	.05	-.4061	.51	-.01	-.0292	.72	-.00	.1187
.70	.05	-.2812	.70	.05	-.3780	.61	-.01	.0146			
.75	.04	-.2499	.75	.04	-.3465	.71	-.00	.0588			
.80	.03	-.2060	.80	.04	-.2346						
.85	.03	-.1623	.85	.03	-.1893						
.90	.02	-.1112	0.00	.01	.5609						
0.00	.03	.6013	.04	-.00	.0263						
.05	.01	-.1705	.09	-.01	-.1387						
.10	.01	-.1522	.14	-.01	-.1078						
.15	.00	-.1447	.19	-.01	-.1002						
.20	-.00	-.1448	.24	-.01	-.0989						
.25	-.00	-.1507	.29	-.01	-.0902						
.30	-.01	-.1527	.34	-.01	-.0863						
.35	-.01	-.1506	.39	-.01	-.0853						
.40	-.01	-.1505	.44	-.01	-.0727						
.45	-.01	-.1480	.49	-.01	-.0479						
.50	-.01	-.1467	.54	-.01	-.0281						
.55	-.01	-.1465	.59	-.01	-.0058						
.60	-.01	-.1235	.64	-.00	.0118						
.65	-.01	-.0985	.69	-.00	.0482						
.70	-.00	-.0749	.74	.00	.0543						
.75	-.00	-.0443	.79	.00	.0652						
.80	-.00	-.0142	.84	.00	.0847						
.85	.00	.0095									
.90	.00	.0664									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17167

MACH .602

Q 20158.9

ALPW

1.11

BETA

0.00

P1 79375.73

PT1 101429.96

Y/B/2 = .51

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5906
.05	.05	-.2771
.10	.06	-.3617
.15	.06	-.3900
.20	.07	-.4114
.25	.07	-.4321
.30	.07	-.4526
.35	.07	-.4644
.40	.07	-.4709
.45	.07	-.4544
.50	.07	-.4292
.55	.06	-.4058
.60	.06	-.3674
.65	.05	-.3322
.70	.05	-.2922
.75	.04	-.2599
.80	.03	-.2120
.85	.03	-.1650
.90	.02	-.1144
0.00	.03	.5913
.05	.01	-.1098
.10	.01	-.1076
.15	.00	-.1094
.20	-.00	-.1112
.25	-.00	-.1250
.30	-.01	-.1254
.35	-.01	-.1311
.40	-.01	-.1314
.45	-.01	-.1314
.50	-.01	-.1268
.55	-.01	-.1183
.60	-.01	-.1027
.65	-.01	-.0843
.70	-.00	-.0608
.75	-.00	-.0333
.80	-.00	-.0062
.85	.00	.0223
.90	.00	.0497

X/C	Z/C	CP
0.00	.01	.6353
.05	.03	-.3012
.10	.04	-.4163
.15	.05	-.4641
.20	.06	-.4790
.25	.06	-.5059
.30	.07	-.5232
.35	.07	-.5331
.40	.07	-.5426
.45	.07	-.5263
.50	.07	-.4988
.55	.06	-.4619
.60	.06	-.4295
.65	.05	-.4271
.70	.05	-.4013
.75	.04	-.3683
.80	.04	-.2431
.85	.03	-.1929
0.00	.01	.5322
.04	-.00	.0351
.09	-.01	-.0866
.14	-.01	-.0745
.19	-.01	-.0739
.24	-.01	-.0725
.29	-.01	-.0689
.34	-.01	-.0690
.39	-.01	-.0658
.44	-.01	-.0580
.49	-.01	-.0356
.54	-.01	-.0162
.59	-.01	.0089
.64	-.00	.0194
.69	-.00	.0612
.74	.00	.0592
.79	.00	.0767
.84	.00	.0972

X/C	Z/C	CP
0.00	-.01	.1174
.11	.03	.1143
.20	.05	-.2403
.31	.06	-.5213
.40	.07	-.7574
.51	.06	-.6816
.61	.06	-.5444
.71	.05	-.4152
0.00	-.01	.0696
.11	-.02	-.0393
.21	-.02	-.0713
.31	-.02	-.0720
.40	-.02	-.0245
.51	-.01	-.0135
.61	-.01	.0230
.71	-.00	.0622

X/C	Z/C	CP
.11	.01	-.6117
.21	.00	-.6095
.31	.00	-.7740
.41	.01	-.7560
.51	.01	-.6750
.62	.01	-.5641
.71	.00	-.4322
.11	-.05	-.0081
.22	-.04	.0189
.32	-.03	.0290
.42	-.03	.0352
.51	-.02	.0530
.62	-.01	.0807
.72	-.00	.1257

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17168

MACH .602

Q 20149.0

ALPW

1.52

BETA

0.00

P1 79384.20

PT1 101426.47

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6006	0.00	.01	.6260	0.00	-.01	.1244	.11	.01	-.6807
.05	.05	-.3148	.05	.03	-.3735	.11	.03	.0608	.21	.00	-.6603
.10	.06	-.4091	.10	.04	-.4828	.20	.05	-.3000	.31	.00	-.8300
.15	.06	-.4240	.15	.05	-.4977	.31	.06	-.5712	.41	.01	-.7724
.20	.07	-.4414	.20	.06	-.5244	.40	.07	-.7958	.51	.01	-.6979
.25	.07	-.4606	.25	.06	-.5461	.51	.06	-.7136	.62	.01	-.5792
.30	.07	-.4797	.30	.07	-.5631	.61	.06	-.5664	.71	.00	-.4436
.35	.07	-.4850	.35	.07	-.5613	.71	.05	-.4247	.11	-.05	.0251
.40	.07	-.4858	.40	.07	-.5669	0.00	-.01	.0232	.22	-.04	.0303
.45	.07	-.4691	.45	.07	-.5501	.11	-.02	-.0340	.32	-.03	.0303
.50	.07	-.4453	.50	.07	-.5168	.21	-.02	-.0591	.42	-.03	.0402
.55	.06	-.4212	.55	.06	-.4784	.31	-.02	-.0573	.51	-.02	.0560
.60	.06	-.3759	.60	.06	-.4438	.40	-.02	-.0123	.62	-.01	.0865
.65	.05	-.3442	.65	.05	-.4411	.51	-.01	-.0033	.72	-.00	.1323
.70	.05	-.3005	.70	.05	-.3484	.61	-.01	.0268			
.75	.04	-.2682	.75	.04	-.3526	.71	-.00	.0662			
.80	.03	-.2181	.80	.04	-.2490						
.85	.03	-.1728	.85	.03	-.1992						
.90	.02	-.1165	0.00	.01	.6383						
0.00	.03	.5758	.04	-.00	.0161						
.05	.01	-.0718	.09	-.01	-.0059						
.10	.01	-.0756	.14	-.01	-.0349						
.15	.00	-.0862	.19	-.01	-.0376						
.20	-.00	-.0968	.24	-.01	-.0485						
.25	-.00	-.1073	.29	-.01	-.0529						
.30	-.01	-.1081	.34	-.01	-.0499						
.35	-.01	-.1072	.39	-.01	-.0504						
.40	-.01	-.1148	.44	-.01	-.0474						
.45	-.01	-.1192	.49	-.01	-.0274						
.50	-.01	-.1214	.54	-.01	-.0050						
.55	-.01	-.1078	.59	-.01	.0129						
.60	-.01	-.0931	.64	-.00	.0387						
.65	-.01	-.0715	.69	-.00	.0695						
.70	-.00	-.0476	.74	.00	.0683						
.75	-.00	-.0271	.79	.00	.0850						
.80	-.00	-.0030	.84	.00	.0996						
.85	.00	.0265									
.90	.00	.1055									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17169

MACH .603

Q 20167.9

ALPW

2.03

BETA

0.00

P1 79359.25

PT1 101424.61

Y/B/2 - .31

$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.5980
.05	.05	-.3987
.10	.06	-.4613
.15	.06	-.4674
.20	.07	-.4779
.25	.07	-.4902
.30	.07	-.5060
.35	.07	-.5086
.40	.07	-.5158
.45	.07	-.4930
.50	.07	-.4640
.55	.06	-.4291
.60	.06	-.3933
.65	.05	-.3554
.70	.05	-.3116
.75	.04	-.2721
.80	.03	-.2258
.85	.03	-.1741
.90	.02	-.1211
0.00	.03	.5327
.05	.01	-.0130
.10	.01	-.0381
.15	.00	-.0563
.20	-.00	-.0698
.25	-.00	-.0802
.30	-.01	-.0832
.35	-.01	-.0888
.40	-.01	-.0899
.45	-.01	-.1039
.50	-.01	-.1004
.55	-.01	-.0921
.60	-.01	-.0761
.65	-.01	-.0566
.70	-.00	-.0399
.75	-.00	-.0132
.80	-.00	.0114
.85	.00	.0357
.90	.00	.1056

X/C	Z/C	CP
0.00	.01	.5962
.05	.03	-.4827
.10	.04	-.5502
.15	.05	-.5657
.20	.06	-.5805
.25	.06	-.5924
.30	.07	-.6022
.35	.07	-.6073
.40	.07	-.5999
.45	.07	-.5807
.50	.07	-.5417
.55	.06	-.4972
.60	.06	-.4590
.65	.05	-.4647
.70	.05	-.3592
.75	.04	-.3157
.80	.04	-.2551
.85	.03	-.2025
0.00	.01	.6023
.04	-.00	.0164
.09	-.01	.0165
.14	-.01	-.0054
.19	-.01	.0022
.24	-.01	-.0224
.29	-.01	-.0245
.34	-.01	-.0336
.39	-.01	-.0292
.44	-.01	-.0271
.49	-.01	-.0128
.54	-.01	.0068
.59	-.01	.0268
.64	-.00	.0493
.69	-.00	.0800
.74	.00	.0835
.79	.00	.0932
.84	.00	.1076

X/C	Z/C	CP
0.00	-.01	.1263
.11	.03	.0329
.20	.05	-.3502
.31	.06	-.6347
.40	.07	-.8441
.51	.06	-.7526
.61	.06	-.5827
.71	.05	-.4404
0.00	-.01	-.0451
.11	-.02	-.0174
.21	-.02	-.0441
.31	-.02	-.0457
.40	-.02	.0004
.51	-.01	.0038
.61	-.01	.0349
.71	-.00	.0656

X/C	Z/C	CP
.11	.01	-.7660
.21	.00	-.7351
.31	.00	-.8690
.41	.01	-.8121
.51	.01	-.7231
.62	.01	-.5944
.71	.00	-.4548
.11	-.05	.0669
.22	-.04	.0556
.32	-.03	.0515
.42	-.03	.0499
.51	-.02	.0641
.62	-.01	.0889
.72	-.00	.1337

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17170

MACH .602

Q 20157.5

ALPW

2.55

BETA

0.00

P1 79366.84

PT1 101419.66

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5805	0.00	.01	.5197	0.00	-.01	.1286	.11	.01	-.8749
.05	.05	-.4746	.05	.03	-.5771	.11	.03	-.0554	.21	.00	-.7953
.10	.06	-.5107	.10	.04	-.6307	.20	.05	-.4289	.31	.00	-.9162
.15	.06	-.5104	.15	.05	-.6310	.31	.06	-.6996	.41	.01	-.8501
.20	.07	-.5150	.20	.06	-.6272	.40	.07	-.8969	.51	.01	-.7414
.25	.07	-.5322	.25	.06	-.6344	.51	.06	-.7775	.62	.01	-.6079
.30	.07	-.5319	.30	.07	-.6441	.61	.06	-.6091	.71	.00	-.4657
.35	.07	-.5379	.35	.07	-.6404	.71	.05	-.4519	.11	-.05	.1086
.40	.07	-.5399	.40	.07	-.6358	0.00	-.01	-.1418	.22	-.04	.0812
.45	.07	-.5134	.45	.07	-.6096	.11	-.02	-.0071	.32	-.03	.0684
.50	.07	-.4829	.50	.07	-.5669	.21	-.02	-.0316	.42	-.03	.0618
.55	.06	-.4480	.55	.06	-.5157	.31	-.02	-.0331	.51	-.02	.0734
.60	.06	-.4096	.60	.06	-.4830	.40	-.02	.0071	.62	-.01	.0957
.65	.05	-.3645	.65	.05	-.4244	.51	-.01	.0130	.72	-.00	.1349
.70	.05	-.3203	.70	.05	-.3726	.61	-.01	.0385			
.75	.04	-.2818	.75	.04	-.3189	.71	-.00	.0699			
.80	.03	-.2295	.80	.04	-.2615						
.85	.03	-.1824	.85	.03	-.2076						
.90	.02	-.1196	0.00	.01	.5755						
0.00	.03	.4745	.04	-.00	.0338						
.05	.01	.0376	.09	-.01	.0342						
.10	.01	-.0033	.14	-.01	.0318						
.15	.00	-.0244	.19	-.01	.0338						
.20	-.00	-.0437	.24	-.01	.0092						
.25	-.00	-.0626	.29	-.01	-.0025						
.30	-.01	-.0619	.34	-.01	-.0051						
.35	-.01	-.0676	.39	-.01	-.0103						
.40	-.01	-.0697	.44	-.01	-.0107						
.45	-.01	-.0872	.49	-.01	.0048						
.50	-.01	-.0884	.54	-.01	.0212						
.55	-.01	-.0817	.59	-.01	.0351						
.60	-.01	-.0677	.64	-.00	.0534						
.65	-.01	-.0467	.69	-.00	.0867						
.70	-.00	-.0229	.74	.00	.0900						
.75	-.00	-.0046	.79	.00	.0978						
.80	-.00	.0203	.84	.00	.1107						
.85	.00	.0422									
.90	.00	.1146									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17171

MACH .602

Q 20131.0

ALPW

3.03

BETA

0.00

P1 79392.94

PT1 101413.53

Y/R/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5417
.05	.05	-.5499
.10	.06	-.5673
.15	.06	-.5599
.20	.07	-.5559
.25	.07	-.5610
.30	.07	-.5693
.35	.07	-.5613
.40	.07	-.5658
.45	.07	-.5333
.50	.07	-.4951
.55	.06	-.4659
.60	.06	-.4171
.65	.05	-.3781
.70	.05	-.3328
.75	.04	-.2871
.80	.03	-.2353
.85	.03	-.1832
.90	.02	-.1229
0.00	.03	.3870
.05	.01	.0792
.10	.01	.0305
.15	.00	.0007
.20	-.00	-.0184
.25	-.00	-.0389
.30	-.01	-.0424
.35	-.01	-.0486
.40	-.01	-.0504
.45	-.01	-.0739
.50	-.01	-.0713
.55	-.01	-.0611
.60	-.01	-.0535
.65	-.01	-.0349
.70	-.00	-.0167
.75	-.00	.0011
.80	-.00	.0223
.85	.00	.0461
.90	.00	.1164

X/C	Z/C	CP
0.00	.01	.4311
.05	.03	-.6911
.10	.04	-.7064
.15	.05	-.7035
.20	.06	-.6886
.25	.06	-.6830
.30	.07	-.6808
.35	.07	-.6745
.40	.07	-.6675
.45	.07	-.6350
.50	.07	-.5894
.55	.06	-.5354
.60	.06	-.4936
.65	.05	-.4364
.70	.05	-.3800
.75	.04	-.3280
.80	.04	-.2690
.85	.03	-.2079
0.00	.01	.4918
.04	-.00	.0371
.09	-.01	.0634
.14	-.01	.0685
.19	-.01	.0645
.24	-.01	.0345
.29	-.01	.0248
.34	-.01	.0128
.39	-.01	.0073
.44	-.01	.0079
.49	-.01	.0194
.54	-.01	.0338
.59	-.01	.0495
.64	-.00	.0641
.69	-.00	.0948
.74	.00	.0960
.79	.00	.1074
.84	.00	.1182

X/C	Z/C	CP
0.00	-.01	.1368
.11	.03	-.1584
.20	.05	-.5818
.31	.06	-.8004
.40	.07	-.9385
.51	.06	-.8095
.61	.06	-.6243
.71	.05	-.4672
0.00	-.01	-.2597
.11	-.02	.0048
.21	-.02	-.0210
.31	-.02	-.0122
.40	-.02	.0163
.51	-.01	.0177
.61	-.01	.0447
.71	-.00	.0701

X/C	Z/C	CP
.11	.01	-.9548
.21	.00	-.8740
.31	.00	-.9566
.41	.01	-.8851
.51	.01	-.7594
.62	.01	-.6202
.71	.00	-.4678
.11	-.05	.1433
.22	-.04	.1003
.32	-.03	.0859
.42	-.03	.0741
.51	-.02	.0826
.62	-.01	.0985
.72	-.00	.1379

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17172

MACH .603

Q 20166.6

ALPW

4.05

BETA

0.00

P1 79340.69

PT1 101405.00

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.4191	0.00	.01	.1559	0.00	-.01	.1399	.11	.01	-1.1263
.05	.05	-.7136	.05	.03	-.8848	.11	.03	-.3665	.21	.00	-.9748
.10	.06	-.6805	.10	.04	-.8556	.20	.05	-.6762	.31	.00	-1.0245
.15	.06	-.6423	.15	.05	-.8006	.31	.06	-.9027	.41	.01	-.9178
.20	.07	-.6187	.20	.06	-.7682	.40	.07	-1.0031	.51	.01	-.7601
.25	.07	-.6035	.25	.06	-.7554	.51	.06	-.8534	.62	.01	-.6150
.30	.07	-.6154	.30	.07	-.7534	.61	.06	-.6523	.71	.00	-.4632
.35	.07	-.6109	.35	.07	-.7229	.71	.05	-.4868	.11	-.05	.1987
.40	.07	-.6026	.40	.07	-.7212	0.00	-.01	-.5704	.22	-.04	.1391
.45	.07	-.5778	.45	.07	-.6780	.11	-.02	.0051	.32	-.03	.1097
.50	.07	-.5395	.50	.07	-.6316	.21	-.02	-.0097	.42	-.03	.0915
.55	.06	-.4935	.55	.06	-.5727	.31	-.02	-.0040	.51	-.02	.0949
.60	.06	-.4481	.60	.06	-.5158	.40	-.02	.0169	.62	-.01	.1059
.65	.05	-.3981	.65	.05	-.5101	.51	-.01	.0240	.72	-.00	.1329
.70	.05	-.3443	.70	.05	-.3944	.61	-.01	.0499			
.75	.04	-.3024	.75	.04	-.3269	.71	-.00	.0692			
.80	.03	-.2451	.80	.04	-.2667						
.85	.03	-.1889	.85	.03	-.2044						
.90	.02	-.1235	0.00	.01	.1504						
0.00	.03	.1771	.04	-.00	.0532						
.05	.01	.1601	.09	-.01	.1726						
.10	.01	.0947	.14	-.01	.1320						
.15	.00	.0537	.19	-.01	.1285						
.20	-.00	.0497	.24	-.01	.0827						
.25	-.00	.0045	.29	-.01	.0616						
.30	-.01	.0096	.34	-.01	.0522						
.35	-.01	-.0018	.39	-.01	.0389						
.40	-.01	-.0191	.44	-.01	.0355						
.45	-.01	-.0451	.49	-.01	.0411						
.50	-.01	-.0471	.54	-.01	.0539						
.55	-.01	-.0364	.59	-.01	.0680						
.60	-.01	-.0310	.64	-.00	.0815						
.65	-.01	-.0205	.69	-.00	.1035						
.70	-.00	-.0007	.74	.00	.1027						
.75	-.00	.0217	.79	.00	.1141						
.80	-.00	.0412	.84	.00	.1239						
.85	.00	.0608									
.90	.00	.0823									

7 X 10 HIGH SPEED TUNNEL

TP 17173

PT1 101395.11

$$Y/B/2 = 1.011$$

X/C	Z/C	CP
.11	.01	-1.1732
.21	.00	-.9479
.31	.00	-.9977
.41	.01	-.8170
.51	.01	-.6314
.62	.01	-.4606
.71	.00	-.3257
.11	-.05	.2479
.22	-.04	.1656
.32	-.03	.1234
.42	-.03	.0976
.51	-.02	.0926
.62	-.01	.0904
.72	-.00	.1056

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 18

TP 17174

MACH .603

Q 20171.6

ALPW

.03

BETA

0.00

P1 79320.24

PT1 101391.04

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5289
.05	.05	-.1536
.10	.06	-.2559
.15	.06	-.2994
.20	.07	-.3388
.25	.07	-.3698
.30	.07	-.3876
.35	.07	-.4058
.40	.07	-.4181
.45	.07	-.4061
.50	.07	-.3887
.55	.06	-.3697
.60	.06	-.3382
.65	.05	-.3070
.70	.05	-.2696
.75	.04	-.2424
.80	.03	-.1985
.85	.03	-.1589
.90	.02	-.1045
0.00	.03	.5999
.05	.01	-.2428
.10	.01	-.1881
.15	.00	-.1725
.20	-.00	-.1785
.25	-.00	-.1772
.30	-.01	-.1767
.35	-.01	-.1770
.40	-.01	-.1758
.45	-.01	-.1750
.50	-.01	-.1784
.55	-.01	-.1603
.60	-.01	-.1374
.65	-.01	-.1154
.70	-.00	-.0862
.75	-.00	-.0635
.80	-.00	-.0299
.85	.00	.0012
.90	.00	.0324

X/C	Z/C	CP
0.00	.01	.6105
.05	.03	-.1280
.10	.04	-.2642
.15	.05	-.3291
.20	.06	-.3756
.25	.06	-.4129
.30	.07	-.4409
.35	.07	-.4575
.40	.07	-.4807
.45	.07	-.4648
.50	.07	-.4416
.55	.06	-.4193
.60	.06	-.3940
.65	.05	-.3492
.70	.05	-.3105
.75	.04	-.2642
.80	.04	-.2233
.85	.03	-.1800
0.00	.01	.5076
.04	-.00	.0658
.09	-.01	-.1791
.14	-.01	-.1442
.19	-.01	-.1466
.24	-.01	-.1284
.29	-.01	-.1216
.34	-.01	-.1127
.39	-.01	-.1135
.44	-.01	-.0934
.49	-.01	-.0674
.54	-.01	-.0488
.59	-.01	-.0208
.64	-.00	-.0004
.69	-.00	.0353
.74	.00	.0415
.79	.00	.0551
.84	.00	.0687

X/C	Z/C	CP
0.00	-.01	.0970
.11	.03	.0977
.20	.05	-.1495
.31	.06	-.4024
.40	.07	-.6490
.51	.06	-.6106
.61	.06	-.4967
.71	.05	-.3749
0.00	-.01	.1270
.11	-.02	-.1831
.21	-.02	-.0524
.31	-.02	-.0517
.40	-.02	-.0539
.51	-.01	-.0390
.61	-.01	.0083
.71	-.00	.0585

X/C	Z/C	CP
.11	.01	-.4319
.21	.00	-.4718
.31	.00	-.6713
.41	.01	-.6673
.51	.01	-.6187
.62	.01	-.5260
.71	.00	-.4070
.11	-.05	-.0537
.22	-.04	-.0364
.32	-.03	-.0136
.42	-.03	.0019
.51	-.02	.0268
.62	-.01	.0647
.72	-.00	.1136

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17191

MACH .806

Q 30200.0

ALPW

-2.05

BETA

0.00

P1 66375.65

PT1 101805.83

Y/B/2 = .31

$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.2060
.05	.05	.0895
.10	.06	-.0718
.15	.06	-.1504
.20	.07	-.2075
.25	.07	-.2696
.30	.07	-.3083
.35	.07	-.3558
.40	.07	-.4105
.45	.07	-.4300
.50	.07	-.4209
.55	.06	-.4091
.60	.06	-.3829
.65	.05	-.3506
.70	.05	-.3048
.75	.04	-.2739
.80	.03	-.2199
.85	.03	-.1710
.90	.02	-.1083
0.00	.03	.0365
.05	.01	-.5646
.10	.01	-.5237
.15	.00	-.4528
.20	-.00	-.4105
.25	-.00	-.3911
.30	-.01	-.3787
.35	-.01	-.3511
.40	-.01	-.3468
.45	-.01	-.3394
.50	-.01	-.3239
.55	-.01	-.2968
.60	-.01	-.2491
.65	-.01	-.2117
.70	-.00	-.1699
.75	-.00	-.0957
.80	-.00	-.0666
.85	.00	-.0148
.90	.00	.0717

X/C	Z/C	CP
0.00	.01	.3838
.05	.03	.1528
.10	.04	-.0402
.15	.05	-.1457
.20	.06	-.2300
.25	.06	-.2906
.30	.07	-.3559
.35	.07	-.4050
.40	.07	-.4572
.45	.07	-.4677
.50	.07	-.4613
.55	.06	-.4541
.60	.06	-.4022
.65	.05	-.4126
.70	.05	-.3783
.75	.04	-.3405
.80	.04	-.2228
.85	.03	-.2222
0.00	.01	.3890
.04	-.00	.0199
.09	-.01	-.6698
.14	-.01	-.5639
.19	-.01	-.4658
.24	-.01	-.3808
.29	-.01	-.3139
.34	-.01	-.2655
.39	-.01	-.2335
.44	-.01	-.1942
.49	-.01	-.1596
.54	-.01	-.1200
.59	-.01	-.0777
.64	-.00	-.0872
.69	-.00	-.0074
.74	.00	.0146
.79	.00	.0245
.84	.00	.0443

X/C	Z/C	CP
0.00	-.01	-.0666
.11	.03	-.2509
.20	.05	-.2090
.31	.06	-.2954
.40	.07	-.4032
.51	.06	-.4816
.61	.06	-.3857
.71	.05	-.2842
0.00	-.01	-.0485
.11	-.02	-.4363
.21	-.02	-.3653
.31	-.02	-.3625
.40	-.02	-.2412
.51	-.01	-.1865
.61	-.01	-.1233
.71	-.00	-.0743

X/C	Z/C	CP
.11	.01	-.0745
.21	.00	-.1056
.31	.00	-.4701
.41	.01	-.5557
.51	.01	-.5740
.62	.01	-.4332
.71	.00	-.2858
.11	-.05	-.6359
.22	-.04	-.4329
.32	-.03	-.3062
.42	-.03	-.3159
.51	-.02	-.1410
.62	-.01	-.0637
.72	-.00	.0028

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17192

MACH .805

Q 30142.7

ALPW

-1.47

BETA

0.00

P1 66462.01

PT1 101807.36

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.3080	0.00	.01	.4571	0.00	-.01	.0954	.11	.01	-.1363
.05	.05	.0410	.05	.03	.0913	.11	.03	-.1109	.21	.00	-.1174
.10	.06	-.1186	.10	.04	-.0978	.20	.05	-.1898	.31	.00	-.5392
.15	.06	-.1936	.15	.05	-.2130	.31	.06	-.2868	.41	.01	-.5972
.20	.07	-.2486	.20	.06	-.2833	.40	.07	-.4537	.51	.01	-.6273
.25	.07	-.3119	.25	.06	-.3500	.51	.06	-.5457	.62	.01	-.4538
.30	.07	-.3535	.30	.07	-.4108	.61	.06	-.4105	.71	.00	-.2921
.35	.07	-.3890	.35	.07	-.4641	.71	.05	-.2927	.11	-.05	-.4853
.40	.07	-.4461	.40	.07	-.5034	0.00	-.01	-.0255	.22	-.04	-.2951
.45	.07	-.4633	.45	.07	-.5200	.11	-.02	-.3896	.32	-.03	-.1942
.50	.07	-.4535	.50	.07	-.4847	.21	-.02	-.3014	.42	-.03	-.2620
.55	.06	-.4402	.55	.06	-.4747	.31	-.02	-.2988	.51	-.02	-.0920
.60	.06	-.4099	.60	.06	-.4277	.40	-.02	-.1969	.62	-.01	-.0241
.65	.05	-.3635	.65	.05	-.4261	.51	-.01	-.2009	.72	-.00	.0389
.70	.05	-.3203	.70	.05	-.3988	.61	-.01	-.0981			
.75	.04	-.2877	.75	.04	-.3580	.71	-.00	-.0502			
.80	.03	-.2281	.80	.04	-.2297						
.85	.03	-.1781	.85	.03	-.2292						
.90	.02	-.1116	0.00	.01	.4434						
0.00	.03	.2002	.04	-.00	.0566						
.05	.01	-.4832	.09	-.01	-.5562						
.10	.01	-.3673	.14	-.01	-.4229						
.15	.00	-.3707	.19	-.01	-.3347						
.20	-.00	-.3470	.24	-.01	-.2796						
.25	-.00	-.3255	.29	-.01	-.2513						
.30	-.01	-.3165	.34	-.01	-.2211						
.35	-.01	-.3228	.39	-.01	-.1995						
.40	-.01	-.3115	.44	-.01	-.1710						
.45	-.01	-.3136	.49	-.01	-.1322						
.50	-.01	-.2881	.54	-.01	-.0972						
.55	-.01	-.2588	.59	-.01	-.0609						
.60	-.01	-.2260	.64	-.00	-.0589						
.65	-.01	-.1897	.69	-.00	.0126						
.70	-.00	-.1414	.74	.00	.0166						
.75	-.00	-.0932	.79	.00	.0358						
.80	-.00	-.0556	.84	.00	.0679						
.85	.00	-.0126									
.90	.00	.0796									

7 X 10 HIGH SPEED TUNNEL

RUN

19

TP 17193

MACH .806

Q 30175.7

ALPW

- 89

BETA

0.00

P1 66413.93

PT1 101807.94

$$Y/B/2 = .31$$

Y/B/2 = .74

Y/B/2 = 1.003

$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.3855
.05	.05	-.0196
.10	.06	-.1690
.15	.06	-.2382
.20	.07	-.2959
.25	.07	-.3536
.30	.07	-.3938
.35	.07	-.4379
.40	.07	-.4751
.45	.07	-.5080
.50	.07	-.4949
.55	.06	-.4745
.60	.06	-.4269
.65	.05	-.3883
.70	.05	-.3367
.75	.04	-.3002
.80	.03	-.2387
.85	.03	-.1847
.90	.02	-.1150
0.00	.03	.3637
.05	.01	-.4160
.10	.01	-.3154
.15	.00	-.2940
.20	-.00	-.2931
.25	-.00	-.2969
.30	-.01	-.2939
.35	-.01	-.2804
.40	-.01	-.2910
.45	-.01	-.2801
.50	-.01	-.2853
.55	-.01	-.2397
.60	-.01	-.2178
.65	-.01	-.1597
.70	-.00	-.1262
.75	-.00	-.0744
.80	-.00	-.0365
.85	.00	.0014
.90	.00	.0809

X/C	Z/C	CP
0.00	.01	.5286
.05	.03	.0232
.10	.04	-.1749
.15	.05	-.2807
.20	.06	-.3377
.25	.06	-.4057
.30	.07	-.4663
.35	.07	-.5122
.40	.07	-.5461
.45	.07	-.5774
.50	.07	-.5517
.55	.06	-.5002
.60	.06	-.4563
.65	.05	-.4508
.70	.05	-.4084
.75	.04	-.3736
.80	.04	-.2384
.85	.03	-.2455
0.00	.01	.5160
.04	-.00	.0333
.09	-.01	-.4064
.14	-.01	-.3164
.19	-.01	-.2628
.24	-.01	-.2384
.29	-.01	-.2125
.34	-.01	-.1946
.39	-.01	-.1762
.44	-.01	-.1548
.49	-.01	-.1183
.54	-.01	-.0838
.59	-.01	-.0484
.64	-.00	-.0518
.69	-.00	.0239
.74	.00	.0252
.79	.00	.0530
.84	.00	.0684

X/C	Z/C	CP
0.00	-.01	.1068
.11	.03	-.0744
.20	.05	-.2536
.31	.06	-.3605
.40	.07	-.5066
.51	.06	-.6166
.61	.06	-.4348
.71	.05	-.3154
0.00	-.01	-.0001
.11	-.02	-.2997
.21	-.02	-.2235
.31	-.02	-.2263
.40	-.02	-.1697
.51	-.01	-.1697
.61	-.01	-.0864
.71	-.00	-.0445

X/C	Z/C	CP
.11	.01	-.2075
.21	.00	-.1230
.31	.00	-.6126
.41	.01	-.6554
.51	.01	-.6517
.62	.01	-.4672
.71	.00	-.3002
.11	-.05	-.2454
.22	-.04	-.1858
.32	-.03	-.1475
.42	-.03	-.2047
.51	-.02	-.0697
.62	-.01	-.0042
.72	-.00	.0722

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17194

MACH .807

Q 30220.8

ALPW

-.50

BETA

0.00

P1 66338.68

PT1 101800.29

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.4591	0.00	.01	.5763	0.00	-.01	.1087	.11	.01	-.2787
.05	.05	-.0555	.05	.03	-.0297	.11	.03	-.0412	.21	.00	-.1304
.10	.06	-.1988	.10	.04	-.2221	.20	.05	-.2716	.31	.00	-.6583
.15	.06	-.2696	.15	.05	-.3220	.31	.06	-.3888	.41	.01	-.7054
.20	.07	-.3221	.20	.06	-.3894	.40	.07	-.5916	.51	.01	-.6691
.25	.07	-.3803	.25	.06	-.4511	.51	.06	-.6597	.62	.01	-.4801
.30	.07	-.4193	.30	.07	-.5097	.61	.06	-.4568	.71	.00	-.3088
.35	.07	-.4636	.35	.07	-.5565	.71	.05	-.3263	.11	-.05	-.1623
.40	.07	-.5077	.40	.07	-.5850	0.00	-.01	-.0058	.22	-.04	-.1574
.45	.07	-.5350	.45	.07	-.6105	.11	-.02	-.3048	.32	-.03	-.1228
.50	.07	-.5284	.50	.07	-.5850	.21	-.02	-.2147	.42	-.03	-.1656
.55	.06	-.4950	.55	.06	-.5237	.31	-.02	-.2123	.51	-.02	-.0593
.60	.06	-.4526	.60	.06	-.4681	.40	-.02	-.1511	.62	-.01	.0050
.65	.05	-.4053	.65	.05	-.4629	.51	-.01	-.1469	.72	-.00	.0804
.70	.05	-.3460	.70	.05	-.4355	.61	-.01	-.0763			
.75	.04	-.3033	.75	.04	-.3912	.71	-.00	-.0324			
.80	.03	-.2430	.80	.04	-.2432						
.85	.03	-.1881	.85	.03	-.2414						
.90	.02	-.1171	0.00	.01	.5723						
0.00	.03	.5447	.04	-.00	.0392						
.05	.01	-.3732	.09	-.01	-.3056						
.10	.01	-.2852	.14	-.01	-.2551						
.15	.00	-.2660	.19	-.01	-.2304						
.20	-.00	-.2442	.24	-.01	-.2040						
.25	-.00	-.2610	.29	-.01	-.1883						
.30	-.01	-.2436	.34	-.01	-.1753						
.35	-.01	-.2556	.39	-.01	-.1589						
.40	-.01	-.2633	.44	-.01	-.1392						
.45	-.01	-.2641	.49	-.01	-.1060						
.50	-.01	-.2494	.54	-.01	-.0737						
.55	-.01	-.2243	.59	-.01	-.0382						
.60	-.01	-.2011	.64	-.00	-.0341						
.65	-.01	-.1613	.69	-.00	.0268						
.70	-.00	-.1184	.74	.00	.0300						
.75	-.00	-.0832	.79	.00	.0542						
.80	-.00	-.0414	.84	.00	.0833						
.85	.00	.0064									
.90	.00	.0995									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17195

MACH .806

Q 30194.3 ALPW

.06

BETA

0.00

P1 66370.36

PT1 101793.32

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5128
.05	.05	-.1271
.10	.06	-.2586
.15	.06	-.3107
.20	.07	-.3679
.25	.07	-.4170
.30	.07	-.4594
.35	.07	-.5049
.40	.07	-.5481
.45	.07	-.5816
.50	.07	-.5790
.55	.06	-.5339
.60	.06	-.4795
.65	.05	-.4152
.70	.05	-.3613
.75	.04	-.3180
.80	.03	-.2508
.85	.03	-.1911
.90	.02	-.1199
0.00	.03	.6018
.05	.01	-.3001
.10	.01	-.2411
.15	.00	-.2272
.20	-.00	-.2144
.25	-.00	-.2217
.30	-.01	-.2240
.35	-.01	-.2216
.40	-.01	-.2249
.45	-.01	-.2344
.50	-.01	-.2221
.55	-.01	-.2064
.60	-.01	-.1769
.65	-.01	-.1525
.70	-.00	-.0940
.75	-.00	-.0492
.80	-.00	-.0191
.85	.00	.0078
.90	.00	.0888

X/C	Z/C	CP
0.00	.01	.6162
.05	.03	-.1192
.10	.04	-.2988
.15	.05	-.4006
.20	.06	-.4545
.25	.06	-.5179
.30	.07	-.5777
.35	.07	-.6245
.40	.07	-.6777
.45	.07	-.6485
.50	.07	-.6441
.55	.06	-.5798
.60	.06	-.4863
.65	.05	-.4861
.70	.05	-.4449
.75	.04	-.3978
.80	.04	-.2511
.85	.03	-.2438
0.00	.01	.5832
.04	-.00	.0320
.09	-.01	-.2355
.14	-.01	-.1958
.19	-.01	-.1963
.24	-.01	-.1674
.29	-.01	-.1512
.34	-.01	-.1439
.39	-.01	-.1370
.44	-.01	-.1144
.49	-.01	-.0891
.54	-.01	-.0558
.59	-.01	-.0244
.64	-.00	-.0255
.69	-.00	.0415
.74	.00	.0463
.79	.00	.0634
.84	.00	.0924

X/C	Z/C	CP
0.00	-.01	.1152
.11	.03	-.0075
.20	.05	-.3060
.31	.06	-.4154
.40	.07	-.7076
.51	.06	-.7012
.61	.06	-.5042
.71	.05	-.3398
0.00	-.01	-.0199
.11	-.02	-.2122
.21	-.02	-.1722
.31	-.02	-.1605
.40	-.02	-.1176
.51	-.01	-.1173
.61	-.01	-.0644
.71	-.00	-.0231

X/C	Z/C	CP
.11	.01	-.3657
.21	.00	-.1341
.31	.00	-.7038
.41	.01	-.8590
.51	.01	-.6667
.62	.01	-.4939
.71	.00	-.3196
.11	-.05	-.1117
.22	-.04	-.1138
.32	-.03	-.0919
.42	-.03	-.1304
.51	-.02	-.0401
.62	-.01	.0197
.72	-.00	.0946

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17196

MACH .806

Q 30184.3

ALPW

.54

BETA

0.00

P1 66386.06

PT1 101794.21

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5564	0.00	.01	.6353	0.00	-.01	.1233	.11	.01	-.4378
.05	.05	-.1664	.05	.03	-.2022	.11	.03	.0055	.21	.00	-.1401
.10	.06	-.3014	.10	.04	-.3742	.20	.05	-.3913	.31	.00	-.8693
.15	.06	-.3641	.15	.05	-.4516	.31	.06	-.6514	.41	.01	-.9418
.20	.07	-.4044	.20	.06	-.5211	.40	.07	-.7490	.51	.01	-.6862
.25	.07	-.4500	.25	.06	-.5821	.51	.06	-.7987	.62	.01	-.4899
.30	.07	-.4885	.30	.07	-.6299	.61	.06	-.6311	.71	.00	-.3226
.35	.07	-.5338	.35	.07	-.6599	.71	.05	-.3693	.11	-.05	-.0923
.40	.07	-.5784	.40	.07	-.7783	0.00	-.01	-.0341	.22	-.04	-.0835
.45	.07	-.6133	.45	.07	-.6980	.11	-.02	-.1575	.32	-.03	-.0642
.50	.07	-.6062	.50	.07	-.6651	.21	-.02	-.1346	.42	-.03	-.1003
.55	.06	-.5906	.55	.06	-.6140	.31	-.02	-.1346	.51	-.02	-.0215
.60	.06	-.5203	.60	.06	-.5039	.40	-.02	-.0934	.62	-.01	.0209
.65	.05	-.4322	.65	.05	-.5065	.51	-.01	-.0973	.72	-.00	.1015
.70	.05	-.3694	.70	.05	-.4716	.61	-.01	-.0490			
.75	.04	-.3255	.75	.04	-.4211	.71	-.00	-.0170			
.80	.03	-.2578	.80	.04	-.2570						
.85	.03	-.1955	.85	.03	-.2615						
.90	.02	-.1209	0.00	.01	.5722						
0.00	.03	.6090	.04	-.00	.0597						
.05	.01	-.2423	.09	-.01	-.1688						
.10	.01	-.1967	.14	-.01	-.1436						
.15	.00	-.1957	.19	-.01	-.1260						
.20	-.00	-.1938	.24	-.01	-.1345						
.25	-.00	-.2057	.29	-.01	-.1236						
.30	-.01	-.2026	.34	-.01	-.1144						
.35	-.01	-.2103	.39	-.01	-.1151						
.40	-.01	-.2190	.44	-.01	-.0956						
.45	-.01	-.2147	.49	-.01	-.0697						
.50	-.01	-.2137	.54	-.01	-.0425						
.55	-.01	-.1875	.59	-.01	-.0104						
.60	-.01	-.1609	.64	-.00	-.0056						
.65	-.01	-.1217	.69	-.00	.0518						
.70	-.00	-.0844	.74	.00	.0504						
.75	-.00	-.0472	.79	.00	.0747						
.80	-.00	-.0223	.84	.00	.0911						
.85	.00	.0136									
.90	.00	.0940									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17197

MACH .806

Q 30194.4

ALPW

.99

BETA

0.00

P1 66368.81

PT1 101792.05

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5837
.05	.05	-.2302
.10	.06	-.3466
.15	.06	-.3962
.20	.07	-.4394
.25	.07	-.4833
.30	.07	-.5149
.35	.07	-.5636
.40	.07	-.6028
.45	.07	-.6496
.50	.07	-.6531
.55	.06	-.6184
.60	.06	-.5205
.65	.05	-.4549
.70	.05	-.3768
.75	.04	-.3293
.80	.03	-.2593
.85	.03	-.1967
.90	.02	-.1217
0.00	.03	.6137
.05	.01	-.1724
.10	.01	-.1710
.15	.00	-.1602
.20	-.00	-.1624
.25	-.00	-.1707
.30	-.01	-.1689
.35	-.01	-.1869
.40	-.01	-.1953
.45	-.01	-.1940
.50	-.01	-.1939
.55	-.01	-.1853
.60	-.01	-.1566
.65	-.01	-.1167
.70	-.00	-.0866
.75	-.00	-.0403
.80	-.00	-.0128
.85	.00	.0209
.90	.00	.0915

X/C	Z/C	CP
0.00	.01	.6427
.05	.03	-.2744
.10	.04	-.4403
.15	.05	-.5256
.20	.06	-.5780
.25	.06	-.6410
.30	.07	-.6916
.35	.07	-.7152
.40	.07	-.8093
.45	.07	-.8314
.50	.07	-.7621
.55	.06	-.5903
.60	.06	-.5177
.65	.05	-.5145
.70	.05	-.4777
.75	.04	-.4283
.80	.04	-.2595
.85	.03	-.2609
0.00	.01	.5481
.04	-.00	.0440
.09	-.01	-.1353
.14	-.01	-.1081
.19	-.01	-.1076
.24	-.01	-.1020
.29	-.01	-.0958
.34	-.01	-.0900
.39	-.01	-.0895
.44	-.01	-.0751
.49	-.01	-.0487
.54	-.01	-.0236
.59	-.01	.0042
.64	-.00	.0100
.69	-.00	.0612
.74	.00	.0595
.79	.00	.0848
.84	.00	.1053

X/C	Z/C	CP
0.00	-.01	.1224
.11	.03	.0052
.20	.05	-.4723
.31	.06	-.7354
.40	.07	-.7131
.51	.06	-.8239
.61	.06	-.7478
.71	.05	-.4169
0.00	-.01	-.0471
.11	-.02	-.1292
.21	-.02	-.1223
.31	-.02	-.1199
.40	-.02	-.0751
.51	-.01	-.0714
.61	-.01	-.0419
.71	-.00	-.0082

X/C	Z/C	CP
.11	.01	-.5195
.21	.00	-.1500
.31	.00	-.9382
.41	.01	-1.0543
.51	.01	-.9070
.62	.01	-.5093
.71	.00	-.3201
.11	-.05	-.0399
.22	-.04	-.0449
.32	-.03	-.0444
.42	-.03	-.0727
.51	-.02	-.0052
.62	-.01	.0454
.72	-.00	.0843

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17198

MACH .807

Q 30231.6

ALPW

1.46

BETA

0.00

P1 66314.33

PT1 101792.66

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6022	0.00	.01	.6430	0.00	-.01	.1403	.11	.01	-.6664
.05	.05	-.2836	.05	.03	-.3630	.11	.03	-.0193	.21	.00	-.1632
.10	.06	-.3929	.10	.04	-.5239	.20	.05	-.4354	.31	.00	-1.0053
.15	.06	-.4473	.15	.05	-.5976	.31	.06	-.7221	.41	.01	-1.1330
.20	.07	-.4750	.20	.06	-.6430	.40	.07	-.7139	.51	.01	-1.0810
.25	.07	-.5153	.25	.06	-.6969	.51	.06	-.8013	.62	.01	-.5791
.30	.07	-.5446	.30	.07	-.7608	.61	.06	-.8123	.71	.00	-.3406
.35	.07	-.5920	.35	.07	-.7957	.71	.05	-.4618	.11	-.05	.0147
.40	.07	-.6410	.40	.07	-.8426	0.00	-.01	-.1035	.22	-.04	-.0049
.45	.07	-.6924	.45	.07	-.8937	.11	-.02	-.1235	.32	-.03	-.0104
.50	.07	-.6968	.50	.07	-.8951	.21	-.02	-.1060	.42	-.03	-.0756
.55	.06	-.6950	.55	.06	-.6492	.31	-.02	-.0978	.51	-.02	.0111
.60	.06	-.6467	.60	.06	-.5019	.40	-.02	-.0568	.62	-.01	.0570
.65	.05	-.4683	.65	.05	-.4975	.51	-.01	-.0547	.72	-.00	.0999
.70	.05	-.3837	.70	.05	-.4650	.61	-.01	-.0328			
.75	.04	-.3343	.75	.04	-.4184	.71	-.00	.0001			
.80	.03	-.2573	.80	.04	-.2576						
.85	.03	-.1979	.85	.03	-.2564						
.90	.02	-.1214	0.00	.01	.4051						
0.00	.03	.5946	.04	-.00	.0704						
.05	.01	-.1300	.09	-.01	-.0865						
.10	.01	-.1297	.14	-.01	-.0784						
.15	.00	-.1333	.19	-.01	-.0767						
.20	-.00	-.1304	.24	-.01	-.0737						
.25	-.00	-.1523	.29	-.01	-.0758						
.30	-.01	-.1541	.34	-.01	-.0756						
.35	-.01	-.1582	.39	-.01	-.0726						
.40	-.01	-.1668	.44	-.01	-.0644						
.45	-.01	-.1765	.49	-.01	-.0404						
.50	-.01	-.1763	.54	-.01	-.0170						
.55	-.01	-.1594	.59	-.01	.0138						
.60	-.01	-.1347	.64	-.00	.0132						
.65	-.01	-.1079	.69	-.00	.0725						
.70	-.00	-.0725	.74	.00	.0767						
.75	-.00	-.0380	.79	.00	.0946						
.80	-.00	-.0020	.84	.00	.1165						
.85	.00	.0329									
.90	.00	.0824									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17199

MACH .807

Q

30242.1

ALPW

2.03

BETA

0.00

P1 66305.60

PT1 101798.93

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6113
.05	.05	-.3605
.10	.06	-.4584
.15	.06	-.4909
.20	.07	-.5170
.25	.07	-.5568
.30	.07	-.5848
.35	.07	-.6242
.40	.07	-.6739
.45	.07	-.7218
.50	.07	-.7447
.55	.06	-.7315
.60	.06	-.7277
.65	.05	-.6109
.70	.05	-.3917
.75	.04	-.3341
.80	.03	-.2657
.85	.03	-.1967
.90	.02	-.1198
0.00	.03	.5917
.05	.01	-.0625
.10	.01	-.0833
.15	.00	-.0759
.20	-.00	-.0751
.25	-.00	-.1299
.30	-.01	-.1272
.35	-.01	-.1406
.40	-.01	-.1487
.45	-.01	-.1470
.50	-.01	-.1466
.55	-.01	-.1400
.60	-.01	-.1153
.65	-.01	-.0839
.70	-.00	-.0572
.75	-.00	-.0277
.80	-.00	.0049
.85	.00	.0404
.90	.00	.0755

X/C	Z/C	CP
0.00	.01	.6285
.05	.03	-.4543
.10	.04	-.6181
.15	.05	-.6745
.20	.06	-.7090
.25	.06	-.7670
.30	.07	-.8232
.35	.07	-.8662
.40	.07	-.9315
.45	.07	-.9959
.50	.07	-.9834
.55	.06	-.8935
.60	.06	-.5439
.65	.05	-.5325
.70	.05	-.4732
.75	.04	-.4127
.80	.04	-.2460
.85	.03	-.2438
0.00	.01	.2266
.04	-.00	.0727
.09	-.01	-.0207
.14	-.01	-.0324
.19	-.01	-.0325
.24	-.01	-.0412
.29	-.01	-.0415
.34	-.01	-.0471
.39	-.01	-.0475
.44	-.01	-.0415
.49	-.01	-.0215
.54	-.01	.0004
.59	-.01	.0244
.64	-.00	.0238
.69	-.00	.0906
.74	.00	.0874
.79	.00	.1077
.84	.00	.1265

X/C	Z/C	CP
0.00	-.01	.1453
.11	.03	-.0635
.20	.05	-.4477
.31	.06	-.7350
.40	.07	-.8308
.51	.06	-.8620
.61	.06	-.8341
.71	.05	-.4650
0.00	-.01	-.2076
.11	-.02	-.1091
.21	-.02	-.0883
.31	-.02	-.0899
.40	-.02	-.0407
.51	-.01	-.0393
.61	-.01	-.0226
.71	-.00	.0005

X/C	Z/C	CP
.11	.01	-.8382
.21	.00	-.1930
.31	.00	-1.0544
.41	.01	-1.1511
.51	.01	-1.0546
.62	.01	-.7117
.71	.00	-.4331
.11	-.05	.0817
.22	-.04	.0424
.32	-.03	.0249
.42	-.03	-.0403
.51	-.02	.0286
.62	-.01	.0682
.72	-.00	.1151

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17200

MACH .806

Q 30199.5

ALPW

2.56

BETA

0.00

P1 66364.47

PT1 101794.97

Y/B/2 = .21

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6137	0.00	.01	.5983	0.00	-.01	.1540	.11	.01	-1.0293
.05	.05	-.4280	.05	.03	-.5644	.11	.03	-.1255	.21	.00	-.2158
.10	.06	-.5195	.10	.04	-.7041	.20	.05	-.5696	.31	.00	-1.0641
.15	.06	-.5411	.15	.05	-.7615	.31	.06	-.7830	.41	.01	-1.0716
.20	.07	-.5621	.20	.06	-.7779	.40	.07	-1.0104	.51	.01	-.8173
.25	.07	-.6086	.25	.06	-.8233	.51	.06	-.9435	.62	.01	-.6337
.30	.07	-.6253	.30	.07	-.8840	.61	.06	-.8470	.71	.00	-.4904
.35	.07	-.6485	.35	.07	-.9232	.71	.05	-.4627	.11	-.05	.1237
.40	.07	-.6975	.40	.07	-.9739	0.00	-.01	-.3263	.22	-.04	.0729
.45	.07	-.7516	.45	.07	-1.0468	.11	-.02	-.1064	.32	-.03	.0474
.50	.07	-.7692	.50	.07	-1.0596	.21	-.02	-.1081	.42	-.03	-.0068
.55	.06	-.7730	.55	.06	-1.0319	.31	-.02	-.0904	.51	-.02	.0449
.60	.06	-.7686	.60	.06	-.6346	.40	-.02	-.0302	.62	-.01	.0787
.65	.05	-.7053	.65	.05	-.7358	.51	-.01	-.0324	.72	-.00	.1223
.70	.05	-.4220	.70	.05	-.5649	.61	-.01	-.0141			
.75	.04	-.3355	.75	.04	-.4561	.71	-.00	.0001			
.80	.03	-.2609	.80	.04	-.2384						
.85	.03	-.1921	.85	.03	-.2396						
.90	.02	-.1184	0.00	.01	.4642						
0.00	.03	.5565	.04	-.00	.0570						
.05	.01	-.0039	.09	-.01	.0258						
.10	.01	-.0226	.14	-.01	.0099						
.15	.00	-.0597	.19	-.01	.0167						
.20	-.00	-.0587	.24	-.01	-.0093						
.25	-.00	-.0968	.29	-.01	-.0168						
.30	-.01	-.1179	.34	-.01	-.0232						
.35	-.01	-.1023	.39	-.01	-.0216						
.40	-.01	-.1162	.44	-.01	-.0211						
.45	-.01	-.1350	.49	-.01	-.0017						
.50	-.01	-.1332	.54	-.01	.0154						
.55	-.01	-.1176	.59	-.01	.0365						
.60	-.01	-.0966	.64	-.00	.0249						
.65	-.01	-.0787	.69	-.00	.0987						
.70	-.00	-.0451	.74	.00	.0966						
.75	-.00	-.0188	.79	.00	.1054						
.80	-.00	.0128	.84	.00	.1253						
.85	.00	.0417									
.90	.00	.0711									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17201

MACH .307

Q 30211.3

ALPW

3.06

BETA

0.00

P1 66345.23

PT1 101793.40

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6021
.05	.05	-.4919
.10	.06	-.5528
.15	.06	-.5817
.20	.07	-.6006
.25	.07	-.6390
.30	.07	-.6672
.35	.07	-.6902
.40	.07	-.7171
.45	.07	-.7725
.50	.07	-.7907
.55	.06	-.7993
.60	.06	-.7998
.65	.05	-.7720
.70	.05	-.4970
.75	.04	-.3374
.80	.03	-.2605
.85	.03	-.1938
.90	.02	-.1154
0.00	.03	.5168
.05	.01	.0390
.10	.01	-.0034
.15	.00	-.0186
.20	-.00	-.0213
.25	-.00	-.0751
.30	-.01	-.0619
.35	-.01	-.0808
.40	-.01	-.0841
.45	-.01	-.1066
.50	-.01	-.1063
.55	-.01	-.0972
.60	-.01	-.0850
.65	-.01	-.0514
.70	-.00	-.0243
.75	-.00	-.0063
.80	-.00	.0178
.85	.00	.0520
.90	.00	.0758

X/C	Z/C	CP
0.00	.01	.5501
.05	.03	-.6471
.10	.04	-.7796
.15	.05	-.8479
.20	.06	-.8457
.25	.06	-.8898
.30	.07	-.9377
.35	.07	-.9662
.40	.07	-1.0197
.45	.07	-1.0811
.50	.07	-1.1023
.55	.06	-1.0829
.60	.06	-.7452
.65	.05	-.7176
.70	.05	-.6112
.75	.04	-.4736
.80	.04	-.2371
.85	.03	-.2244
0.00	.01	.5002
.04	-.00	.0462
.09	-.01	.0729
.14	-.01	.0457
.19	-.01	.0439
.24	-.01	.0222
.29	-.01	.0115
.34	-.01	-.0000
.39	-.01	-.0044
.44	-.01	-.0024
.49	-.01	.0136
.54	-.01	.0304
.59	-.01	.0487
.64	-.00	.0509
.69	-.00	.1001
.74	.00	.1136
.79	.00	.1179
.84	.00	.1404

X/C	Z/C	CP
0.00	-.01	.1580
.11	.03	-.1811
.20	.05	-.6036
.31	.06	-.8085
.40	.07	-1.0758
.51	.06	-.9371
.61	.06	-.8486
.71	.05	-.4450
0.00	-.01	-.4759
.11	-.02	-.1054
.21	-.02	-.0813
.31	-.02	-.0806
.40	-.02	-.0237
.51	-.01	-.0242
.61	-.01	-.0154
.71	-.00	.0047

X/C	Z/C	CP
.11	.01	-1.1291
.21	.00	-.2287
.31	.00	-1.0554
.41	.01	-.9666
.51	.01	-.7450
.62	.01	-.6411
.71	.00	-.5488
.11	-.05	.1570
.22	-.04	.0979
.32	-.03	.0703
.42	-.03	.0219
.51	-.02	.0549
.62	-.01	.0827
.72	-.00	.1225

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17202

MACH .805

Q 30155.1 ALPW

3.98

BETA

0.00

P1 66424.97

PT1 101790.10

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5561
.05	.05	-.6131
.10	.06	-.6669
.15	.06	-.6822
.20	.07	-.6825
.25	.07	-.6997
.30	.07	-.7470
.35	.07	-.7594
.40	.07	-.7937
.45	.07	-.8155
.50	.07	-.8289
.55	.06	-.8386
.60	.06	-.8477
.65	.05	-.8530
.70	.05	-.5912
.75	.04	-.3577
.80	.03	-.2643
.85	.03	-.1890
.90	.02	-.1107
0.00	.03	.4143
.05	.01	.1137
.10	.01	.0583
.15	.00	.0583
.20	-.00	.0401
.25	-.00	-.0286
.30	-.01	-.0271
.35	-.01	-.0464
.40	-.01	-.0492
.45	-.01	-.0701
.50	-.01	-.0740
.55	-.01	-.0608
.60	-.01	-.0479
.65	-.01	-.0392
.70	-.00	-.0169
.75	-.00	.0075
.80	-.00	.0393
.85	.00	.0659
.90	.00	.0995

X/C	Z/C	CP
0.00	.01	.4440
.05	.03	-.8185
.10	.04	-.9158
.15	.05	-.9868
.20	.06	-1.0258
.25	.06	-1.0375
.30	.07	-1.0605
.35	.07	-1.0623
.40	.07	-1.0997
.45	.07	-1.1534
.50	.07	-1.1083
.55	.06	-.8396
.60	.06	-.6684
.65	.05	-.6632
.70	.05	-.6187
.75	.04	-.5460
.80	.04	-.2820
.85	.03	-.2476
0.00	.01	.2950
.04	-.00	.0495
.09	-.01	.1412
.14	-.01	.1109
.19	-.01	.1180
.24	-.01	.0654
.29	-.01	.0492
.34	-.01	.0380
.39	-.01	.0291
.44	-.01	.0265
.49	-.01	.0382
.54	-.01	.0519
.59	-.01	.0690
.64	-.00	.0723
.69	-.00	.1137
.74	.00	.1202
.79	.00	.1263
.84	.00	.1445

X/C	Z/C	CP
0.00	-.01	.1628
.11	.03	-.2923
.20	.05	-.7380
.31	.06	-.9176
.40	.07	-.7898
.51	.06	-.9082
.61	.06	-.7008
.71	.05	-.4320
0.00	-.01	-.8197
.11	-.02	-.1164
.21	-.02	-.0888
.31	-.02	-.0834
.40	-.02	-.0195
.51	-.01	-.0211
.61	-.01	-.0143
.71	-.00	.0055

X/C	Z/C	CP
.11	.01	-1.2066
.21	.00	-.2477
.31	.00	-1.1142
.41	.01	-1.0329
.51	.01	-.8168
.62	.01	-.7009
.71	.00	-.5763
.11	-.05	.1983
.22	-.04	.1295
.32	-.03	.0921
.42	-.03	.0439
.51	-.02	.0640
.62	-.01	.0845
.72	-.00	.1180

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17203

MACH .806

Q 30181.8

ALPW

6.00

BETA

0.00

P1 66387.13

PT1 101791.39

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4179
.05	.05	-.9800
.10	.06	-.8654
.15	.06	-.9085
.20	.07	-.7801
.25	.07	-.8167
.30	.07	-.8802
.35	.07	-.9061
.40	.07	-.9260
.45	.07	-.9675
.50	.07	-.9938
.55	.06	-.9369
.60	.06	-.9198
.65	.05	-.9266
.70	.05	-.5788
.75	.04	-.3984
.80	.03	-.3063
.85	.03	-.2262
.90	.02	-.1389
0.00	.03	.1614
.05	.01	.2591
.10	.01	.1742
.15	.00	.1277
.20	-.00	.1145
.25	-.00	.0622
.30	-.01	.0488
.35	-.01	.0355
.40	-.01	.0288
.45	-.01	-.0192
.50	-.01	-.0011
.55	-.01	.0039
.60	-.01	.0074
.65	-.01	.0131
.70	-.00	.0241
.75	-.00	.0338
.80	-.00	.0489
.85	.00	.0746
.90	.00	.1314

X/C	Z/C	CP
0.00	.01	.2053
.05	.03	-1.3032
.10	.04	-1.2695
.15	.05	-1.2627
.20	.06	-1.2680
.25	.06	-1.2712
.30	.07	-1.2640
.35	.07	-1.1655
.40	.07	-1.1136
.45	.07	-.9640
.50	.07	-.7712
.55	.06	-.5552
.60	.06	-.5096
.65	.05	-.5002
.70	.05	-.4440
.75	.04	-.4159
.80	.04	-.3093
.85	.03	-.2754
0.00	.01	.1907
.04	-.00	.0361
.09	-.01	.2439
.14	-.01	.1969
.19	-.01	.1620
.24	-.01	.1286
.29	-.01	.1059
.34	-.01	.0842
.39	-.01	.0685
.44	-.01	.0597
.49	-.01	.0663
.54	-.01	.0695
.59	-.01	.0809
.64	-.00	.0692
.69	-.00	.0968
.74	.00	.1009
.79	.00	.1201
.84	.00	.1310

X/C	Z/C	CP
0.00	-.01	.1366
.11	.03	-.3758
.20	.05	-.5774
.31	.06	-.6960
.40	.07	-.6331
.51	.06	-.6240
.61	.06	-.4785
.71	.05	-.4297
0.00	-.01	-1.1046
.11	-.02	-.1210
.21	-.02	-.1045
.31	-.02	-.1082
.40	-.02	-.0522
.51	-.01	-.0531
.61	-.01	-.0477
.71	-.00	-.0350

X/C	Z/C	CP
.11	.01	-1.2031
.21	.00	-.2303
.31	.00	-1.1026
.41	.01	-1.0318
.51	.01	-.8042
.62	.01	-.5255
.71	.00	-.3197
.11	-.05	.1852
.22	-.04	.1220
.32	-.03	.0822
.42	-.03	.0712
.51	-.02	.0540
.62	-.01	.0743
.72	-.00	.1045

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 19

TP 17204

MACH .806

Q 30204.0

ALPW

.04

BETA

0.00

P1 66349.12

PT1 101787.00

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5161	0.00	.01	.6152	0.00	-.01	.1103	.11	.01	-.3537
.05	.05	-.1061	.05	.03	-.1170	.11	.03	.0074	.21	.00	-.1381
.10	.06	-.2504	.10	.04	-.2965	.20	.05	-.2139	.31	.00	-.7244
.15	.06	-.3118	.15	.05	-.3946	.31	.06	-.3968	.41	.01	-.8594
.20	.07	-.3635	.20	.06	-.4541	.40	.07	-.6576	.51	.01	-.6545
.25	.07	-.4080	.25	.06	-.5078	.51	.06	-.6976	.62	.01	-.4888
.30	.07	-.4543	.30	.07	-.5727	.61	.06	-.5142	.71	.00	-.3174
.35	.07	-.5026	.35	.07	-.6152	.71	.05	-.3395	.11	-.05	-.1134
.40	.07	-.5427	.40	.07	-.6494	0.00	-.01	-.0163	.22	-.04	-.1118
.45	.07	-.5777	.45	.07	-.6443	.11	-.02	-.2224	.32	-.03	-.0884
.50	.07	-.5727	.50	.07	-.6347	.21	-.02	-.1579	.42	-.03	-.1357
.55	.06	-.5423	.55	.06	-.5717	.31	-.02	-.1586	.51	-.02	-.0371
.60	.06	-.4908	.60	.06	-.4838	.40	-.02	-.1168	.62	-.01	.0231
.65	.05	-.4227	.65	.05	-.4836	.51	-.01	-.0995	.72	-.00	.0962
.70	.05	-.3627	.70	.05	-.4313	.61	-.01	-.0584			
.75	.04	-.3248	.75	.04	-.3957	.71	-.00	-.0235			
.80	.03	-.2534	.80	.04	-.2482						
.85	.03	-.1911	.85	.03	-.1856						
.90	.02	-.1190	0.00	.01	.5439						
0.00	.03	.6096	.04	-.00	.0321						
.05	.01	-.3086	.09	-.01	-.2336						
.10	.01	-.2495	.14	-.01	-.1941						
.15	.00	-.2294	.19	-.01	-.1919						
.20	-.00	-.2316	.24	-.01	-.1680						
.25	-.00	-.2311	.29	-.01	-.1545						
.30	-.01	-.2233	.34	-.01	-.1424						
.35	-.01	-.2256	.39	-.01	-.1355						
.40	-.01	-.2262	.44	-.01	-.1181						
.45	-.01	-.2371	.49	-.01	-.0869						
.50	-.01	-.2245	.54	-.01	-.0563						
.55	-.01	-.2084	.59	-.01	-.0246						
.60	-.01	-.1776	.64	-.00	-.0256						
.65	-.01	-.1498	.69	-.00	.0390						
.70	-.00	-.1157	.74	.00	.0445						
.75	-.00	-.0771	.79	.00	.0597						
.80	-.00	-.0346	.84	.00	.0889						
.85	.00	.0013									
.90	.00	.0707									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17218

MACH .754

Q 27768.7

ALPW

-2.00

BETA

0.00

P1 69724.07

PT1 101669.91

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.1996
.05	.05	.0807
.10	.06	-.0777
.15	.06	-.1582
.20	.07	-.2158
.25	.07	-.2670
.30	.07	-.3066
.35	.07	-.3392
.40	.07	-.3827
.45	.07	-.3955
.50	.07	-.3843
.55	.06	-.3666
.60	.06	-.3399
.65	.05	-.3154
.70	.05	-.2770
.75	.04	-.2415
.80	.03	-.2050
.85	.03	-.1602
.90	.02	-.1057
0.00	.03	.4491
.05	.01	.5117
.10	.01	-.3931
.15	.00	-.3480
.20	-.00	-.3521
.25	-.00	-.3331
.30	-.01	-.3244
.35	-.01	-.3184
.40	-.01	-.3166
.45	-.01	-.3152
.50	-.01	-.2942
.55	-.01	-.2742
.60	-.01	-.2430
.65	-.01	-.2013
.70	-.00	-.1603
.75	-.00	-.0932
.80	-.00	-.0615
.85	.00	-.0280
.90	.00	.0644

X/C	Z/C	CP
0.00	.01	.3628
.05	.03	.1508
.10	.04	-.0408
.15	.05	-.1510
.20	.06	-.2177
.25	.06	-.2801
.30	.07	-.3360
.35	.07	-.3811
.40	.07	-.4202
.45	.07	-.4278
.50	.07	-.4132
.55	.06	-.3949
.60	.06	-.3730
.65	.05	-.3739
.70	.05	-.3514
.75	.04	-.3224
.80	.04	-.2148
.85	.03	-.1670
0.00	.01	.3186
.04	-.00	.0354
.09	-.01	-.6175
.14	-.01	-.4643
.19	-.01	-.3602
.24	-.01	-.3132
.29	-.01	-.2692
.34	-.01	-.2389
.39	-.01	-.2143
.44	-.01	-.1840
.49	-.01	-.1469
.54	-.01	-.1122
.59	-.01	-.0729
.64	-.00	-.0671
.69	-.00	-.0054
.74	.00	.0044
.79	.00	.0224
.84	.00	.0477

X/C	Z/C	CP
0.00	-.01	.0691
.11	.03	-.1726
.20	.05	-.1393
.31	.06	-.2191
.40	.07	-.3901
.51	.06	-.4309
.61	.06	-.3485
.71	.05	-.2570
0.00	-.01	-.0388
.11	-.02	-.3907
.21	-.02	-.2964
.31	-.02	-.2988
.40	-.02	-.2119
.51	-.01	-.1692
.61	-.01	-.1145
.71	-.00	-.0682

X/C	Z/C	CP
.11	.01	-.0824
.21	.00	-.1091
.31	.00	-.4497
.41	.01	-.5152
.51	.01	-.4950
.62	.01	-.3974
.71	.00	-.2711
.11	-.05	-.6304
.22	-.04	-.4058
.32	-.03	-.2583
.42	-.03	-.1997
.51	-.02	-.1149
.62	-.01	-.0527
.72	-.00	.0158

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17219

MACH .754

Q 27732.7

ALPW

-1.45

BETA

0.00

P1 69768.88

PT1 101664.75

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.2936
.05	.05	.0144
.10	.06	-.1227
.15	.06	-.1939
.20	.07	-.2571
.25	.07	-.3013
.30	.07	-.3491
.35	.07	-.3832
.40	.07	-.4082
.45	.07	-.4206
.50	.07	-.4055
.55	.06	-.3864
.60	.06	-.3589
.65	.05	-.3309
.70	.05	-.2912
.75	.04	-.2499
.80	.03	-.2123
.85	.03	-.1667
.90	.02	-.1091
0.00	.03	.5091
.05	.01	-.4518
.10	.01	-.3447
.15	.00	-.3055
.20	-.00	-.3032
.25	-.00	-.2881
.30	-.01	-.2761
.35	-.01	-.2811
.40	-.01	-.2814
.45	-.01	-.2855
.50	-.01	-.2714
.55	-.01	-.2422
.60	-.01	-.2111
.65	-.01	-.1773
.70	-.00	-.1415
.75	-.00	-.1034
.80	-.00	-.0679
.85	.00	-.0250
.90	.00	.0483

X/C	Z/C	CP
0.00	.01	.4379
.05	.03	.0891
.10	.04	-.1021
.15	.05	-.2021
.20	.06	-.2699
.25	.06	-.3289
.30	.07	-.3803
.35	.07	-.4254
.40	.07	-.4627
.45	.07	-.4642
.50	.07	-.4425
.55	.06	-.4203
.60	.06	-.3913
.65	.05	-.3811
.70	.05	-.3644
.75	.04	-.3330
.80	.04	-.2230
.85	.03	-.2043
0.00	.01	.3803
.04	-.00	.0566
.09	-.01	-.4829
.14	-.01	-.3468
.19	-.01	-.3558
.24	-.01	-.2621
.29	-.01	-.2301
.34	-.01	-.2087
.39	-.01	-.1895
.44	-.01	-.1645
.49	-.01	-.1278
.54	-.01	-.0944
.59	-.01	-.0586
.64	-.00	-.0517
.69	-.00	.0087
.74	.00	.0118
.79	.00	.0290
.84	.00	.0529

X/C	Z/C	CP
0.00	-.01	.0843
.11	.03	-.1079
.20	.05	-.1424
.31	.06	-.2641
.40	.07	-.4347
.51	.06	-.4745
.61	.06	-.3695
.71	.05	-.2734
0.00	-.01	-.0239
.11	-.02	-.3817
.21	-.02	-.2847
.31	-.02	-.2898
.40	-.02	-.1885
.51	-.01	-.1557
.61	-.01	-.0945
.71	-.00	-.0472

X/C	Z/C	CP
.11	.01	-.1439
.21	.00	-.1171
.31	.00	-.5042
.41	.01	-.5473
.51	.01	-.5246
.62	.01	-.4161
.71	.00	-.2805
.11	-.05	-.4565
.22	-.04	-.2574
.32	-.03	-.1798
.42	-.03	-.1528
.51	-.02	-.0863
.62	-.01	-.0233
.72	-.00	.0457

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17220

MACH .754

Q

27756.7

ALPW

-.91

BETA

0.00

P1 69725.88

PT1 101655.85

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.3924
.05	.05	-.0358
.10	.06	-.1717
.15	.06	-.2390
.20	.07	-.2938
.25	.07	-.3432
.30	.07	-.3817
.35	.07	-.4136
.40	.07	-.4405
.45	.07	-.4414
.50	.07	-.4337
.55	.06	-.4133
.60	.06	-.3809
.65	.05	-.3498
.70	.05	-.3042
.75	.04	-.2609
.80	.03	-.2208
.85	.03	-.1710
.90	.02	-.1142
0.00	.03	.5546
.05	.01	-.4029
.10	.01	-.2987
.15	.00	-.2954
.20	-.00	-.2736
.25	-.00	-.2542
.30	-.01	-.2540
.35	-.01	-.2540
.40	-.01	-.2573
.45	-.01	-.2636
.50	-.01	-.2434
.55	-.01	-.2227
.60	-.01	-.1936
.65	-.01	-.1618
.70	-.00	-.1325
.75	-.00	-.0914
.80	-.00	-.0500
.85	.00	-.0175
.90	.00	.0384

X/C	Z/C	CP
0.00	.01	.5197
.05	.03	.0196
.10	.04	-.1670
.15	.05	-.2683
.20	.06	-.3279
.25	.06	-.3851
.30	.07	-.4301
.35	.07	-.4724
.40	.07	-.5011
.45	.07	-.4997
.50	.07	-.4794
.55	.06	-.4483
.60	.06	-.4178
.65	.05	-.4074
.70	.05	-.3846
.75	.04	-.3526
.80	.04	-.2298
.85	.03	-.2225
0.00	.01	.0762
.04	-.00	.0705
.09	-.01	-.3376
.14	-.01	-.2815
.19	-.01	-.2801
.24	-.01	-.2248
.29	-.01	-.2021
.34	-.01	-.1848
.39	-.01	-.1707
.44	-.01	-.1488
.49	-.01	-.1139
.54	-.01	-.0816
.59	-.01	-.0491
.64	-.00	-.0440
.69	-.00	.0225
.74	.00	.0217
.79	.00	.0350
.84	.00	.0684

X/C	Z/C	CP
0.00	-.01	.0956
.11	.03	-.0613
.20	.05	-.1579
.31	.06	-.3105
.40	.07	-.4870
.51	.06	-.5167
.61	.06	-.4018
.71	.05	-.2929
0.00	-.01	.0051
.11	-.02	-.3369
.21	-.02	-.2422
.31	-.02	-.2436
.40	-.02	-.1662
.51	-.01	-.1403
.61	-.01	-.0874
.71	-.00	-.0395

X/C	Z/C	CP
.11	.01	-.2143
.21	.00	-.1251
.31	.00	-.5532
.41	.01	-.5990
.51	.01	-.5556
.62	.01	-.4356
.71	.00	-.2916
.11	-.05	-.2428
.22	-.04	-.1840
.32	-.03	-.1427
.42	-.03	-.1366
.51	-.02	-.0690
.62	-.01	-.0082
.72	-.00	.0669

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17221

MACH .754

Q 27772.3

ALPW

-0.42

BETA

0.00

P1 69699.80

PT1 101651.85

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4560
.05	.05	-.0854
.10	.06	-.2058
.15	.06	-.2806
.20	.07	-.3320
.25	.07	-.3745
.30	.07	-.4153
.35	.07	-.4378
.40	.07	-.4761
.45	.07	-.4774
.50	.07	-.4537
.55	.06	-.4320
.60	.06	-.4005
.65	.05	-.3649
.70	.05	-.3179
.75	.04	-.2731
.80	.03	-.2293
.85	.03	-.1787
.90	.02	-.1180
0.00	.03	.5818
.05	.01	-.3394
.10	.01	-.2648
.15	.00	-.2634
.20	-.00	-.2485
.25	-.00	-.2270
.30	-.01	-.2165
.35	-.01	-.2345
.40	-.01	-.2252
.45	-.01	-.2370
.50	-.01	-.2255
.55	-.01	-.2056
.60	-.01	-.1812
.65	-.01	-.1510
.70	-.00	-.1207
.75	-.00	-.0875
.80	-.00	-.0521
.85	.00	-.0036
.90	.00	.0664

X/C	Z/C	CP
0.00	.01	.5774
.05	.03	-.0496
.10	.04	-.2256
.15	.05	-.3186
.20	.06	-.3870
.25	.06	-.4299
.30	.07	-.4863
.35	.07	-.5107
.40	.07	-.5432
.45	.07	-.5312
.50	.07	-.5068
.55	.06	-.4749
.60	.06	-.4379
.65	.05	-.4378
.70	.05	-.4136
.75	.04	-.3699
.80	.04	-.2415
.85	.03	-.2320
0.00	.01	.4821
.04	-.00	.0578
.09	-.01	-.2713
.14	-.01	-.2238
.19	-.01	-.2271
.24	-.01	-.1873
.29	-.01	-.1725
.34	-.01	-.1616
.39	-.01	-.1489
.44	-.01	-.1283
.49	-.01	-.1004
.54	-.01	-.0669
.59	-.01	-.0374
.64	-.00	-.0299
.69	-.00	.0257
.74	.00	.0319
.79	.00	.0482
.84	.00	.0737

X/C	Z/C	CP
0.00	-.01	.1001
.11	.03	-.0233
.20	.05	-.1897
.31	.06	-.3553
.40	.07	-.5434
.51	.06	-.5722
.61	.06	-.4322
.71	.05	-.3110
0.00	-.01	.0152
.11	-.02	-.2651
.21	-.02	-.1950
.31	-.02	-.1978
.40	-.02	-.1468
.51	-.01	-.1289
.61	-.01	-.0769
.71	-.00	-.0292

X/C	Z/C	CP
.11	.01	-.2834
.21	.00	-.1299
.31	.00	-.6015
.41	.01	-.6350
.51	.01	-.5903
.62	.01	-.4528
.71	.00	-.3061
.11	-.05	-.1705
.22	-.04	-.1537
.32	-.03	-.1181
.42	-.03	-.1199
.51	-.02	-.0571
.62	-.01	.0048
.72	-.00	.0766

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17222

MACH .755

Q 27773.3

ALPW

.04

BETA

0.00

P1 69690.85

PT1 101644.80

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5164
.05	.05	-.1311
.10	.06	-.2594
.15	.06	-.3211
.20	.07	-.3609
.25	.07	-.4109
.30	.07	-.4489
.35	.07	-.4751
.40	.07	-.4990
.45	.07	-.5044
.50	.07	-.4817
.55	.06	-.4533
.60	.06	-.4124
.65	.05	-.3741
.70	.05	-.3283
.75	.04	-.2829
.80	.03	-.2359
.85	.03	-.1804
.90	.02	-.1189
0.00	.03	.6037
.05	.01	-.2775
.10	.01	-.2230
.15	.00	-.2296
.20	-.00	-.2206
.25	-.00	-.2140
.30	-.01	-.2064
.35	-.01	-.2067
.40	-.01	-.2100
.45	-.01	-.2131
.50	-.01	-.2029
.55	-.01	-.1943
.60	-.01	-.1667
.65	-.01	-.1420
.70	-.00	-.1089
.75	-.00	-.0661
.80	-.00	-.0381
.85	.00	.0030
.90	.00	.0603

X/C	Z/C	CP
0.00	.01	.6167
.05	.03	-.1191
.10	.04	-.2952
.15	.05	-.3760
.20	.06	-.4274
.25	.06	-.4771
.30	.07	-.5241
.35	.07	-.5522
.40	.07	-.5784
.45	.07	-.5669
.50	.07	-.5403
.55	.06	-.5017
.60	.06	-.4579
.65	.05	-.4524
.70	.05	-.4245
.75	.04	-.3884
.80	.04	-.2491
.85	.03	-.2379
0.00	.01	.5147
.04	-.00	.0417
.09	-.01	-.2204
.14	-.01	-.1757
.19	-.01	-.1759
.24	-.01	-.1551
.29	-.01	-.1438
.34	-.01	-.1363
.39	-.01	-.1269
.44	-.01	-.1104
.49	-.01	-.0821
.54	-.01	-.0544
.59	-.01	-.0252
.64	-.00	-.0195
.69	-.00	.0370
.74	.00	.0349
.79	.00	.0555
.84	.00	.0801

X/C	Z/C	CP
0.00	-.01	.0969
.11	.03	.0031
.20	.05	-.2167
.31	.06	-.3927
.40	.07	-.5969
.51	.06	-.6292
.61	.06	-.4561
.71	.05	-.3292
0.00	-.01	.0092
.11	-.02	-.2206
.21	-.02	-.1614
.31	-.02	-.1573
.40	-.02	-.1207
.51	-.01	-.1028
.61	-.01	-.0647
.71	-.00	-.0269

X/C	Z/C	CP
.11	.01	-.3654
.21	.00	-.1378
.31	.00	-.6653
.41	.01	-.6762
.51	.01	-.6117
.62	.01	-.4661
.71	.00	-.3162
.11	-.05	-.1341
.22	-.04	-.1156
.32	-.03	-.0932
.42	-.03	-.0981
.51	-.02	-.0406
.62	-.01	.0161
.72	-.00	.0857

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17223

MACH .753

Q 27717.3

ALPW

.52

BETA

0.00

P1 69764.05

PT1 101640.06

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5624
.05	.05	-.1939
.10	.06	-.3175
.15	.06	-.3635
.20	.07	-.4033
.25	.07	-.4447
.30	.07	-.4813
.35	.07	-.5060
.40	.07	-.5264
.45	.07	-.5311
.50	.07	-.4999
.55	.06	-.4764
.60	.06	-.4311
.65	.05	-.3875
.70	.05	-.3390
.75	.04	-.2885
.80	.03	-.2418
.85	.03	-.1852
.90	.02	-.1214
0.00	.03	.6137
.05	.01	-.2203
.10	.01	-.1850
.15	.00	-.1813
.20	-.00	-.1773
.25	-.00	-.1885
.30	-.01	-.1818
.35	-.01	-.1818
.40	-.01	-.1886
.45	-.01	-.1848
.50	-.01	-.1898
.55	-.01	-.1742
.60	-.01	-.1540
.65	-.01	-.1195
.70	-.00	-.0919
.75	-.00	-.0575
.80	-.00	-.0243
.85	.00	.0063
.90	.00	.0711

X/C	Z/C	CP
0.00	.01	.6376
.05	.03	-.2002
.10	.04	-.3689
.15	.05	-.4390
.20	.06	-.4886
.25	.06	-.5385
.30	.07	-.5818
.35	.07	-.6019
.40	.07	-.6204
.45	.07	-.6092
.50	.07	-.5724
.55	.06	-.5295
.60	.06	-.4786
.65	.05	-.4661
.70	.05	-.3810
.75	.04	-.3707
.80	.04	-.2571
.85	.03	-.1905
0.00	.01	.5545
.04	-.00	.0477
.09	-.01	-.1681
.14	-.01	-.1327
.19	-.01	-.1189
.24	-.01	-.1190
.29	-.01	-.1153
.34	-.01	-.1045
.39	-.01	-.1048
.44	-.01	-.0907
.49	-.01	-.0639
.54	-.01	-.0366
.59	-.01	-.0130
.64	-.00	-.0037
.69	-.00	.0472
.74	.00	.0500
.79	.00	.0743
.84	.00	.0884

X/C	Z/C	CP
0.00	-.01	.1128
.11	.03	.0163
.20	.05	-.2511
.31	.06	-.4424
.40	.07	-.6561
.51	.06	-.7030
.61	.06	-.4796
.71	.05	-.3435
0.00	-.01	-.0052
.11	-.02	-.1559
.21	-.02	-.1313
.31	-.02	-.1302
.40	-.02	-.0981
.51	-.01	-.0861
.61	-.01	-.0524
.71	-.00	-.0163

X/C	Z/C	CP
.11	.01	-.4678
.21	.00	-.1351
.31	.00	-.7583
.41	.01	-.7166
.51	.01	-.6467
.62	.01	-.4864
.71	.00	-.3270
.11	-.05	-.1058
.22	-.04	-.0884
.32	-.03	-.0714
.42	-.03	-.0708
.51	-.02	-.0254
.62	-.01	.0197
.72	-.00	.0920

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17224

MACH .755

Q 27778.6

ALPW

.99

BETA

0.00

P1 69679.45

PT1 101641.12

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5919
.05	.05	-.2464
.10	.06	-.3629
.15	.06	-.3988
.20	.07	-.4346
.25	.07	-.4831
.30	.07	-.5105
.35	.07	-.5359
.40	.07	-.5557
.45	.07	-.5576
.50	.07	-.5373
.55	.06	-.4945
.60	.06	-.4534
.65	.05	-.4067
.70	.05	-.3498
.75	.04	-.3004
.80	.03	-.2484
.85	.03	-.1913
.90	.02	-.1268
0.00	.03	.6109
.05	.01	-.1647
.10	.01	-.1472
.15	.00	-.1525
.20	-.00	-.1397
.25	-.00	-.1609
.30	-.01	-.1521
.35	-.01	-.1623
.40	-.01	-.1657
.45	-.01	-.1680
.50	-.01	-.1680
.55	-.01	-.1603
.60	-.01	-.1329
.65	-.01	-.1128
.70	-.00	-.0793
.75	-.00	-.0434
.80	-.00	-.0172
.85	.00	.0251
.90	.00	.1121

X/C	Z/C	CP
0.00	.01	.6430
.05	.03	-.2957
.10	.04	-.4424
.15	.05	-.4988
.20	.06	-.5467
.25	.06	-.5847
.30	.07	-.6226
.35	.07	-.6472
.40	.07	-.6617
.45	.07	-.6478
.50	.07	-.5997
.55	.06	-.5508
.60	.06	-.4966
.65	.05	-.4936
.70	.05	-.4046
.75	.04	-.3894
.80	.04	-.2626
.85	.03	-.2014
0.00	.01	.6433
.04	-.00	.0310
.09	-.01	-.1120
.14	-.01	-.1008
.19	-.01	-.0920
.24	-.01	-.0909
.29	-.01	-.0899
.34	-.01	-.0845
.39	-.01	-.0870
.44	-.01	-.0741
.49	-.01	-.0471
.54	-.01	-.0217
.59	-.01	.0049
.64	-.00	.0118
.69	-.00	.0606
.74	.00	.0630
.79	.00	.0833
.84	.00	.1027

X/C	Z/C	CP
0.00	-.01	.1209
.11	.03	.0240
.20	.05	-.3414
.31	.06	-.5097
.40	.07	-.7875
.51	.06	-.7859
.61	.06	-.5051
.71	.05	-.3647
0.00	-.01	-.0295
.11	-.02	-.1255
.21	-.02	-.1107
.31	-.02	-.1043
.40	-.02	-.0819
.51	-.01	-.0718
.61	-.01	-.0428
.71	-.00	-.0120

X/C	Z/C	CP
.11	.01	-.5525
.21	.00	-.1548
.31	.00	-.8094
.41	.01	-.7528
.51	.01	-.6750
.62	.01	-.4982
.71	.00	-.3361
.11	-.05	-.0507
.22	-.04	-.0539
.32	-.03	-.0454
.42	-.03	-.0459
.51	-.02	-.0102
.62	-.01	.0375
.72	-.00	.0776

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17225

MACH .754

Q 27737.1

ALPW

1.55

BETA

0.00

P1 69731.57

PT1 101635.54

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6027	0.00	.01	.6349	0.00	-.01	.1320	.11	.01	-.6615
.05	.05	-.3277	.05	.03	-.4030	.11	.03	.0134	.21	.00	-.1595
.10	.06	-.4201	.10	.04	-.5298	.20	.05	-.3672	.31	.00	-.8624
.15	.06	-.4553	.15	.05	-.5837	.31	.06	-.5712	.41	.01	-.7859
.20	.07	-.4842	.20	.06	-.6244	.40	.07	-.8822	.51	.01	-.6945
.25	.07	-.5246	.25	.06	-.6577	.51	.06	-.8536	.62	.01	-.5179
.30	.07	-.5569	.30	.07	-.6874	.61	.06	-.5255	.71	.00	-.3469
.35	.07	-.5717	.35	.07	-.6994	.71	.05	-.3783	.11	-.05	.0073
.40	.07	-.5988	.40	.07	-.7151	0.00	-.01	-.0709	.22	-.04	-.0104
.45	.07	-.5944	.45	.07	-.7027	.11	-.02	-.1174	.32	-.03	-.0140
.50	.07	-.5586	.50	.07	-.6347	.21	-.02	-.0893	.42	-.03	-.0178
.55	.06	-.5192	.55	.06	-.5741	.31	-.02	-.0825	.51	-.02	.0077
.60	.06	-.4666	.60	.06	-.5187	.40	-.02	-.0615	.62	-.01	.0522
.65	.05	-.4165	.65	.05	-.5037	.51	-.01	-.0559	.72	-.00	.0970
.70	.05	-.3626	.70	.05	-.4265	.61	-.01	-.0311			
.75	.04	-.3093	.75	.04	-.3346	.71	-.00	-.0042			
.80	.03	-.2550	.80	.04	-.2677						
.85	.03	-.1959	.85	.03	-.2059						
.90	.02	-.1265	0.00	.01	.5757						
0.00	.03	.5985	.04	-.00	.0329						
.05	.01	-.1010	.09	-.01	-.0619						
.10	.01	-.1011	.14	-.01	-.0589						
.15	.00	-.1100	.19	-.01	-.0666						
.20	-.00	-.1126	.24	-.01	-.0636						
.25	-.00	-.1301	.29	-.01	-.0622						
.30	-.01	-.1208	.34	-.01	-.0663						
.35	-.01	-.1408	.39	-.01	-.0634						
.40	-.01	-.1419	.44	-.01	-.0571						
.45	-.01	-.1524	.49	-.01	-.0360						
.50	-.01	-.1507	.54	-.01	-.0138						
.55	-.01	-.1380	.59	-.01	.0088						
.60	-.01	-.1263	.64	-.00	.0267						
.65	-.01	-.1001	.69	-.00	.0759						
.70	-.00	-.0623	.74	.00	.0762						
.75	-.00	-.0350	.79	.00	.0897						
.80	-.00	-.0094	.84	.00	.1067						
.85	.00	.0306									
.90	.00	.1106									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17226

MACH .754

Q

27745.2

ALPW

2.01

BETA

0.00

P1 69718.05

PT1 101633.56

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6074
.05	.05	-.3925
.10	.06	-.4726
.15	.06	-.4975
.20	.07	-.5261
.25	.07	-.5594
.30	.07	-.5827
.35	.07	-.6139
.40	.07	-.6303
.45	.07	-.6225
.50	.07	-.5838
.55	.06	-.5399
.60	.06	-.4886
.65	.05	-.4327
.70	.05	-.3721
.75	.04	-.3151
.80	.03	-.2613
.85	.03	-.1983
.90	.02	-.1283
0.00	.03	.5730
.05	.01	-.0472
.10	.01	-.0666
.15	.00	-.0855
.20	-.00	-.0773
.25	-.00	-.1098
.30	-.01	-.1137
.35	-.01	-.1111
.40	-.01	-.1236
.45	-.01	-.1311
.50	-.01	-.1363
.55	-.01	-.1243
.60	-.01	-.1090
.65	-.01	-.0832
.70	-.00	-.0612
.75	-.00	-.0307
.80	-.00	.0064
.85	.00	.0366
.90	.00	.1063

X/C	Z/C	CP
0.00	.01	.6141
.05	.03	-.4991
.10	.04	-.6174
.15	.05	-.6601
.20	.06	-.6822
.25	.06	-.7058
.30	.07	-.7497
.35	.07	-.7440
.40	.07	-.7632
.45	.07	-.7436
.50	.07	-.6717
.55	.06	-.5871
.60	.06	-.5331
.65	.05	-.5366
.70	.05	-.4654
.75	.04	-.4163
.80	.04	-.2717
.85	.03	-.2097
0.00	.01	.5557
.04	-.00	.0382
.09	-.01	-.0116
.14	-.01	-.0190
.19	-.01	-.0224
.24	-.01	-.0323
.29	-.01	-.0375
.34	-.01	-.0445
.39	-.01	-.0444
.44	-.01	-.0402
.49	-.01	-.0197
.54	-.01	.0013
.59	-.01	.0225
.64	-.00	.0298
.69	-.00	.0863
.74	.00	.0857
.79	.00	.0992
.84	.00	.1134

X/C	Z/C	CP
0.00	-.01	.1351
.11	.03	-.0088
.20	.05	-.4098
.31	.06	-.6369
.40	.07	-.9327
.51	.06	-.9630
.61	.06	-.5381
.71	.05	-.3855
0.00	-.01	-.1325
.11	-.02	-.1011
.21	-.02	-.0797
.31	-.02	-.0835
.40	-.02	-.0478
.51	-.01	-.0443
.61	-.01	-.0259
.71	-.00	-.0014

X/C	Z/C	CP
.11	.01	-.7816
.21	.00	-.1670
.31	.00	-1.0400
.41	.01	-.8372
.51	.01	-.6715
.62	.01	-.5191
.71	.00	-.3529
.11	-.05	.0483
.22	-.04	.0211
.32	-.03	.0106
.42	-.03	.0013
.51	-.02	.0234
.62	-.01	.0628
.72	-.00	.1067

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17227

MACH .753

Q 27717.8

ALPW

2.54

BETA

0.00

P1 69752.73

PT1 101630.10

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5972	0.00	.01	.5744	0.00	-.01	.1398	.11	.01	-.9551
.05	.05	-.4618	.05	.03	-.5945	.11	.03	-.0438	.21	.00	-.1976
.10	.06	-.5230	.10	.04	-.7147	.20	.05	-.5468	.31	.00	-1.1586
.15	.06	-.5506	.15	.05	-.7375	.31	.06	-.7914	.41	.01	-1.0144
.20	.07	-.5680	.20	.06	-.7667	.40	.07	-.9731	.51	.01	-.6626
.25	.07	-.6029	.25	.06	-.7729	.51	.06	-1.0349	.62	.01	-.5159
.30	.07	-.6176	.30	.07	-.8175	.61	.06	-.5565	.71	.00	-.3534
.35	.07	-.6432	.35	.07	-.8074	.71	.05	-.3924	.11	-.05	.0982
.40	.07	-.6640	.40	.07	-.8095	0.00	-.01	-.2309	.22	-.04	.0547
.45	.07	-.6596	.45	.07	-.7737	.11	-.02	-.0891	.32	-.03	.0376
.50	.07	-.6123	.50	.07	-.7165	.21	-.02	-.0768	.42	-.03	.0189
.55	.06	-.5605	.55	.06	-.6022	.31	-.02	-.0767	.51	-.02	.0399
.60	.06	-.5010	.60	.06	-.5489	.40	-.02	-.0368	.62	-.01	.0755
.65	.05	-.4466	.65	.05	-.5448	.51	-.01	-.0343	.72	-.00	.1185
.70	.05	-.3810	.70	.05	-.4333	.61	-.01	-.0201			
.75	.04	-.3222	.75	.04	-.3887	.71	-.00	.0028			
.80	.03	-.2655	.80	.04	-.2750						
.85	.03	-.2016	.85	.03	-.2056						
.90	.02	-.1294	0.00	.01	.6045						
0.00	.03	.5276	.04	-.00	.0498						
.05	.01	.0056	.09	-.01	.0436						
.10	.01	-.0274	.14	-.01	.0195						
.15	.00	-.0516	.19	-.01	.0118						
.20	-.00	-.0655	.24	-.01	-.0014						
.25	-.00	-.0849	.29	-.01	-.0106						
.30	-.01	-.0802	.34	-.01	-.0145						
.35	-.01	-.0979	.39	-.01	-.0214						
.40	-.01	-.1009	.44	-.01	-.0183						
.45	-.01	-.1133	.49	-.01	-.0022						
.50	-.01	-.1205	.54	-.01	.0161						
.55	-.01	-.1097	.59	-.01	.0352						
.60	-.01	-.0951	.64	-.00	.0465						
.65	-.01	-.0711	.69	-.00	.0915						
.70	-.00	-.0387	.74	.00	.0945						
.75	-.00	.0211	.79	.00	.1118						
.80	-.00	.0285	.84	.00	.1194						
.85	.00	.0514									
.90	.00	.1218									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17228

MACH .755

Q 27791.5

ALPW

3.03

BETA

0.00

P1 69643.85

PT1 101624.63

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5829
.05	.05	-.5406
.10	.06	-.5879
.15	.06	-.6066
.20	.07	-.6137
.25	.07	-.6387
.30	.07	-.6576
.35	.07	-.6876
.40	.07	-.7111
.45	.07	-.6924
.50	.07	-.6458
.55	.06	-.5896
.60	.06	-.5224
.65	.05	-.4583
.70	.05	-.3937
.75	.04	-.3274
.80	.03	-.2696
.85	.03	-.2039
.90	.02	-.1295
0.00	.03	.4773
.05	.01	.0471
.10	.01	.0073
.15	.00	-.0218
.20	-.00	-.0253
.25	-.00	-.0657
.30	-.01	-.0533
.35	-.01	-.0693
.40	-.01	-.0789
.45	-.01	-.0926
.50	-.01	-.0909
.55	-.01	-.0809
.60	-.01	-.0702
.65	-.01	-.0601
.70	-.00	-.0339
.75	-.00	-.0091
.80	-.00	.0159
.85	.00	.0490
.90	.00	.1262

X/C	Z/C	CP
0.00	.01	.4915
.05	.03	-.7341
.10	.04	-.8159
.15	.05	-.8307
.20	.06	-.8334
.25	.06	-.8579
.30	.07	-.8949
.35	.07	-.8666
.40	.07	-.8691
.45	.07	-.8121
.50	.07	-.7458
.55	.06	-.6201
.60	.06	-.5613
.65	.05	-.5595
.70	.05	-.4513
.75	.04	-.4232
.80	.04	-.2766
.85	.03	-.2054
0.00	.01	.5054
.04	-.00	.0211
.09	-.01	.0864
.14	-.01	.0601
.19	-.01	.0599
.24	-.01	.0277
.29	-.01	.0131
.34	-.01	.0053
.39	-.01	-.0017
.44	-.01	.0003
.49	-.01	.0131
.54	-.01	.0298
.59	-.01	.0466
.64	-.00	.0574
.69	-.00	.1015
.74	.00	.1045
.79	.00	.1116
.84	.00	.1279

X/C	Z/C	CP
0.00	-.01	.1506
.11	.03	-.0972
.20	.05	-.4524
.31	.06	-.7735
.40	.07	-.9674
.51	.06	-1.0781
.61	.06	-.6250
.71	.05	-.4099
0.00	-.01	-.3751
.11	-.02	-.0814
.21	-.02	-.0663
.31	-.02	-.0655
.40	-.02	-.0252
.51	-.01	-.0265
.61	-.01	-.0170
.71	-.00	.0011

X/C	Z/C	CP
.11	.01	-1.1613
.21	.00	-.2219
.31	.00	-1.1922
.41	.01	-1.1244
.51	.01	-.7436
.62	.01	-.5138
.71	.00	-.3496
.11	-.05	.1304
.22	-.04	.0856
.32	-.03	.0601
.42	-.03	.0445
.51	-.02	.0542
.62	-.01	.0854
.72	-.00	.1262

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17229

MACH .756

Q 27814.1

ALPW

4.16

BETA

0.00

P1 69604.85

PT1 101617.72

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4986
.05	.05	-.7166
.10	.06	-.7401
.15	.06	-.7322
.20	.07	-.7145
.25	.07	-.7121
.30	.07	-.7430
.35	.07	-.7671
.40	.07	-.7976
.45	.07	-.8081
.50	.07	-.7259
.55	.06	-.6415
.60	.06	-.5583
.65	.05	-.4805
.70	.05	-.4042
.75	.04	-.3398
.80	.03	-.2762
.85	.03	-.2053
.90	.02	-.1283
0.00	.03	.3117
.05	.01	.1518
.10	.01	.0845
.15	.00	.0483
.20	-.00	.0154
.25	-.00	-.0074
.30	-.01	-.0076
.35	-.01	-.0178
.40	-.01	-.0307
.45	-.01	-.0575
.50	-.01	-.0576
.55	-.01	-.0449
.60	-.01	-.0376
.65	-.01	-.0238
.70	-.00	-.0068
.75	-.00	.0529
.80	-.00	.0565
.85	.00	.0738
.90	.00	.1354

X/C	Z/C	CP
0.00	.01	.3077
.05	.03	-1.0078
.10	.04	-1.0357
.15	.05	-1.0899
.20	.06	-1.0122
.25	.06	-1.0070
.30	.07	-1.0335
.35	.07	-1.0532
.40	.07	-1.0582
.45	.07	-.8977
.50	.07	-.7069
.55	.06	-.6347
.60	.06	-.5636
.65	.05	-.5533
.70	.05	-.4097
.75	.04	-.4115
.80	.04	-.2697
.85	.03	-.1967
0.00	.01	.2781
.04	-.00	.0285
.09	-.01	.1773
.14	-.01	.1350
.19	-.01	.1317
.24	-.01	.0855
.29	-.01	.0672
.34	-.01	.0537
.39	-.01	.0437
.44	-.01	.0404
.49	-.01	.0496
.54	-.01	.0610
.59	-.01	.0760
.64	-.00	.0863
.69	-.00	.1192
.74	.00	.1210
.79	.00	.1257
.84	.00	.1367

X/C	Z/C	CP
0.00	-.01	.1620
.11	.03	-.2529
.20	.05	-.6706
.31	.06	-.9357
.40	.07	-1.1352
.51	.06	-1.1549
.61	.06	-.6952
.71	.05	-.4847
0.00	-.01	-.8834
.11	-.02	-.0762
.21	-.02	-.0666
.31	-.02	-.0668
.40	-.02	-.0087
.51	-.01	-.0146
.61	-.01	-.0116
.71	-.00	.0092

X/C	Z/C	CP
.11	.01	-1.3355
.21	.00	-.2516
.31	.00	-1.1358
.41	.01	-.9308
.51	.01	-.7085
.62	.01	-.5673
.71	.00	-.4372
.11	-.05	.2056
.22	-.04	.1361
.32	-.03	.1025
.42	-.03	.0756
.51	-.02	.0782
.62	-.01	.0989
.72	-.00	.1353

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17230

MACH .755

Q 27777.1

ALPW

6.04

BETA

0.00

P1 69653.35

PT1 101614.61

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.3008
.05	.05	-1.1720
.10	.06	-.8968
.15	.06	-.9210
.20	.07	-.8833
.25	.07	-.8994
.30	.07	-.9210
.35	.07	-.9001
.40	.07	-.9116
.45	.07	-.9407
.50	.07	-.8885
.55	.06	-.6913
.60	.06	-.5807
.65	.05	-.4936
.70	.05	-.4070
.75	.04	-.3357
.80	.03	-.2668
.85	.03	-.1944
.90	.02	-.1200
0.00	.03	-.0046
.05	.01	.2824
.10	.01	.1887
.15	.00	.1406
.20	-.00	.1303
.25	-.00	.0741
.30	-.01	.0871
.35	-.01	.0687
.40	-.01	.0497
.45	-.01	-.0044
.50	-.01	-.0111
.55	-.01	-.0078
.60	-.01	.0074
.65	-.01	.0177
.70	-.00	.0365
.75	-.00	.0509
.80	-.00	.0678
.85	.00	.0895
.90	.00	.1378

X/C	Z/C	CP
0.00	.01	.0204
.05	.03	-1.6004
.10	.04	-1.5441
.15	.05	-1.5198
.20	.06	-1.5063
.25	.06	-1.4685
.30	.07	-1.4553
.35	.07	-1.3678
.40	.07	-1.3270
.45	.07	-1.1551
.50	.07	-.7300
.55	.06	-.5051
.60	.06	-.4410
.65	.05	-.4314
.70	.05	-.3268
.75	.04	-.3321
.80	.04	-.2190
.85	.03	-.1596
0.00	.01	.0392
.04	-.00	-.0112
.09	-.01	.2507
.14	-.01	.2392
.19	-.01	.1886
.24	-.01	.1572
.29	-.01	.1362
.34	-.01	.1154
.39	-.01	.0978
.44	-.01	.0866
.49	-.01	.0974
.54	-.01	.1054
.59	-.01	.1118
.64	-.00	.1253
.69	-.00	.1359
.74	.00	.1410
.79	.00	.1452
.84	.00	.1501

X/C	Z/C	CP
0.00	-.01	.1539
.11	.03	-.4736
.20	.05	-.8132
.31	.06	-.9837
.40	.07	-.8503
.51	.06	-.7548
.61	.06	-.4517
.71	.05	-.3874
0.00	-.01	-1.5917
.11	-.02	-.1197
.21	-.02	-.0831
.31	-.02	-.0755
.40	-.02	-.0165
.51	-.01	-.0187
.61	-.01	-.0154
.71	-.00	.0053

X/C	Z/C	CP
.11	.01	-1.3173
.21	.00	-.2186
.31	.00	-.9202
.41	.01	-.8256
.51	.01	-.7589
.62	.01	-.6902
.71	.00	-.6085
.11	-.05	.2637
.22	-.04	.1737
.32	-.03	.1236
.42	-.03	.0864
.51	-.02	.0642
.62	-.01	.0614
.72	-.00	.0796

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 20

TP 17231

MACH .754

Q 27752.1

ALPW

.05

BETA

0.00

P1 69679.60

PT1 101606.57

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5163
.05	.05	-.1382
.10	.06	-.2624
.15	.06	-.3236
.20	.07	-.3639
.25	.07	-.4037
.30	.07	-.4453
.35	.07	-.4753
.40	.07	-.5018
.45	.07	-.5045
.50	.07	-.4884
.55	.06	-.4569
.60	.06	-.4166
.65	.05	-.3732
.70	.05	-.3264
.75	.04	-.2793
.80	.03	-.2344
.85	.03	-.1830
.90	.02	-.1190
0.00	.03	.6054
.05	.01	-.2782
.10	.01	-.2231
.15	.00	-.2115
.20	-.00	-.2071
.25	-.00	-.2089
.30	-.01	-.1951
.35	-.01	-.1940
.40	-.01	-.1982
.45	-.01	-.1986
.50	-.01	-.1995
.55	-.01	-.1829
.60	-.01	-.1670
.65	-.01	-.1303
.70	-.00	-.1010
.75	-.00	-.0058
.80	-.00	-.0055
.85	.00	.0162
.90	.00	.1044

X/C	Z/C	CP
0.00	.01	.6202
.05	.03	-.1186
.10	.04	-.2906
.15	.05	-.3752
.20	.06	-.4308
.25	.06	-.4777
.30	.07	-.5279
.35	.07	-.5536
.40	.07	-.5847
.45	.07	-.5670
.50	.07	-.5367
.55	.06	-.4995
.60	.06	-.4558
.65	.05	-.4511
.70	.05	-.3523
.75	.04	-.3545
.80	.04	-.2471
.85	.03	-.1931
0.00	.01	.5497
.04	-.00	.0241
.09	-.01	-.1877
.14	-.01	-.1815
.19	-.01	-.1809
.24	-.01	-.1551
.29	-.01	-.1403
.34	-.01	-.1343
.39	-.01	-.1278
.44	-.01	-.1096
.49	-.01	-.0808
.54	-.01	-.0540
.59	-.01	-.0245
.64	-.00	-.0083
.69	-.00	.0386
.74	.00	.0378
.79	.00	.0589
.84	.00	.0799

X/C	Z/C	CP
0.00	-.01	.1063
.11	.03	.0120
.20	.05	-.1923
.31	.06	-.3712
.40	.07	-.5923
.51	.06	-.6275
.61	.06	-.4584
.71	.05	-.3291
0.00	-.01	.0076
.11	-.02	-.2142
.21	-.02	-.1591
.31	-.02	-.1556
.40	-.02	-.1216
.51	-.01	-.1017
.61	-.01	-.0636
.71	-.00	-.0250

X/C	Z/C	CP
.11	.01	-.3785
.21	.00	-.1381
.31	.00	-.6529
.41	.01	-.6678
.51	.01	-.6176
.62	.01	-.4635
.71	.00	-.3140
.11	-.05	-.1346
.22	-.04	-.1137
.32	-.03	-.0905
.42	-.03	-.0967
.51	-.02	-.0393
.62	-.01	.0157
.72	-.00	.0877

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17247

MACH .704

Q 25224.0

ALPW

-2.02

BETA

0.00

P1 72659.44

PT1 101167.58

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.1257
.05	.05	.0783
.10	.06	-.0759
.15	.06	-.1507
.20	.07	-.2112
.25	.07	-.2584
.30	.07	-.2965
.35	.07	-.3162
.40	.07	-.3572
.45	.07	-.3631
.50	.07	-.3532
.55	.06	-.3398
.60	.06	-.3181
.65	.05	-.2984
.70	.05	-.2649
.75	.04	-.2279
.80	.03	-.1933
.85	.03	-.1542
.90	.02	-.1021
0.00	.03	.4401
.05	.01	-.5043
.10	.01	-.3796
.15	.00	-.3302
.20	-.00	-.3128
.25	-.00	-.3079
.30	-.01	-.3074
.35	-.01	-.2950
.40	-.01	-.2934
.45	-.01	-.2929
.50	-.01	-.2735
.55	-.01	-.2491
.60	-.01	-.2188
.65	-.01	-.1771
.70	-.00	-.1340
.75	-.00	-.0951
.80	-.00	-.0625
.85	.00	-.0211
.90	.00	.0674

X/C	Z/C	CP
0.00	.01	.3153
.05	.03	.1525
.10	.04	-.0367
.15	.05	-.1388
.20	.06	-.2093
.25	.06	-.2675
.30	.07	-.3190
.35	.07	-.3552
.40	.07	-.3891
.45	.07	-.3999
.50	.07	-.4014
.55	.06	-.3953
.60	.06	-.3473
.65	.05	-.3533
.70	.05	-.3249
.75	.04	-.2990
.80	.04	-.2063
.85	.03	-.2036
0.00	.01	.3241
.04	-.00	.0098
.09	-.01	-.5798
.14	-.01	-.4198
.19	-.01	-.3292
.24	-.01	-.2954
.29	-.01	-.2624
.34	-.01	-.2315
.39	-.01	-.2081
.44	-.01	-.1811
.49	-.01	-.1419
.54	-.01	-.1106
.59	-.01	-.0735
.64	-.00	-.0545
.69	-.00	-.0035
.74	.00	.0284
.79	.00	.0240
.84	.00	.0496

X/C	Z/C	CP
0.00	-.01	-.1296
.11	.03	-.2596
.20	.05	-.1453
.31	.06	-.2194
.40	.07	-.3750
.51	.06	-.4113
.61	.06	-.3260
.71	.05	-.2397
0.00	-.01	-.0174
.11	-.02	-.5149
.21	-.02	-.3516
.31	-.02	-.3423
.40	-.02	-.1975
.51	-.01	-.1588
.61	-.01	-.1013
.71	-.00	-.0559

X/C	Z/C	CP
.11	.01	-.0850
.21	.00	-.1197
.31	.00	-.4265
.41	.01	-.4763
.51	.01	-.4559
.62	.01	-.3679
.71	.00	-.2602
.11	-.05	-.5971
.22	-.04	-.3979
.32	-.03	-.2736
.42	-.03	-.2092
.51	-.02	-.1173
.62	-.01	-.0554
.72	-.00	.0104

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17248

MACH .702

Q 25139.5

ALPW

-1.50

BETA

0.00

P1 72779.75

PT1 101175.19

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.2608
.05	.05	.0277
.10	.06	-.1222
.15	.06	-.1954
.20	.07	-.2465
.25	.07	-.2942
.30	.07	-.3313
.35	.07	-.3558
.40	.07	-.3820
.45	.07	-.3847
.50	.07	-.3751
.55	.06	-.3589
.60	.06	-.3345
.65	.05	-.3098
.70	.05	-.2729
.75	.04	-.2357
.80	.03	-.1983
.85	.03	-.1593
.90	.02	-.1058
0.00	.03	.3861
.05	.01	-.4450
.10	.01	-.3286
.15	.00	-.3119
.20	-.00	-.3084
.25	-.00	-.2932
.30	-.01	-.2732
.35	-.01	-.2661
.40	-.01	-.2606
.45	-.01	-.2643
.50	-.01	-.2545
.55	-.01	-.2224
.60	-.01	-.1928
.65	-.01	-.1612
.70	-.00	-.1204
.75	-.00	-.0878
.80	-.00	-.0453
.85	.00	-.0032
.90	.00	.0604

X/C	Z/C	CP
0.00	.01	.4066
.05	.03	.0948
.10	.04	-.0944
.15	.05	-.1941
.20	.06	-.2557
.25	.06	-.3082
.30	.07	-.3555
.35	.07	-.3917
.40	.07	-.4247
.45	.07	-.4274
.50	.07	-.4173
.55	.06	-.3905
.60	.06	-.3684
.65	.05	-.3654
.70	.05	-.3446
.75	.04	-.3126
.80	.04	-.2150
.85	.03	-.2182
0.00	.01	.3804
.04	-.00	.0526
.09	-.01	-.4370
.14	-.01	-.3288
.19	-.01	-.2787
.24	-.01	-.2546
.29	-.01	-.2252
.34	-.01	-.2039
.39	-.01	-.1891
.44	-.01	-.1632
.49	-.01	-.1290
.54	-.01	-.0956
.59	-.01	-.0617
.64	-.00	-.0566
.69	-.00	.0077
.74	.00	.0283
.79	.00	.0317
.84	.00	.0548

X/C	Z/C	CP
0.00	-.01	.0864
.11	.03	-.1457
.20	.05	-.1484
.31	.06	-.2654
.40	.07	-.4126
.51	.06	-.4437
.61	.06	-.3454
.71	.05	-.2496
0.00	-.01	-.0056
.11	-.02	-.4617
.21	-.02	-.2756
.31	-.02	-.2699
.40	-.02	-.1777
.51	-.01	-.1470
.61	-.01	-.0913
.71	-.00	-.0434

X/C	Z/C	CP
.11	.01	-.1376
.21	.00	-.1215
.31	.00	-.4611
.41	.01	-.5107
.51	.01	-.4805
.62	.01	-.3845
.71	.00	-.2680
.11	-.05	-.4700
.22	-.04	-.2542
.32	-.03	-.1831
.42	-.03	-.1562
.51	-.02	-.0883
.62	-.01	-.0295
.72	-.00	.0382

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17249

MACH .703

Q 25171.2

ALPW

- .92

BETA

0.00

P1 72753.44

PT1 101190.25

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.3942
.05	.05	-.0302
.10	.06	-.1667
.15	.06	-.2385
.20	.07	-.2871
.25	.07	-.3263
.30	.07	-.3681
.35	.07	-.3951
.40	.07	-.4123
.45	.07	-.4132
.50	.07	-.4007
.55	.06	-.3826
.60	.06	-.3515
.65	.05	-.3279
.70	.05	-.2876
.75	.04	-.2451
.80	.03	-.2121
.85	.03	-.1660
.90	.02	-.1105
0.00	.03	.5511
.05	.01	-.3863
.10	.01	-.2805
.15	.00	-.2513
.20	-.00	-.2575
.25	-.00	-.2400
.30	-.01	-.2422
.35	-.01	-.2426
.40	-.01	-.2441
.45	-.01	-.2439
.50	-.01	-.2420
.55	-.01	-.2062
.60	-.01	-.1842
.65	-.01	-.1502
.70	-.00	-.1167
.75	-.00	-.0716
.80	-.00	-.0402
.85	.00	-.0027
.90	.00	.0560

X/C	Z/C	CP
0.00	.01	.5143
.05	.03	.0162
.10	.04	-.1674
.15	.05	-.2544
.20	.06	-.3103
.25	.06	-.3589
.30	.07	-.4062
.35	.07	-.4469
.40	.07	-.4678
.45	.07	-.4623
.50	.07	-.4653
.55	.06	-.4598
.60	.06	-.3915
.65	.05	-.3884
.70	.05	-.3708
.75	.04	-.3351
.80	.04	-.2257
.85	.03	-.2237
0.00	.01	.4506
.04	-.00	.0510
.09	-.01	-.3286
.14	-.01	-.2653
.19	-.01	-.2325
.24	-.01	-.2110
.29	-.01	-.1946
.34	-.01	-.1769
.39	-.01	-.1656
.44	-.01	-.1440
.49	-.01	-.1093
.54	-.01	-.0791
.59	-.01	-.0489
.64	-.00	-.0463
.69	-.00	.0187
.74	.00	.0318
.79	.00	.0431
.84	.00	.0670

X/C	Z/C	CP
0.00	-.01	.0970
.11	.03	-.0687
.20	.05	-.1674
.31	.06	-.3254
.40	.07	-.4673
.51	.06	-.4904
.61	.06	-.3732
.71	.05	-.2688
0.00	-.01	.0167
.11	-.02	-.3628
.21	-.02	-.2305
.31	-.02	-.2319
.40	-.02	-.1646
.51	-.01	-.1654
.61	-.01	-.0859
.71	-.00	-.0393

X/C	Z/C	CP
.11	.01	-.2133
.21	.00	-.1224
.31	.00	-.5154
.41	.01	-.5462
.51	.01	-.5091
.62	.01	-.4003
.71	.00	-.2824
.11	-.05	-.2415
.22	-.04	-.1818
.32	-.03	-.1445
.42	-.03	-.1432
.51	-.02	-.0729
.62	-.01	-.0110
.72	-.00	.0625

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17250

MACH .703

Q 25189.2

ALPW

-.52

BETA

0.00

P1 72736.78

PT1 101197.15

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.4471	0.00	.01	.5679	0.00	-.01	.1040	.11	.01	-.2683
.05	.05	-.0777	.05	.03	-.0326	.11	.03	-.0167	.21	.00	-.1275
.10	.06	-.2073	.10	.04	-.2147	.20	.05	-.1818	.31	.00	-.5499
.15	.06	-.2713	.15	.05	-.2943	.31	.06	-.3453	.41	.01	-.5779
.20	.07	-.3178	.20	.06	-.3539	.40	.07	-.5050	.51	.01	-.5317
.25	.07	-.3603	.25	.06	-.3983	.51	.06	-.5243	.62	.01	-.4178
.30	.07	-.3890	.30	.07	-.4425	.61	.06	-.3950	.71	.00	-.2926
.35	.07	-.4172	.35	.07	-.4753	.71	.05	-.2808	.11	-.05	-.1960
.40	.07	-.4313	.40	.07	-.4945	0.00	-.01	.0294	.22	-.04	-.1568
.45	.07	-.4339	.45	.07	-.4906	.11	-.02	-.2956	.32	-.03	-.1262
.50	.07	-.4147	.50	.07	-.4710	.21	-.02	-.2086	.42	-.03	-.1225
.55	.06	-.3947	.55	.06	-.4428	.31	-.02	-.1935	.51	-.02	-.0628
.60	.06	-.3657	.60	.06	-.4118	.40	-.02	-.1502	.62	-.01	-.0029
.65	.05	-.3385	.65	.05	-.4174	.51	-.01	-.1491	.72	-.00	.0704
.70	.05	-.2981	.70	.05	-.3834	.61	-.01	-.0795			
.75	.04	-.2539	.75	.04	-.3492	.71	-.00	-.0347			
.80	.03	-.2190	.80	.04	-.2327						
.85	.03	-.1720	.85	.03	-.2322						
.90	.02	-.1117	0.00	.01	.5372						
0.00	.03	.5747	.04	-.00	.0376						
.05	.01	-.3369	.09	-.01	-.2748						
.10	.01	-.2534	.14	-.01	-.2222						
.15	.00	-.2402	.19	-.01	-.2013						
.20	-.00	-.2352	.24	-.01	-.1878						
.25	-.00	-.2243	.29	-.01	-.1723						
.30	-.01	-.2283	.34	-.01	-.1594						
.35	-.01	-.2256	.39	-.01	-.1482						
.40	-.01	-.2293	.44	-.01	-.1291						
.45	-.01	-.2271	.49	-.01	-.0982						
.50	-.01	-.2171	.54	-.01	-.0703						
.55	-.01	-.1908	.59	-.01	-.0400						
.60	-.01	-.1647	.64	-.00	-.0388						
.65	-.01	-.1368	.69	-.00	.0260						
.70	-.00	-.1014	.74	.00	.0266						
.75	-.00	-.0673	.79	.00	.0486						
.80	-.00	-.0354	.84	.00	.0729						
.85	.00	.0038									
.90	.00	.0698									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17251

MACH .704

Q 25208.5

ALPW

.01

BETA

0.00

P1 72710.85

PT1 101196.92

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5173
.05	.05	-.1417
.10	.06	-.2520
.15	.06	-.3116
.20	.07	-.3534
.25	.07	-.3924
.30	.07	-.4245
.35	.07	-.4444
.40	.07	-.4626
.45	.07	-.4546
.50	.07	-.4373
.55	.06	-.4154
.60	.06	-.3833
.65	.05	-.3516
.70	.05	-.3110
.75	.04	-.2635
.80	.03	-.2256
.85	.03	-.1763
.90	.02	-.1224
0.00	.03	.5975
.05	.01	-.2715
.10	.01	-.2220
.15	.00	-.2270
.20	-.00	-.2181
.25	-.00	-.2017
.30	-.01	-.1987
.35	-.01	-.2035
.40	-.01	-.1975
.45	-.01	-.2036
.50	-.01	-.1907
.55	-.01	-.1715
.60	-.01	-.1473
.65	-.01	-.1216
.70	-.00	-.0869
.75	-.00	-.0553
.80	-.00	-.0217
.85	.00	.0156
.90	.00	.0574

X/C	Z/C	CP
0.00	.01	.6140
.05	.03	-.1064
.10	.04	-.2817
.15	.05	-.3594
.20	.06	-.4052
.25	.06	-.4467
.30	.07	-.4899
.35	.07	-.5159
.40	.07	-.5352
.45	.07	-.5241
.50	.07	-.4993
.55	.06	-.4653
.60	.06	-.4302
.65	.05	-.4291
.70	.05	-.4067
.75	.04	-.3570
.80	.04	-.2410
.85	.03	-.2395
0.00	.01	.5279
.04	-.00	.0794
.09	-.01	-.2064
.14	-.01	-.1761
.19	-.01	-.1796
.24	-.01	-.1523
.29	-.01	-.1413
.34	-.01	-.1321
.39	-.01	-.1264
.44	-.01	-.1083
.49	-.01	-.0813
.54	-.01	-.0541
.59	-.01	-.0263
.64	-.00	-.0255
.69	-.00	.0348
.74	.00	.0441
.79	.00	.0602
.84	.00	.0834

X/C	Z/C	CP
0.00	-.01	.1080
.11	.03	.0079
.20	.05	-.2545
.31	.06	-.3973
.40	.07	-.5578
.51	.06	-.5700
.61	.06	-.4242
.71	.05	-.3064
0.00	-.01	.0380
.11	-.02	-.2212
.21	-.02	-.1652
.31	-.02	-.1552
.40	-.02	-.1245
.51	-.01	-.1220
.61	-.01	-.0679
.71	-.00	-.0296

X/C	Z/C	CP
.11	.01	-.3537
.21	.00	-.1245
.31	.00	-.6059
.41	.01	-.6200
.51	.01	-.5608
.62	.01	-.4349
.71	.00	-.3059
.11	-.05	-.1507
.22	-.04	-.1216
.32	-.03	-.0977
.42	-.03	-.1044
.51	-.02	-.0458
.62	-.01	.0096
.72	-.00	.0811

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17252

MACH .704

Q 25208.7

ALPW

.55

BETA

0.00

P1 72716.52

PT1 101202.51

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5606	0.00	.01	.6341	0.00	-.01	.1161	.11	.01	-.4418
.05	.05	-.2045	.05	.03	-.2074	.11	.03	.0218	.21	.00	-.1286
.10	.06	-.3184	.10	.04	-.3595	.20	.05	-.2559	.31	.00	-.6660
.15	.06	-.3620	.15	.05	-.4301	.31	.06	-.4684	.41	.01	-.6648
.20	.07	-.3966	.20	.06	-.4695	.40	.07	-.6204	.51	.01	-.5938
.25	.07	-.4356	.25	.06	-.5047	.51	.06	-.6270	.62	.01	-.4570
.30	.07	-.4612	.30	.07	-.5385	.61	.06	-.4624	.71	.00	-.3201
.35	.07	-.4779	.35	.07	-.5593	.71	.05	-.3298	.11	-.05	-.1133
.40	.07	-.4912	.40	.07	-.5743	0.00	-.01	.0247	.22	-.04	-.0902
.45	.07	-.4889	.45	.07	-.5641	.11	-.02	-.1535	.32	-.03	-.0710
.50	.07	-.4623	.50	.07	-.5287	.21	-.02	-.1290	.42	-.03	-.0760
.55	.06	-.4351	.55	.06	-.4893	.31	-.02	-.1304	.51	-.02	-.0278
.60	.06	-.3989	.60	.06	-.4536	.40	-.02	-.1005	.62	-.01	.0176
.65	.05	-.3661	.65	.05	-.4522	.51	-.01	-.1019	.72	-.00	.0982
.70	.05	-.3178	.70	.05	-.4258	.61	-.01	-.0538			
.75	.04	-.2722	.75	.04	-.3872	.71	-.00	-.0196			
.80	.03	-.2321	.80	.04	-.2531						
.85	.03	-.1830	.85	.03	-.2546						
.90	.02	-.1205	0.00	.01	.5583						
0.00	.03	.6100	.04	-.00	.0314						
.05	.01	-.2017	.09	-.01	-.1546						
.10	.01	-.2068	.14	-.01	-.1226						
.15	.00	-.1806	.19	-.01	-.1309						
.20	-.00	-.1768	.24	-.01	-.1079						
.25	-.00	-.1716	.29	-.01	-.1063						
.30	-.01	-.1695	.34	-.01	-.0989						
.35	-.01	-.1798	.39	-.01	-.1014						
.40	-.01	-.1844	.44	-.01	-.0887						
.45	-.01	-.1850	.49	-.01	-.0597						
.50	-.01	-.1787	.54	-.01	-.0369						
.55	-.01	-.1562	.59	-.01	-.0110						
.60	-.01	-.1333	.64	-.00	-.0118						
.65	-.01	-.1086	.69	-.00	.0463						
.70	-.00	-.0796	.74	.00	.0421						
.75	-.00	-.0498	.79	.00	.0669						
.80	-.00	-.0218	.84	.00	.0893						
.85	.00	.0266									
.90	.00	.0499									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17253

MACH .703

Q 25191.5

ALPW

1.08

BETA

0.00

P1 72738.19

PT1 101201.46

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5941
.05	.05	-.2692
.10	.06	-.3749
.15	.06	-.4158
.20	.07	-.4414
.25	.07	-.4699
.30	.07	-.4916
.35	.07	-.5001
.40	.07	-.5152
.45	.07	-.5101
.50	.07	-.4808
.55	.06	-.4533
.60	.06	-.4166
.65	.05	-.3786
.70	.05	-.3282
.75	.04	-.2795
.80	.03	-.2358
.85	.03	-.1855
.90	.02	-.1234
0.00	.03	.5999
.05	.01	-.1514
.10	.01	-.1284
.15	.00	-.1193
.20	-.00	-.1298
.25	-.00	-.1435
.30	-.01	-.1488
.35	-.01	-.1656
.40	-.01	-.1562
.45	-.01	-.1517
.50	-.01	-.1553
.55	-.01	-.1344
.60	-.01	-.1151
.65	-.01	-.0988
.70	-.00	-.0724
.75	-.00	-.0398
.80	-.00	-.0106
.85	.00	.0270
.90	.00	.0601

X/C	Z/C	CP
0.00	.01	.6401
.05	.03	-.3085
.10	.04	-.4397
.15	.05	-.4932
.20	.06	-.5221
.25	.06	-.5593
.30	.07	-.5845
.35	.07	-.6054
.40	.07	-.6221
.45	.07	-.6016
.50	.07	-.5694
.55	.06	-.5261
.60	.06	-.4743
.65	.05	-.4767
.70	.05	-.4499
.75	.04	-.3888
.80	.04	-.2590
.85	.03	-.2584
0.00	.01	.5326
.04	-.00	.0978
.09	-.01	-.0996
.14	-.01	-.0820
.19	-.01	-.0785
.24	-.01	-.0841
.29	-.01	-.0806
.34	-.01	-.0770
.39	-.01	-.0803
.44	-.01	-.0674
.49	-.01	-.0441
.54	-.01	-.0205
.59	-.01	.0031
.64	-.00	.0000
.69	-.00	.0589
.74	.00	.0657
.79	.00	.0873
.84	.00	.0989

X/C	Z/C	CP
0.00	-.01	.1286
.11	.03	.0297
.20	.05	-.3163
.31	.06	-.5240
.40	.07	-.6703
.51	.06	-.6695
.61	.06	-.4820
.71	.05	-.3463
0.00	-.01	.0012
.11	-.02	-.1194
.21	-.02	-.1101
.31	-.02	-.1081
.40	-.02	-.0825
.51	-.01	-.0769
.61	-.01	-.0431
.71	-.00	-.0079

X/C	Z/C	CP
.11	.01	-.5283
.21	.00	-.1302
.31	.00	-.7149
.41	.01	-.7010
.51	.01	-.6212
.62	.01	-.4747
.71	.00	-.3331
.11	-.05	-.0557
.22	-.04	-.0531
.32	-.03	-.0475
.42	-.03	-.0457
.51	-.02	-.0103
.62	-.01	.0339
.72	-.00	.0781

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17254

MACH .704

Q 25209.2 ALPW 1.50

BETA

0.00 P1 72718.63

PT1 101205.19

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.6056	0.00	.01	.6311	0.00	-.01	.1356	.11	.01	-.6133
.05	.05	-.3246	.05	.03	-.3852	.11	.03	.0205	.21	.00	-.1388
.10	.06	-.4097	.10	.04	-.5043	.20	.05	-.3482	.31	.00	-.7664
.15	.06	-.4446	.15	.05	-.5526	.31	.06	-.5762	.41	.01	-.7349
.20	.07	-.4717	.20	.06	-.5794	.40	.07	-.7231	.51	.01	-.6464
.25	.07	-.5007	.25	.06	-.5996	.51	.06	-.7137	.62	.01	-.4878
.30	.07	-.5185	.30	.07	-.6243	.61	.06	-.5060	.71	.00	-.3435
.35	.07	-.5321	.35	.07	-.6448	.71	.05	-.3619	.11	-.05	-.0119
.40	.07	-.5444	.40	.07	-.6469	0.00	-.01	-.0273	.22	-.04	-.0223
.45	.07	-.5361	.45	.07	-.6229	.11	-.02	-.1167	.32	-.03	-.0224
.50	.07	-.5000	.50	.07	-.5772	.21	-.02	-.0907	.42	-.03	-.0287
.55	.06	-.4733	.55	.06	-.5352	.31	-.02	-.0941	.51	-.02	.0018
.60	.06	-.4317	.60	.06	-.4899	.40	-.02	-.0671	.62	-.01	.0443
.65	.05	-.3925	.65	.05	-.4889	.51	-.01	-.0603	.72	-.00	.0902
.70	.05	-.3429	.70	.05	-.4512	.61	-.01	-.0344			
.75	.04	-.2890	.75	.04	-.4116	.71	-.00	-.0041			
.80	.03	-.2437	.80	.04	-.2659						
.85	.03	-.1898	.85	.03	-.2599						
.90	.02	-.1251	0.00	.01	.4320						
0.00	.03	.5897	.04	-.00	.0988						
.05	.01	-.0948	.09	-.01	-.0650						
.10	.01	-.1000	.14	-.01	-.0595						
.15	.00	-.1004	.19	-.01	-.0513						
.20	-.00	-.0976	.24	-.01	-.0596						
.25	-.00	-.1009	.29	-.01	-.0607						
.30	-.01	-.1178	.34	-.01	-.0657						
.35	-.01	-.1280	.39	-.01	-.0638						
.40	-.01	-.1374	.44	-.01	-.0576						
.45	-.01	-.1375	.49	-.01	-.0362						
.50	-.01	-.1424	.54	-.01	-.0153						
.55	-.01	-.1244	.59	-.01	.0078						
.60	-.01	-.1140	.64	-.00	.0071						
.65	-.01	-.0834	.69	-.00	.0739						
.70	-.00	-.0628	.74	.00	.0703						
.75	-.00	-.0257	.79	.00	.0949						
.80	-.00	.0037	.84	.00	.1064						
.85	.00	.0313									
.90	.00	.0603									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17255

MACH .703

Q 25153.7 ALPW

1.95

BETA

0.00

P1 72790.96

PT1 101203.82

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.6059
.05	.05	-.3882
.10	.06	-.4644
.15	.06	-.4913
.20	.07	-.5062
.25	.07	-.5320
.30	.07	-.5500
.35	.07	-.5629
.40	.07	-.5701
.45	.07	-.5595
.50	.07	-.5212
.55	.06	-.4900
.60	.06	-.4441
.65	.05	-.4058
.70	.05	-.3539
.75	.04	-.2963
.80	.03	-.2450
.85	.03	-.1941
.90	.02	-.1271
0.00	.03	.5619
.05	.01	-.0440
.10	.01	-.0510
.15	.00	-.0589
.20	-.00	-.0660
.25	-.00	-.1026
.30	-.01	-.1022
.35	-.01	-.1069
.40	-.01	-.1250
.45	-.01	-.1264
.50	-.01	-.1278
.55	-.01	-.1171
.60	-.01	-.0985
.65	-.01	-.0690
.70	-.00	-.0457
.75	-.00	-.0165
.80	-.00	.0076
.85	.00	.0382
.90	.00	.0661

X/C	Z/C	CP
0.00	.01	.6145
.05	.03	-.4834
.10	.04	-.5743
.15	.05	-.6123
.20	.06	-.6208
.25	.06	-.6395
.30	.07	-.6636
.35	.07	-.6786
.40	.07	-.6870
.45	.07	-.6535
.50	.07	-.6082
.55	.06	-.5508
.60	.06	-.5046
.65	.05	-.5009
.70	.05	-.4655
.75	.04	-.4244
.80	.04	-.2715
.85	.03	-.2652
0.00	.01	.0894
.04	-.00	.0857
.09	-.01	-.0153
.14	-.01	-.0202
.19	-.01	-.0223
.24	-.01	-.0247
.29	-.01	-.0401
.34	-.01	-.0455
.39	-.01	-.0452
.44	-.01	-.0402
.49	-.01	-.0231
.54	-.01	-.0018
.59	-.01	.0184
.64	-.00	.0201
.69	-.00	.0842
.74	.00	.0765
.79	.00	.0972
.84	.00	.1114

X/C	Z/C	CP
0.00	-.01	.1323
.11	.03	-.0040
.20	.05	-.3980
.31	.06	-.6301
.40	.07	-.7957
.51	.06	-.7670
.61	.06	-.5265
.71	.05	-.3771
0.00	-.01	-.0826
.11	-.02	-.0995
.21	-.02	-.0789
.31	-.02	-.0786
.40	-.02	-.0540
.51	-.01	-.0549
.61	-.01	-.0365
.71	-.00	-.0037

X/C	Z/C	CP
.11	.01	-.7172
.21	.00	-.1469
.31	.00	-.8131
.41	.01	-.7692
.51	.01	-.6653
.62	.01	-.5005
.71	.00	-.3527
.11	-.05	.0330
.22	-.04	.0050
.32	-.03	-.0013
.42	-.03	-.0079
.51	-.02	.0157
.62	-.01	.0538
.72	-.00	.0998

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17256

MACH .704

Q 25198.4

ALPW

2.62

BETA

0.00

P1 72733.70

PT1 101205.94

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5874	0.00	.01	.5408	0.00	-.01	.1354	.11	.01	-.8981
.05	.05	-.4842	.05	.03	-.6354	.11	.03	-.0612	.21	.00	-.1615
.10	.06	-.5342	.10	.04	-.7033	.20	.05	-.4721	.31	.00	-.9005
.15	.06	-.5539	.15	.05	-.7077	.31	.06	-.6963	.41	.01	-.8195
.20	.07	-.5591	.20	.06	-.7235	.40	.07	-.8888	.51	.01	-.6913
.25	.07	-.5845	.25	.06	-.7211	.51	.06	-.8523	.62	.01	-.5237
.30	.07	-.6004	.30	.07	-.7365	.61	.06	-.5520	.71	.00	-.3662
.35	.07	-.6054	.35	.07	-.7351	.71	.05	-.3929	.11	-.05	.0911
.40	.07	-.6144	.40	.07	-.7371	0.00	-.01	-.1934	.22	-.04	.0495
.45	.07	-.5884	.45	.07	-.7001	.11	-.02	-.0854	.32	-.03	.0336
.50	.07	-.5512	.50	.07	-.6439	.21	-.02	-.0744	.42	-.03	.0205
.55	.06	-.5094	.55	.06	-.5800	.31	-.02	-.0746	.51	-.02	.0343
.60	.06	-.4659	.60	.06	-.5284	.40	-.02	-.0384	.62	-.01	.0684
.65	.05	-.4189	.65	.05	-.5354	.51	-.01	-.0385	.72	-.00	.1122
.70	.05	-.3630	.70	.05	-.4936	.61	-.01	-.0219			
.75	.04	-.3012	.75	.04	-.4404	.71	-.00	.0019			
.80	.03	-.2611	.80	.04	-.2770						
.85	.03	-.1972	.85	.03	-.2761						
.90	.02	-.1250	0.00	.01	.3620						
0.00	.03	.5040	.04	-.00	.0749						
.05	.01	.0200	.09	-.01	.0492						
.10	.01	.0095	.14	-.01	.0295						
.15	.00	.0020	.19	-.01	.0393						
.20	-.00	-.0188	.24	-.01	.0030						
.25	-.00	-.0353	.29	-.01	-.0045						
.30	-.01	-.0568	.34	-.01	-.0139						
.35	-.01	-.0762	.39	-.01	-.0155						
.40	-.01	-.0884	.44	-.01	-.0147						
.45	-.01	-.0994	.49	-.01	-.0004						
.50	-.01	-.0999	.54	-.01	.0172						
.55	-.01	-.0996	.59	-.01	.0364						
.60	-.01	-.0825	.64	-.00	.0322						
.65	-.01	-.0553	.69	-.00	.0960						
.70	-.00	-.0333	.74	.00	.0937						
.75	-.00	-.0103	.79	.00	.1057						
.80	-.00	.0202	.84	.00	.1211						
.85	.00	.0502									
.90	.00	.0784									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17257

MACH .703

Q 25164.0

ALPW

3.01

BETA

0.00

P1 72789.81

PT1 101215.78

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5758
.05	.05	-.5438
.10	.06	-.5897
.15	.06	-.5892
.20	.07	-.5956
.25	.07	-.6090
.30	.07	-.6243
.35	.07	-.6204
.40	.07	-.6293
.45	.07	-.6095
.50	.07	-.5669
.55	.06	-.5271
.60	.06	-.4782
.65	.05	-.4282
.70	.05	-.3727
.75	.04	-.3115
.80	.03	-.2624
.85	.03	-.2006
.90	.02	-.1279
0.00	.03	.4380
.05	.01	.0580
.10	.01	.0129
.15	.00	.0115
.20	-.00	-.0026
.25	-.00	-.0529
.30	-.01	-.0518
.35	-.01	-.0682
.40	-.01	-.0762
.45	-.01	-.0860
.50	-.01	-.0920
.55	-.01	-.0785
.60	-.01	-.0641
.65	-.01	-.0551
.70	-.00	-.0257
.75	-.00	-.0039
.80	-.00	.0209
.85	.00	.0526
.90	.00	.0743

X/C	Z/C	CP
0.00	.01	.4840
.05	.03	-.7008
.10	.04	-.7626
.15	.05	-.7724
.20	.06	-.7623
.25	.06	-.7688
.30	.07	-.7774
.35	.07	-.7678
.40	.07	-.7673
.45	.07	-.7274
.50	.07	-.6657
.55	.06	-.5955
.60	.06	-.5403
.65	.05	-.5406
.70	.05	-.5032
.75	.04	-.4471
.80	.04	-.2814
.85	.03	-.2760
0.00	.01	.4191
.04	-.00	.0833
.09	-.01	.0911
.14	-.01	.0591
.19	-.01	.0583
.24	-.01	.0241
.29	-.01	.0138
.34	-.01	.0056
.39	-.01	-.0010
.44	-.01	-.0013
.49	-.01	.0139
.54	-.01	.0282
.59	-.01	.0458
.64	-.00	.0484
.69	-.00	.0945
.74	.00	.0983
.79	.00	.1106
.84	.00	.1227

X/C	Z/C	CP
0.00	-.01	.1469
.11	.03	-.0996
.20	.05	-.5353
.31	.06	-.7612
.40	.07	-.9939
.51	.06	-.8941
.61	.06	-.5632
.71	.05	-.4057
0.00	-.01	-.2994
.11	-.02	-.0770
.21	-.02	-.0701
.31	-.02	-.0652
.40	-.02	-.0314
.51	-.01	-.0332
.61	-.01	-.0170
.71	-.00	-.0004

X/C	Z/C	CP
.11	.01	-1.0379
.21	.00	-.1758
.31	.00	-.9363
.41	.01	-.8531
.51	.01	-.6967
.62	.01	-.5329
.71	.00	-.3710
.11	-.05	.1264
.22	-.04	.0704
.32	-.03	.0498
.42	-.03	.0355
.51	-.02	.0450
.62	-.01	.0755
.72	-.00	.1196

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17258

MACH .704

Q 25214.4

ALPW

4.00

BETA

0.00

P1 72721.46

PT1 101214.46

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4937
.05	.05	-.7069
.10	.06	-.7061
.15	.06	-.6816
.20	.07	-.6766
.25	.07	-.6733
.30	.07	-.6878
.35	.07	-.6725
.40	.07	-.6909
.45	.07	-.6599
.50	.07	-.6104
.55	.06	-.5599
.60	.06	-.5033
.65	.05	-.4502
.70	.05	-.3886
.75	.04	-.3230
.80	.03	-.2687
.85	.03	-.2038
.90	.02	-.1296
0.00	.03	.2879
.05	.01	.1454
.10	.01	.0771
.15	.00	.0657
.20	-.00	.0614
.25	-.00	-.0102
.30	-.01	-.0017
.35	-.01	-.0233
.40	-.01	-.0242
.45	-.01	-.0444
.50	-.01	-.0545
.55	-.01	-.0429
.60	-.01	-.0334
.65	-.01	-.0169
.70	-.00	-.0051
.75	-.00	.0167
.80	-.00	.0321
.85	.00	.0626
.90	.00	.0961

X/C	Z/C	CP
0.00	.01	.2795
.05	.03	-.9639
.10	.04	-.9410
.15	.05	-.9107
.20	.06	-.8859
.25	.06	-.8551
.30	.07	-.8562
.35	.07	-.8423
.40	.07	-.8368
.45	.07	-.7838
.50	.07	-.6996
.55	.06	-.6331
.60	.06	-.5617
.65	.05	-.5528
.70	.05	-.5196
.75	.04	-.4565
.80	.04	-.2741
.85	.03	-.2710
0.00	.01	.1129
.04	-.00	.0767
.09	-.01	.1409
.14	-.01	.1303
.19	-.01	.1280
.24	-.01	.0797
.29	-.01	.0606
.34	-.01	.0451
.39	-.01	.0365
.44	-.01	.0319
.49	-.01	.0423
.54	-.01	.0541
.59	-.01	.0679
.64	-.00	.0772
.69	-.00	.1061
.74	.00	.1149
.79	.00	.1216
.84	.00	.1305

X/C	Z/C	CP
0.00	-.01	.1504
.11	.03	-.2051
.20	.05	-.6450
.31	.06	-.8666
.40	.07	-1.1561
.51	.06	-.9748
.61	.06	-.5786
.71	.05	-.4171
0.00	-.01	-.6350
.11	-.02	-.0679
.21	-.02	-.0594
.31	-.02	-.0591
.40	-.02	-.0186
.51	-.01	-.0278
.61	-.01	-.0121
.71	-.00	.0113

X/C	Z/C	CP
.11	.01	-1.4813
.21	.00	-.2462
.31	.00	-1.0377
.41	.01	-.7883
.51	.01	-.6923
.62	.01	-.5252
.71	.00	-.3600
.11	-.05	.1887
.22	-.04	.1206
.32	-.03	.0896
.42	-.03	.0641
.51	-.02	.0697
.62	-.01	.0938
.72	-.00	.1302

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17259

MACH .703

Q 25174.2

ALPW

5.96

BETA

0.00

P1 72776.96

PT1 101216.42

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.2221
.05	.05	-.9330
.10	.06	-.9403
.15	.06	-.8719
.20	.07	-.8341
.25	.07	-.8309
.30	.07	-.8166
.35	.07	-.8044
.40	.07	-.7859
.45	.07	-.7377
.50	.07	-.6748
.55	.06	-.6061
.60	.06	-.5351
.65	.05	-.4699
.70	.05	-.3993
.75	.04	-.3285
.80	.03	-.2686
.85	.03	-.1998
.90	.02	-.1268
0.00	.03	-.1008
.05	.01	.2849
.10	.01	.1877
.15	.00	.1539
.20	-.00	.1389
.25	-.00	.0696
.30	-.01	.0629
.35	-.01	.0524
.40	-.01	.0405
.45	-.01	.0128
.50	-.01	.0189
.55	-.01	.0056
.60	-.01	.0111
.65	-.01	.0245
.70	-.00	.0267
.75	-.00	.0497
.80	-.00	.0591
.85	.00	.0816
.90	.00	.1009

X/C	Z/C	CP
0.00	.01	-.0974
.05	.03	-1.7570
.10	.04	-1.5658
.15	.05	-1.4457
.20	.06	-.9884
.25	.06	-.8919
.30	.07	-.9434
.35	.07	-.8921
.40	.07	-.8499
.45	.07	-.7833
.50	.07	-.6904
.55	.06	-.5991
.60	.06	-.5162
.65	.05	-.5238
.70	.05	-.4724
.75	.04	-.4043
.80	.04	-.2143
.85	.03	-.1933
0.00	.01	-.0395
.04	-.00	-.0730
.09	-.01	.2134
.14	-.01	.2340
.19	-.01	.2271
.24	-.01	.1495
.29	-.01	.1226
.34	-.01	.1027
.39	-.01	.0876
.44	-.01	.0741
.49	-.01	.0760
.54	-.01	.0787
.59	-.01	.0885
.64	-.00	.0810
.69	-.00	.1101
.74	.00	.1108
.79	.00	.1110
.84	.00	.1294

X/C	Z/C	CP
0.00	-.01	.1328
.11	.03	-.5694
.20	.05	-.8611
.31	.06	-1.1345
.40	.07	-1.0926
.51	.06	-.8726
.61	.06	-.5318
.71	.05	-.3974
0.00	-.01	-1.3132
.11	-.02	-.0970
.21	-.02	-.0739
.31	-.02	-.0756
.40	-.02	-.0228
.51	-.01	-.0239
.61	-.01	-.0145
.71	-.00	.0070

X/C	Z/C	CP
.11	.01	-1.6108
.21	.00	-.2493
.31	.00	-.9793
.41	.01	-.7854
.51	.01	-.6491
.62	.01	-.5241
.71	.00	-.4073
.11	-.05	.2495
.22	-.04	.1657
.32	-.03	.1241
.42	-.03	.0959
.51	-.02	.0850
.62	-.01	.0991
.72	-.00	.1259

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 21

TP 17260

MACH .704

Q

25219.9

ALPW

.07

BETA

0.00

P1 72713.46

PT1 101213.81

Y/B/2 = .51

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5158	0.00	.01	.6140	0.00	-.01	.1102	.11	.01	-.3498
.05	.05	-.1414	.05	.03	-.1294	.11	.03	.0141	.21	.00	-.1263
.10	.06	-.2605	.10	.04	-.2911	.20	.05	-.2109	.31	.00	-.6065
.15	.06	-.3185	.15	.05	-.3676	.31	.06	-.3882	.41	.01	-.6215
.20	.07	-.3584	.20	.06	-.4122	.40	.07	-.5517	.51	.01	-.5619
.25	.07	-.3941	.25	.06	-.4537	.51	.06	-.5760	.62	.01	-.4359
.30	.07	-.4294	.30	.07	-.4946	.61	.06	-.4256	.71	.00	-.3073
.35	.07	-.4449	.35	.07	-.5141	.71	.05	-.3067	.11	-.05	-.1439
.40	.07	-.4681	.40	.07	-.5331	0.00	-.01	.0364	.22	-.04	-.1177
.45	.07	-.4605	.45	.07	-.5310	.11	-.02	-.2124	.32	-.03	-.0941
.50	.07	-.4391	.50	.07	-.5012	.21	-.02	-.1561	.42	-.03	-.1010
.55	.06	-.4222	.55	.06	-.4677	.31	-.02	-.1570	.51	-.02	-.0430
.60	.06	-.3842	.60	.06	-.4338	.40	-.02	-.1209	.62	-.01	.0128
.65	.05	-.3549	.65	.05	-.4422	.51	-.01	-.1107	.72	-.00	.0832
.70	.05	-.3121	.70	.05	-.4040	.61	-.01	-.0654			
.75	.04	-.2675	.75	.04	-.3692	.71	-.00	-.0260			
.80	.03	-.2272	.80	.04	-.2420						
.85	.03	-.1774	.85	.03	-.2340						
.90	.02	-.1176	0.00	.01	.4433						
0.00	.03	.6004	.04	-.00	.0777						
.05	.01	-.2649	.09	-.01	-.1904						
.10	.01	-.2164	.14	-.01	-.1648						
.15	.00	-.2125	.19	-.01	-.1664						
.20	-.00	-.2048	.24	-.01	-.1413						
.25	-.00	-.2050	.29	-.01	-.1337						
.30	-.01	-.2068	.34	-.01	-.1315						
.35	-.01	-.2036	.39	-.01	-.1249						
.40	-.01	-.2040	.44	-.01	-.1078						
.45	-.01	-.2077	.49	-.01	-.0801						
.50	-.01	-.2068	.54	-.01	-.0531						
.55	-.01	-.1750	.59	-.01	-.0257						
.60	-.01	-.1630	.64	-.00	-.0329						
.65	-.01	-.1323	.69	-.00	.0428						
.70	-.00	-.0968	.74	.00	.0378						
.75	-.00	-.0677	.79	.00	.0575						
.80	-.00	-.0365	.84	.00	.0772						
.85	.00	-.0009									
.90	.00	.0332									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17263

MACH .602

Q 20116.0

ALPH

-1.88

BETA

0.00

P1 79210.76

PT1 101217.92

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.1338
.05	.05	.0652
.10	.06	-.0862
.15	.06	-.1528
.20	.07	-.2127
.25	.07	-.2559
.30	.07	-.2895
.35	.07	-.3129
.40	.07	-.3286
.45	.07	-.3351
.50	.07	-.3211
.55	.06	-.3100
.60	.06	-.2890
.65	.05	-.2705
.70	.05	-.2373
.75	.04	-.2047
.80	.03	-.1793
.85	.03	-.1417
.90	.02	-.0958
0.00	.03	.4230
.05	.01	-.4593
.10	.01	-.3357
.15	.00	-.2950
.20	-.00	-.2877
.25	-.00	-.2657
.30	-.01	-.2660
.35	-.01	-.2526
.40	-.01	-.2539
.45	-.01	-.2288
.50	-.01	-.2341
.55	-.01	-.2155
.60	-.01	-.1937
.65	-.01	-.1585
.70	-.00	-.1296
.75	-.00	-.0999
.80	-.00	-.0597
.85	.00	-.0303
.90	.00	.0642

X/C	Z/C	CP
0.00	.01	.2728
.05	.03	.1376
.10	.04	-.0518
.15	.05	-.1448
.20	.06	-.2083
.25	.06	-.2598
.30	.07	-.3039
.35	.07	-.3345
.40	.07	-.3578
.45	.07	-.3622
.50	.07	-.3558
.55	.06	-.3345
.60	.06	-.3212
.65	.05	-.3182
.70	.05	-.2611
.75	.04	-.2575
.80	.04	-.1943
.85	.03	-.1556
0.00	.01	.2584
.04	-.00	.0045
.09	-.01	-.3951
.14	-.01	-.3384
.19	-.01	-.2843
.24	-.01	-.2543
.29	-.01	-.2331
.34	-.01	-.2078
.39	-.01	-.1906
.44	-.01	-.1636
.49	-.01	-.1315
.54	-.01	-.1006
.59	-.01	-.0684
.64	-.00	-.0530
.69	-.00	-.0001
.74	.00	.0120
.79	.00	.0239
.84	.00	.0406

X/C	Z/C	CP
0.00	-.01	.0706
.11	.03	-.1482
.20	.05	-.1108
.31	.06	-.2012
.40	.07	-.3484
.51	.06	-.3745
.61	.06	-.2904
.71	.05	-.2139
0.00	-.01	-.0394
.11	-.02	-.4598
.21	-.02	-.2637
.31	-.02	-.2659
.40	-.02	-.1854
.51	-.01	-.1507
.61	-.01	-.0956
.71	-.00	-.0495

X/C	Z/C	CP
.11	.01	-.0886
.21	.00	-.1113
.31	.00	-.3904
.41	.01	-.4327
.51	.01	-.4152
.62	.01	-.3406
.71	.00	-.2417
.11	-.05	-.5313
.22	-.04	-.3200
.32	-.03	-.2082
.42	-.03	-.1688
.51	-.02	-.1012
.62	-.01	-.0431
.72	-.00	.0193

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17264

MACH .603

Q 20138.8

ALPW

-1.44

BETA

0.00

P1 79178.96

PT1 101214.11

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.2542	0.00	.01	.3839	0.00	-.01	.0780	.11	.01	-.1355
.05	.05	.0121	.05	.03	.0800	.11	.03	-.0918	.21	.00	-.1122
.10	.06	-.1242	.10	.04	-.1005	.20	.05	-.1164	.31	.00	-.4220
.15	.06	-.1923	.15	.05	-.1839	.31	.06	-.2330	.41	.01	-.4564
.20	.07	-.2356	.20	.06	-.2476	.40	.07	-.3822	.51	.01	-.4361
.25	.07	-.2805	.25	.06	-.2912	.51	.06	-.4056	.62	.01	-.3544
.30	.07	-.3117	.30	.07	-.3346	.61	.06	-.3103	.71	.00	-.2501
.35	.07	-.3338	.35	.07	-.3631	.71	.05	-.2282	.11	-.05	-.3808
.40	.07	-.3552	.40	.07	-.3873	0.00	-.01	-.0018	.22	-.04	-.2223
.45	.07	-.3499	.45	.07	-.3890	.11	-.02	-.3440	.32	-.03	-.1668
.50	.07	-.3393	.50	.07	-.3767	.21	-.02	-.2406	.42	-.03	-.1447
.55	.06	-.3236	.55	.06	-.3534	.31	-.02	-.2437	.51	-.02	-.0856
.60	.06	-.3032	.60	.06	-.3379	.40	-.02	-.1798	.62	-.01	-.0267
.65	.05	-.2817	.65	.05	-.3391	.51	-.01	-.1469	.72	-.00	.0393
.70	.05	-.2459	.70	.05	-.2723	.61	-.01	-.0942			
.75	.04	-.2136	.75	.04	-.2360	.71	-.00	-.0493			
.80	.03	-.1832	.80	.04	-.2013						
.85	.03	-.1472	.85	.03	-.1621						
.90	.02	-.0998	0.00	.01	.3128						
0.00	.03	.4887	.04	-.00	.0553						
.05	.01	-.4179	.09	-.01	-.3088						
.10	.01	-.2964	.14	-.01	-.2858						
.15	.00	-.2636	.19	-.01	-.2815						
.20	-.00	-.2668	.24	-.01	-.2248						
.25	-.00	-.2455	.29	-.01	-.2053						
.30	-.01	-.2476	.34	-.01	-.1875						
.35	-.01	-.2444	.39	-.01	-.1728						
.40	-.01	-.2417	.44	-.01	-.1513						
.45	-.01	-.2409	.49	-.01	-.1183						
.50	-.01	-.2302	.54	-.01	-.0875						
.55	-.01	-.2080	.59	-.01	-.0582						
.60	-.01	-.1809	.64	-.00	-.0563						
.65	-.01	-.1563	.69	-.00	.0073						
.70	-.00	-.1271	.74	.00	.0130						
.75	-.00	-.0937	.79	.00	.0308						
.80	-.00	-.0597	.84	.00	.0514						
.85	.00	-.0221									
.90	.00	.0071									

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17265

MACH .603

Q 20155.6

ALPW

-.90

BETA

0.00

P1 79153.35

PT1 101209.23

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.3713
.05	.05	-.0451
.10	.06	-.1661
.15	.06	-.2342
.20	.07	-.2718
.25	.07	-.3124
.30	.07	-.3402
.35	.07	-.3613
.40	.07	-.3791
.45	.07	-.3730
.50	.07	-.3602
.55	.06	-.3423
.60	.06	-.3200
.65	.05	-.2963
.70	.05	-.2534
.75	.04	-.2239
.80	.03	-.1865
.85	.03	-.1534
.90	.02	-.1043
0.00	.03	.5441
.05	.01	-.3457
.10	.01	-.2597
.15	.00	-.2241
.20	-.00	-.2272
.25	-.00	-.2270
.30	-.01	-.2282
.35	-.01	-.2256
.40	-.01	-.2179
.45	-.01	-.2221
.50	-.01	-.2088
.55	-.01	-.1886
.60	-.01	-.1687
.65	-.01	-.1403
.70	-.00	-.1088
.75	-.00	-.0802
.80	-.00	-.0463
.85	.00	-.0125
.90	.00	.0401

X/C	Z/C	CP
0.00	.01	.5105
.05	.03	.0069
.10	.04	-.1618
.15	.05	-.2381
.20	.06	-.2919
.25	.06	-.3370
.30	.07	-.3751
.35	.07	-.4030
.40	.07	-.4192
.45	.07	-.4203
.50	.07	-.4037
.55	.06	-.3776
.60	.06	-.3573
.65	.05	-.3575
.70	.05	-.3367
.75	.04	-.3035
.80	.04	-.2111
.85	.03	-.1877
0.00	.01	.4074
.04	-.00	.0569
.09	-.01	-.2350
.14	-.01	-.2306
.19	-.01	-.2427
.24	-.01	-.1938
.29	-.01	-.1787
.34	-.01	-.1617
.39	-.01	-.1499
.44	-.01	-.1319
.49	-.01	-.1027
.54	-.01	-.0747
.59	-.01	-.0455
.64	-.00	-.0400
.69	-.00	.0183
.74	.00	.0203
.79	.00	.0368
.84	.00	.0613

X/C	Z/C	CP
0.00	-.01	.0880
.11	.03	-.0397
.20	.05	-.1271
.31	.06	-.2685
.40	.07	-.4235
.51	.06	-.4429
.61	.06	-.3359
.71	.05	-.2462
0.00	-.01	.0261
.11	-.02	-.2704
.21	-.02	-.2088
.31	-.02	-.2071
.40	-.02	-.1647
.51	-.01	-.1331
.61	-.01	-.0870
.71	-.00	-.0434

X/C	Z/C	CP
.11	.01	-.1993
.21	.00	-.1082
.31	.00	-.4629
.41	.01	-.4856
.51	.01	-.4571
.62	.01	-.3711
.71	.00	-.2638
.11	-.05	-.2338
.22	-.04	-.1807
.32	-.03	-.1394
.42	-.03	-.1367
.51	-.02	-.0715
.62	-.01	-.0143
.72	-.00	.0540

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17266

MACH .603

Q 20154.6

ALPW

-.48

BETA

0.00

P1 79154.00

PT1 101208.66

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.4446	0.00	.01	.5608	0.00	-.01	.0894	.11	.01	-.2452
.05	.05	-.0876	.05	.03	-.0424	.11	.03	-.0064	.21	.00	-.1143
.10	.06	-.2095	.10	.04	-.2108	.20	.05	-.1385	.31	.00	-.4934
.15	.06	-.2626	.15	.05	-.2872	.31	.06	-.3007	.41	.01	-.5153
.20	.07	-.3036	.20	.06	-.3328	.40	.07	-.4600	.51	.01	-.4772
.25	.07	-.3393	.25	.06	-.3737	.51	.06	-.4723	.62	.01	-.3857
.30	.07	-.3647	.30	.07	-.4063	.61	.06	-.3548	.71	.00	-.2747
.35	.07	-.3802	.35	.07	-.4268	.71	.05	-.2626	.11	-.05	-.1961
.40	.07	-.3949	.40	.07	-.4474	0.00	-.01	.0395	.22	-.04	-.1524
.45	.07	-.3898	.45	.07	-.4414	.11	-.02	-.2395	.32	-.03	-.1184
.50	.07	-.3751	.50	.07	-.4228	.21	-.02	-.1865	.42	-.03	-.1212
.55	.06	-.3569	.55	.06	-.3952	.31	-.02	-.1832	.51	-.02	-.0604
.60	.06	-.3274	.60	.06	-.3734	.40	-.02	-.1472	.62	-.01	-.0055
.65	.05	-.3044	.65	.05	-.3758	.51	-.01	-.1258	.72	-.00	.0629
.70	.05	-.2695	.70	.05	-.3485	.61	-.01	-.0778			
.75	.04	-.2289	.75	.04	-.3207	.71	-.00	-.0392			
.80	.03	-.1992	.80	.04	-.2179						
.85	.03	-.1589	.85	.03	-.1920						
.90	.02	-.1113	0.00	.01	.4771						
0.00	.03	.5736	.04	-.00	.0275						
.05	.01	-.3062	.09	-.01	-.1959						
.10	.01	-.2270	.14	-.01	-.1986						
.15	.00	-.2150	.19	-.01	-.1772						
.20	-.00	-.2166	.24	-.01	-.1653						
.25	-.00	-.1968	.29	-.01	-.1576						
.30	-.01	-.2000	.34	-.01	-.1435						
.35	-.01	-.1971	.39	-.01	-.1351						
.40	-.01	-.2002	.44	-.01	-.1175						
.45	-.01	-.1974	.49	-.01	-.0903						
.50	-.01	-.1963	.54	-.01	-.0626						
.55	-.01	-.1788	.59	-.01	-.0373						
.60	-.01	-.1604	.64	-.00	-.0251						
.65	-.01	-.1307	.69	-.00	.0246						
.70	-.00	-.0994	.74	.00	.0259						
.75	-.00	-.0685	.79	.00	.0438						
.80	-.00	-.0390	.84	.00	.0659						
.85	.00	-.0077									
.90	.00	.0450									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17267

MACH .603

Q 20153.6

ALPW

.10

BETA

0.00

P1 79161.47

PT1 101214.67

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5308
.05	.05	-.1550
.10	.06	-.2629
.15	.06	-.3088
.20	.07	-.3475
.25	.07	-.3764
.30	.07	-.3973
.35	.07	-.4102
.40	.07	-.4231
.45	.07	-.4135
.50	.07	-.3956
.55	.06	-.3730
.60	.06	-.3446
.65	.05	-.3199
.70	.05	-.2787
.75	.04	-.2370
.80	.03	-.2015
.85	.03	-.1629
.90	.02	-.1103
0.00	.03	.5924
.05	.01	-.2392
.10	.01	-.1899
.15	.00	-.1948
.20	-.00	-.1900
.25	-.00	-.1772
.30	-.01	-.1810
.35	-.01	-.1861
.40	-.01	-.1826
.45	-.01	-.1822
.50	-.01	-.1806
.55	-.01	-.1644
.60	-.01	-.1407
.65	-.01	-.1075
.70	-.00	-.0855
.75	-.00	-.0589
.80	-.00	-.0296
.85	.00	-.0046
.90	.00	.0539

X/C	Z/C	CP
0.00	.01	.6112
.05	.03	-.1353
.10	.04	-.2817
.15	.05	-.3478
.20	.06	-.3846
.25	.06	-.4175
.30	.07	-.4481
.35	.07	-.4681
.40	.07	-.4841
.45	.07	-.4720
.50	.07	-.4505
.55	.06	-.4245
.60	.06	-.3943
.65	.05	-.3987
.70	.05	-.3759
.75	.04	-.3383
.80	.04	-.2293
.85	.03	-.1879
0.00	.01	.5210
.04	-.00	.0395
.09	-.01	-.1222
.14	-.01	-.1495
.19	-.01	-.1354
.24	-.01	-.1346
.29	-.01	-.1249
.34	-.01	-.1154
.39	-.01	-.1124
.44	-.01	-.0962
.49	-.01	-.0723
.54	-.01	-.0484
.59	-.01	-.0223
.64	-.00	-.0149
.69	-.00	.0344
.74	.00	.0379
.79	.00	.0542
.84	.00	.0755

X/C	Z/C	CP
0.00	-.01	.0969
.11	.03	.0222
.20	.05	-.1568
.31	.06	-.3488
.40	.07	-.5123
.51	.06	-.5166
.61	.06	-.3847
.71	.05	-.2821
0.00	-.01	.0393
.11	-.02	-.1938
.21	-.02	-.1523
.31	-.02	-.1569
.40	-.02	-.1192
.51	-.01	-.0971
.61	-.01	-.0660
.71	-.00	-.0306

X/C	Z/C	CP
.11	.01	-.3276
.21	.00	-.1148
.31	.00	-.5408
.41	.01	-.5545
.51	.01	-.5088
.62	.01	-.4051
.71	.00	-.2897
.11	-.05	-.1374
.22	-.04	-.1146
.32	-.03	-.0893
.42	-.03	-.0952
.51	-.02	-.0432
.62	-.01	.0084
.72	-.00	.0730

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17268

MACH .603

Q 20136.8

ALPW

.57

BETA

0.00

P1 79182.18

PT1 101214.87

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP	X/C	Z/C	CP
0.00	.03	.5668	0.00	.01	.6254	0.00	-.01	.1015	.11	.01	-.3968
.05	.05	-.2159	.05	.03	-.2080	.11	.03	.0480	.21	.00	-.1118
.10	.06	-.3136	.10	.04	-.3474	.20	.05	-.2062	.31	.00	-.5825
.15	.06	-.3480	.15	.05	-.4012	.31	.06	-.3936	.41	.01	-.5884
.20	.07	-.3766	.20	.06	-.4324	.40	.07	-.5558	.51	.01	-.5345
.25	.07	-.4056	.25	.06	-.4609	.51	.06	-.5572	.62	.01	-.4218
.30	.07	-.4230	.30	.07	-.4897	.61	.06	-.4151	.71	.00	-.3044
.35	.07	-.4363	.35	.07	-.5023	.71	.05	-.3022	.11	-.05	-.1126
.40	.07	-.4455	.40	.07	-.5162	0.00	-.01	.0313	.22	-.04	-.0887
.45	.07	-.4350	.45	.07	-.5009	.11	-.02	-.1391	.32	-.03	-.0721
.50	.07	-.4126	.50	.07	-.4733	.21	-.02	-.1248	.42	-.03	-.0761
.55	.06	-.3892	.55	.06	-.4414	.31	-.02	-.1268	.51	-.02	-.0300
.60	.06	-.3590	.60	.06	-.4108	.40	-.02	-.1021	.62	-.01	.0140
.65	.05	-.3296	.65	.05	-.4112	.51	-.01	-.0927	.72	-.00	.0831
.70	.05	-.2881	.70	.05	-.3835	.61	-.01	-.0559			
.75	.04	-.2495	.75	.04	-.3530	.71	-.00	-.0196			
.80	.03	-.2139	.80	.04	-.2368						
.85	.03	-.1703	.85	.03	-.2060						
.90	.02	-.1156	0.00	.01	.5989						
0.00	.03	.5993	.04	-.00	.0402						
.05	.01	-.1888	.09	-.01	-.0972						
.10	.01	-.1558	.14	-.01	-.1185						
.15	.00	-.1521	.19	-.01	-.1117						
.20	-.00	-.1491	.24	-.01	-.1025						
.25	-.00	-.1495	.29	-.01	-.0992						
.30	-.01	-.1486	.34	-.01	-.0912						
.35	-.01	-.1489	.39	-.01	-.0899						
.40	-.01	-.1569	.44	-.01	-.0776						
.45	-.01	-.1530	.49	-.01	-.0547						
.50	-.01	-.1534	.54	-.01	-.0337						
.55	-.01	-.1464	.59	-.01	-.0093						
.60	-.01	-.1201	.64	-.00	.0034						
.65	-.01	-.1046	.69	-.00	.0459						
.70	-.00	-.0783	.74	.00	.0433						
.75	-.00	-.0467	.79	.00	.0596						
.80	-.00	-.0189	.84	.00	.0801						
.85	.00	.0114									
.90	.00	.0957									

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17269

MACH .602

Q 20118.7

ALPW

1.04

BETA

0.00

P1 79198.65

PT1 101209.34

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$
[illegible]

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17270

MACH .602

Q 20096.2

ALPW

1.50

BETA

0.00

P1 79226.83

PT1 101210.07

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5968
.05	.05	-.3437
.10	.06	-.4103
.15	.06	-.4257
.20	.07	-.4435
.25	.07	-.4660
.30	.07	-.4755
.35	.07	-.4853
.40	.07	-.4919
.45	.07	-.4716
.50	.07	-.4463
.55	.06	-.4175
.60	.06	-.3830
.65	.05	-.3524
.70	.05	-.3060
.75	.04	-.2632
.80	.03	-.2242
.85	.03	-.1769
.90	.02	-.1189
0.00	.03	.5731
.05	.01	-.0701
.10	.01	-.0824
.15	.00	-.0930
.20	-.00	-.0899
.25	-.00	-.1110
.30	-.01	-.1107
.35	-.01	-.1113
.40	-.01	-.1192
.45	-.01	-.1241
.50	-.01	-.1312
.55	-.01	-.1184
.60	-.01	-.1003
.65	-.01	-.0807
.70	-.00	-.0546
.75	-.00	-.0264
.80	-.00	.0004
.85	.00	.0279
.90	.00	.0991

X/C	Z/C	CP
0.00	.01	.6198
.05	.03	-.3821
.10	.04	-.4781
.15	.05	-.5060
.20	.06	-.5275
.25	.06	-.5458
.30	.07	-.5608
.35	.07	-.5667
.40	.07	-.5722
.45	.07	-.5539
.50	.07	-.5184
.55	.06	-.4808
.60	.06	-.4431
.65	.05	-.4450
.70	.05	-.3468
.75	.04	-.3481
.80	.04	-.2519
.85	.03	-.2006
0.00	.01	.5579
.04	-.00	.0468
.09	-.01	-.0080
.14	-.01	-.0493
.19	-.01	-.0595
.24	-.01	-.0527
.29	-.01	-.0566
.34	-.01	-.0582
.39	-.01	-.0567
.44	-.01	-.0537
.49	-.01	-.0315
.54	-.01	-.0122
.59	-.01	.0067
.64	-.00	.0295
.69	-.00	.0701
.74	.00	.0744
.79	.00	.0857
.84	.00	.0979

X/C	Z/C	CP
0.00	-.01	.1189
.11	.03	.0412
.20	.05	-.3037
.31	.06	-.4920
.40	.07	-.6464
.51	.06	-.6248
.61	.06	-.4585
.71	.05	-.3360
0.00	-.01	-.0228
.11	-.02	-.1112
.21	-.02	-.0884
.31	-.02	-.0862
.40	-.02	-.0709
.51	-.01	-.0634
.61	-.01	-.0372
.71	-.00	-.0107

X/C	Z/C	CP
.11	.01	-.5587
.21	.00	-.1173
.31	.00	-.6665
.41	.01	-.6434
.51	.01	-.5843
.62	.01	-.4553
.71	.00	-.3260
.11	-.05	-.0260
.22	-.04	-.0319
.32	-.03	-.0299
.42	-.03	-.0335
.51	-.02	-.0040
.62	-.01	.0381
.72	-.00	.0825

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17271

MACH .603

Q 20125.3

ALPW

2.07

BETA

0.00

P1 79191.81

PT1 101210.60

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5931
.05	.05	-.4109
.10	.06	-.4642
.15	.06	-.4710
.20	.07	-.4820
.25	.07	-.5023
.30	.07	-.5119
.35	.07	-.5098
.40	.07	-.5161
.45	.07	-.4972
.50	.07	-.4661
.55	.06	-.4376
.60	.06	-.4005
.65	.05	-.3646
.70	.05	-.3166
.75	.04	-.2709
.80	.03	-.2320
.85	.03	-.1809
.90	.02	-.1221
0.00	.03	.5243
.05	.01	-.0142
.10	.01	-.0438
.15	.00	-.0565
.20	-.00	-.0710
.25	-.00	-.0668
.30	-.01	-.0964
.35	-.01	-.0970
.40	-.01	-.0952
.45	-.01	-.1022
.50	-.01	-.1070
.55	-.01	-.0929
.60	-.01	-.0927
.65	-.01	-.0707
.70	-.00	-.0439
.75	-.00	-.0220
.80	-.00	.0044
.85	.00	.0262
.90	.00	.0555

X/C	Z/C	CP
0.00	.01	.5905
.05	.03	-.4857
.10	.04	-.5520
.15	.05	-.5757
.20	.06	-.5810
.25	.06	-.5924
.30	.07	-.6037
.35	.07	-.6157
.40	.07	-.6108
.45	.07	-.5829
.50	.07	-.5440
.55	.06	-.4972
.60	.06	-.4640
.65	.05	-.4774
.70	.05	-.3761
.75	.04	-.3685
.80	.04	-.2593
.85	.03	-.2104
0.00	.01	.5452
.04	-.00	.0455
.09	-.01	.0423
.14	-.01	-.0051
.19	-.01	-.0072
.24	-.01	-.0208
.29	-.01	-.0275
.34	-.01	-.0323
.39	-.01	-.0349
.44	-.01	-.0327
.49	-.01	-.0136
.54	-.01	.0040
.59	-.01	.0211
.64	-.00	.0331
.69	-.00	.0791
.74	.00	.0793
.79	.00	.0933
.84	.00	.1028

X/C	Z/C	CP
0.00	-.01	.1309
.11	.03	.0233
.20	.05	-.3509
.31	.06	-.5545
.40	.07	-.6949
.51	.06	-.6646
.61	.06	-.4856
.71	.05	-.3568
0.00	-.01	-.0841
.11	-.02	-.0898
.21	-.02	-.0752
.31	-.02	-.0726
.40	-.02	-.0541
.51	-.01	-.0499
.61	-.01	-.0291
.71	-.00	-.0060

X/C	Z/C	CP
.11	.01	-.6447
.21	.00	-.1237
.31	.00	-.7081
.41	.01	-.6842
.51	.01	-.6071
.62	.01	-.4737
.71	.00	-.3404
.11	-.05	.0261
.22	-.04	.0032
.32	-.03	-.0023
.42	-.03	-.0117
.51	-.02	.0118
.62	-.01	.0500
.72	-.00	.0941

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17272

MACH .603

Q 20132.6

ALPW

2.54

BETA

0.00

P1 79187.18

PT1 101214.72

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5763
.05	.05	-.4799
.10	.06	-.5152
.15	.06	-.5197
.20	.07	-.5181
.25	.07	-.5311
.30	.07	-.5383
.35	.07	-.5395
.40	.07	-.5369
.45	.07	-.5179
.50	.07	-.4846
.55	.06	-.4511
.60	.06	-.4107
.65	.05	-.3755
.70	.05	-.3238
.75	.04	-.2781
.80	.03	-.2371
.85	.03	-.1842
.90	.02	-.1239
0.00	.03	.4650
.05	.01	.0253
.10	.01	-.0111
.15	.00	-.0318
.20	-.00	-.0476
.25	-.00	-.0645
.30	-.01	-.0656
.35	-.01	-.0657
.40	-.01	-.0757
.45	-.01	-.0932
.50	-.01	-.0930
.55	-.01	-.0897
.60	-.01	-.0769
.65	-.01	-.0497
.70	-.00	-.0374
.75	-.00	-.0085
.80	-.00	.0160
.85	.00	.0340
.90	.00	.0609

X/C	Z/C	CP
0.00	.01	.5295
.05	.03	-.5814
.10	.04	-.6317
.15	.05	-.6372
.20	.06	-.6282
.25	.06	-.6424
.30	.07	-.6479
.35	.07	-.6428
.40	.07	-.6412
.45	.07	-.6101
.50	.07	-.5686
.55	.06	-.5174
.60	.06	-.4787
.65	.05	-.4829
.70	.05	-.3732
.75	.04	-.3733
.80	.04	-.2659
.85	.03	-.2092
0.00	.01	.4919
.04	-.00	.0465
.09	-.01	.0471
.14	-.01	.0475
.19	-.01	.0424
.24	-.01	.0053
.29	-.01	-.0065
.34	-.01	-.0124
.39	-.01	-.0162
.44	-.01	-.0153
.49	-.01	-.0003
.54	-.01	.0159
.59	-.01	.0330
.64	-.00	.0552
.69	-.00	.0860
.74	.00	.0863
.79	.00	.0985
.84	.00	.1109

X/C	Z/C	CP
0.00	-.01	.1256
.11	.03	-.0221
.20	.05	-.4435
.31	.06	-.6291
.40	.07	-.7320
.51	.06	-.6988
.61	.06	-.5079
.71	.05	-.3741
0.00	-.01	-.1494
.11	-.02	-.0761
.21	-.02	-.0708
.31	-.02	-.0747
.40	-.02	-.0445
.51	-.01	-.0405
.61	-.01	-.0244
.71	-.00	-.0006

X/C	Z/C	CP
.11	.01	-.7333
.21	.00	-.1278
.31	.00	-.7561
.41	.01	-.7178
.51	.01	-.6306
.62	.01	-.4898
.71	.00	-.3527
.11	-.05	.0657
.22	-.04	.0330
.32	-.03	.0173
.42	-.03	.0058
.51	-.02	.0242
.62	-.01	.0584
.72	-.00	.1011

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17273

MACH .602

Q

20114.7

ALPW

3.04

BETA

0.00

P1 79205.57

PT1 101211.39

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5406
.05	.05	-.5539
.10	.06	-.5654
.15	.06	-.5584
.20	.07	-.5502
.25	.07	-.5548
.30	.07	-.5657
.35	.07	-.5522
.40	.07	-.5610
.45	.07	-.5399
.50	.07	-.5018
.55	.06	-.4648
.60	.06	-.4253
.65	.05	-.3848
.70	.05	-.3339
.75	.04	-.2853
.80	.03	-.2405
.85	.03	-.1871
.90	.02	-.1250
0.00	.03	.3908
.05	.01	.0729
.10	.01	.0266
.15	.00	.0014
.20	-.00	-.0224
.25	-.00	-.0426
.30	-.01	-.0393
.35	-.01	-.0478
.40	-.01	-.0475
.45	-.01	-.0779
.50	-.01	-.0753
.55	-.01	-.0713
.60	-.01	-.0548
.65	-.01	-.0409
.70	-.00	-.0214
.75	-.00	-.0003
.80	-.00	.0153
.85	.00	.0426
.90	.00	.0706

X/C	Z/C	CP
0.00	.01	.4220
.05	.03	-.6839
.10	.04	-.7091
.15	.05	-.7009
.20	.06	-.6858
.25	.06	-.6797
.30	.07	-.6903
.35	.07	-.6776
.40	.07	-.6792
.45	.07	-.6393
.50	.07	-.5897
.55	.06	-.5366
.60	.06	-.4968
.65	.05	-.4955
.70	.05	-.4061
.75	.04	-.3863
.80	.04	-.2715
.85	.03	-.2136
0.00	.01	.4032
.04	-.00	.0180
.09	-.01	.0700
.14	-.01	.0764
.19	-.01	.0713
.24	-.01	.0318
.29	-.01	.0177
.34	-.01	.0094
.39	-.01	.0019
.44	-.01	.0028
.49	-.01	.0160
.54	-.01	.0295
.59	-.01	.0449
.64	-.00	.0571
.69	-.00	.0935
.74	.00	.1016
.79	.00	.1063
.84	.00	.1157

X/C	Z/C	CP
0.00	-.01	.1327
.11	.03	-.0586
.20	.05	-.4607
.31	.06	-.6700
.40	.07	-.7927
.51	.06	-.7464
.61	.06	-.5300
.71	.05	-.3889
0.00	-.01	-.2558
.11	-.02	-.0662
.21	-.02	-.0649
.31	-.02	-.0649
.40	-.02	-.0446
.51	-.01	-.0301
.61	-.01	-.0191
.71	-.00	.0022

X/C	Z/C	CP
.11	.01	-.8431
.21	.00	-.1400
.31	.00	-.8021
.41	.01	-.7493
.51	.01	-.6541
.62	.01	-.5058
.71	.00	-.3654
.11	-.05	.1043
.22	-.04	.0599
.32	-.03	.0401
.42	-.03	.0278
.51	-.02	.0374
.62	-.01	.0680
.72	-.00	.1084

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17274

MACH .602

Q 20107.0

ALPW

4.04

BETA

0.00

P1 79213.64

PT1 101210.02

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.4171
.05	.05	-.7032
.10	.06	-.6775
.15	.06	-.6446
.20	.07	-.6149
.25	.07	-.6097
.30	.07	-.6169
.35	.07	-.6075
.40	.07	-.6070
.45	.07	-.5763
.50	.07	-.5360
.55	.06	-.4958
.60	.06	-.4482
.65	.05	-.4051
.70	.05	-.3463
.75	.04	-.2961
.80	.03	-.2486
.85	.03	-.1915
.90	.02	-.1264
0.00	.03	.1701
.05	.01	.1617
.10	.01	.0920
.15	.00	.0557
.20	-.00	.0249
.25	-.00	.0016
.30	-.01	.0045
.35	-.01	.0033
.40	-.01	-.0163
.45	-.01	-.0483
.50	-.01	-.0512
.55	-.01	-.0363
.60	-.01	-.0269
.65	-.01	-.0258
.70	-.00	-.0152
.75	-.00	.0155
.80	-.00	.0368
.85	.00	.0559
.90	.00	.0735

X/C	Z/C	CP
0.00	.01	.1624
.05	.03	-.8798
.10	.04	-.8568
.15	.05	-.8010
.20	.06	-.7632
.25	.06	-.7559
.30	.07	-.7489
.35	.07	-.7315
.40	.07	-.7204
.45	.07	-.6804
.50	.07	-.6274
.55	.06	-.5708
.60	.06	-.5139
.65	.05	-.5126
.70	.05	-.4281
.75	.04	-.4116
.80	.04	-.2674
.85	.03	-.2078
0.00	.01	.2144
.04	-.00	.0102
.09	-.01	.1422
.14	-.01	.1286
.19	-.01	.1248
.24	-.01	.0796
.29	-.01	.0605
.34	-.01	.0483
.39	-.01	.0365
.44	-.01	.0328
.49	-.01	.0414
.54	-.01	.0525
.59	-.01	.0649
.64	-.00	.0818
.69	-.00	.1061
.74	.00	.1039
.79	.00	.1127
.84	.00	.1239

X/C	Z/C	CP
0.00	-.01	.1435
.11	.03	-.1395
.20	.05	-.5685
.31	.06	-.7893
.40	.07	-.8623
.51	.06	-.7963
.61	.06	-.5650
.71	.05	-.4161
0.00	-.01	-.5616
.11	-.02	-.0594
.21	-.02	-.0567
.31	-.02	-.0633
.40	-.02	-.0222
.51	-.01	-.0259
.61	-.01	-.0154
.71	-.00	.0040

X/C	Z/C	CP
.11	.01	-1.1278
.21	.00	-.1686
.31	.00	-.8692
.41	.01	-.7982
.51	.01	-.6679
.62	.01	-.5256
.71	.00	-.3731
.11	-.05	.1710
.22	-.04	.1087
.32	-.03	.0789
.42	-.03	.0579
.51	-.02	.0623
.62	-.01	.0834
.72	-.00	.1178

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17275

MACH .602

Q 20117.8

ALPW

6.01

BETA

0.00

P1 79198.75

PT1 101208.44

Y/B72 = .31

$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.0177
.05	.05	-.9893
.10	.06	-.8850
.15	.06	-.8111
.20	.07	-.7740
.25	.07	-.7446
.30	.07	-.7304
.35	.07	-.7048
.40	.07	-.6870
.45	.07	-.6459
.50	.07	-.5936
.55	.06	-.5419
.60	.06	-.4861
.65	.05	-.4304
.70	.05	-.3685
.75	.04	-.3116
.80	.03	-.2560
.85	.03	-.1939
.90	.02	-.1256
0.00	.03	-.3841
.05	.01	.3024
.10	.01	.2032
.15	.00	.1514
.20	-.00	.1116
.25	-.00	.0817
.30	-.01	.0727
.35	-.01	.0711
.40	-.01	.0551
.45	-.01	.0076
.50	-.01	.0056
.55	-.01	.0090
.60	-.01	.0167
.65	-.01	.0236
.70	-.00	.0329
.75	-.00	.0530
.80	-.00	.0606
.85	.00	.0823
.90	.00	.0971

X/C	Z/C	CP
0.00	.01	-.4174
.05	.03	-1.4024
.10	.04	-1.1095
.15	.05	-1.0266
.20	.06	-.9384
.25	.06	-.9031
.30	.07	-.8603
.35	.07	-.8190
.40	.07	-.7776
.45	.07	-.7273
.50	.07	-.6541
.55	.06	-.5834
.60	.06	-.5130
.65	.05	-.5165
.70	.05	-.4348
.75	.04	-.3972
.80	.04	-.2366
.85	.03	-.1805
0.00	.01	-.3797
.04	-.00	-.0357
.09	-.01	.2481
.14	-.01	.2457
.19	-.01	.2275
.24	-.01	.1583
.29	-.01	.1335
.34	-.01	.1092
.39	-.01	.0905
.44	-.01	.0803
.49	-.01	.0826
.54	-.01	.0847
.59	-.01	.0898
.64	-.00	.0936
.69	-.00	.1146
.74	.00	.1177
.79	.00	.1231
.84	.00	.1244

X/C	Z/C	CP
0.00	-.01	.1343
.11	.03	-.4775
.20	.05	-.8130
.31	.06	-.9385
.40	.07	-.8753
.51	.06	-.7712
.61	.06	-.5202
.71	.05	-.3857
0.00	-.01	-1.2151
.11	-.02	-.0838
.21	-.02	-.0613
.31	-.02	-.0663
.40	-.02	-.0187
.51	-.01	-.0206
.61	-.01	-.0136
.71	-.00	.0059

X/C	Z/C	CP
.11	.01	-1.6504
.21	.00	-.2379
.31	.00	-.8704
.41	.01	-.7743
.51	.01	-.6437
.62	.01	-.4889
.71	.00	-.3481
.11	-.05	.2467
.22	-.04	.1659
.32	-.03	.1221
.42	-.03	.0943
.51	-.02	.0857
.62	-.01	.0976
.72	-.00	.1237

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 22

TP 17276

MACH .603

Q 20134.3

ALPW

.06

BETA

0.00

P1 79169.30

PT1 101199.36

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5257
.05	.05	-.1455
.10	.06	-.2597
.15	.06	-.3115
.20	.07	-.3404
.25	.07	-.3711
.30	.07	-.3944
.35	.07	-.4083
.40	.07	-.4207
.45	.07	-.4124
.50	.07	-.3940
.55	.06	-.3749
.60	.06	-.3439
.65	.05	-.3184
.70	.05	-.2773
.75	.04	-.2398
.80	.03	-.2070
.85	.03	-.1626
.90	.02	-.1106
0.00	.03	.5935
.05	.01	-.2392
.10	.01	-.1907
.15	.00	-.1806
.20	-.00	-.1763
.25	-.00	-.1786
.30	-.01	-.1733
.35	-.01	-.1737
.40	-.01	-.1743
.45	-.01	-.1825
.50	-.01	-.1814
.55	-.01	-.1655
.60	-.01	-.1480
.65	-.01	-.1155
.70	-.00	-.0916
.75	-.00	-.0473
.80	-.00	-.0181
.85	.00	.0037
.90	.00	.0663

X/C	Z/C	CP
0.00	.01	.6118
.05	.03	-.1333
.10	.04	-.2757
.15	.05	-.3384
.20	.06	-.3798
.25	.06	-.4147
.30	.07	-.4462
.35	.07	-.4683
.40	.07	-.4795
.45	.07	-.4712
.50	.07	-.4513
.55	.06	-.4191
.60	.06	-.3911
.65	.05	-.3857
.70	.05	-.3158
.75	.04	-.3143
.80	.04	-.2283
.85	.03	-.1863
0.00	.01	.5222
.04	-.00	.0421
.09	-.01	-.1799
.14	-.01	-.1612
.19	-.01	-.1620
.24	-.01	-.1378
.29	-.01	-.1312
.34	-.01	-.1190
.39	-.01	-.1120
.44	-.01	-.0966
.49	-.01	-.0719
.54	-.01	-.0483
.59	-.01	-.0232
.64	-.00	-.0082
.69	-.00	.0339
.74	.00	.0335
.79	.00	.0483
.84	.00	.0708

X/C	Z/C	CP
0.00	-.01	.0957
.11	.03	.0222
.20	.05	-.1731
.31	.06	-.3419
.40	.07	-.5096
.51	.06	-.5134
.61	.06	-.3843
.71	.05	-.2814
0.00	-.01	.0431
.11	-.02	-.1949
.21	-.02	-.1526
.31	-.02	-.1534
.40	-.02	-.1204
.51	-.01	-.1044
.61	-.01	-.0668
.71	-.00	-.0301

X/C	Z/C	CP
.11	.01	-.3252
.21	.00	-.1098
.31	.00	-.5373
.41	.01	-.5498
.51	.01	-.5062
.62	.01	-.4078
.71	.00	-.2856
.11	-.05	-.1408
.22	-.04	-.1184
.32	-.03	-.0923
.42	-.03	-.0996
.51	-.02	-.0448
.62	-.01	.0068
.72	-.00	.0741

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 23

TP 17277

MACH .704

Q 25197.0

ALPW

2.14

BETA

0.00

P1 72704.57

PT1 101176.37

$$Y/B/2 = .31$$
$$Y/B/2 = .74$$
$$Y/B/2 = 1.003$$
$$Y/B/2 = 1.011$$

X/C	Z/C	CP
0.00	.03	.6017
.05	.05	-.4175
.10	.06	-.4754
.15	.06	-.5022
.20	.07	-.5191
.25	.07	-.5437
.30	.07	-.5634
.35	.07	-.5724
.40	.07	-.5826
.45	.07	-.5646
.50	.07	-.5350
.55	.06	-.4941
.60	.06	-.4486
.65	.05	-.4048
.70	.05	-.3519
.75	.04	-.3013
.80	.03	-.2552
.85	.03	-.1959
.90	.02	-.1287
0.00	.03	.5468
.05	.01	-.0297
.10	.01	-.0509
.15	.00	-.0684
.20	-.00	-.0820
.25	-.00	-.0971
.30	-.01	-.0969
.35	-.01	-.0977
.40	-.01	-.1040
.45	-.01	-.1152
.50	-.01	-.1143
.55	-.01	-.1104
.60	-.01	-.0977
.65	-.01	-.0754
.70	-.00	-.0445
.75	-.00	-.0196
.80	-.00	.0058
.85	.00	.0345
.90	.00	.0792

X/C	Z/C	CP
0.00	.01	.6070
.05	.03	-.5172
.10	.04	-.6161
.15	.05	-.6334
.20	.06	-.6435
.25	.06	-.6693
.30	.07	-.6939
.35	.07	-.6904
.40	.07	-.6988
.45	.07	-.6642
.50	.07	-.6140
.55	.06	-.5574
.60	.06	-.5113
.65	.05	-.5077
.70	.05	-.4199
.75	.04	-.4050
.80	.04	-.2712
.85	.03	-.2108
0.00	.01	.5112
.04	-.00	.0529
.09	-.01	.0040
.14	-.01	-.0073
.19	-.01	.0016
.24	-.01	-.0217
.29	-.01	-.0330
.34	-.01	-.0360
.39	-.01	-.0401
.44	-.01	-.0319
.49	-.01	-.0173
.54	-.01	.0036
.59	-.01	.0232
.64	-.00	.0349
.69	-.00	.0837
.74	.00	.0812
.79	.00	.0945
.84	.00	.1109

X/C	Z/C	CP
0.00	-.01	.1308
.11	.03	-.0018
.20	.05	-.3724
.31	.06	-.5973
.40	.07	-.8312
.51	.06	-.7906
.61	.06	-.5336
.71	.05	-.3817
0.00	-.01	-.1115
.11	-.02	-.0940
.21	-.02	-.0777
.31	-.02	-.0729
.40	-.02	-.0488
.51	-.01	-.0457
.61	-.01	-.0260
.71	-.00	.0026

X/C	Z/C	CP
.11	.01	-.7678
.21	.00	-.1528
.31	.00	-.8501
.41	.01	-.7806
.51	.01	-.7029
.62	.01	-.5093
.71	.00	-.3558
.11	-.05	.0531
.22	-.04	.0178
.32	-.03	.0091
.42	-.03	-.0041
.51	-.02	.0220
.62	-.01	.0599
.72	-.00	.1029

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 23

TP 17278

MACH .704

Q 25197.2

ALPW

3.03

BETA

0.00

P1 72700.62

PT1 101172.86

Y/B/2 = .31

Y/B/2 = .74

Y/B/2 = 1.003

Y/B/2 = 1.011

X/C	Z/C	CP
0.00	.03	.5707
.05	.05	-.5519
.10	.06	-.5855
.15	.06	-.5883
.20	.07	-.5912
.25	.07	-.6104
.30	.07	-.6249
.35	.07	-.6237
.40	.07	-.6316
.45	.07	-.6147
.50	.07	-.5732
.55	.06	-.5292
.60	.06	-.4796
.65	.05	-.4293
.70	.05	-.3685
.75	.04	-.3123
.80	.03	-.2595
.85	.03	-.2010
.90	.02	-.1306
0.00	.03	.4416
.05	.01	.0563
.10	.01	.0138
.15	.00	-.0129
.20	-.00	-.0358
.25	-.00	-.0539
.30	-.01	-.0522
.35	-.01	-.0574
.40	-.01	-.0599
.45	-.01	-.0783
.50	-.01	-.0848
.55	-.01	-.0837
.60	-.01	-.0673
.65	-.01	-.0484
.70	-.00	-.0318
.75	-.00	-.0041
.80	-.00	.0193
.85	.00	.0488
.90	.00	.1217

X/C	Z/C	CP
0.00	.01	.4738
.05	.03	-.7096
.10	.04	-.7730
.15	.05	-.7683
.20	.06	-.7652
.25	.06	-.7747
.30	.07	-.7773
.35	.07	-.7682
.40	.07	-.7700
.45	.07	-.7175
.50	.07	-.6651
.55	.06	-.5909
.60	.06	-.5400
.65	.05	-.5366
.70	.05	-.4604
.75	.04	-.4014
.80	.04	-.2814
.85	.03	-.2127
0.00	.01	.5170
.04	-.00	.0449
.09	-.01	.0867
.14	-.01	.0644
.19	-.01	.0637
.24	-.01	.0274
.29	-.01	.0123
.34	-.01	.0053
.39	-.01	.0013
.44	-.01	-.0000
.49	-.01	.0138
.54	-.01	.0286
.59	-.01	.0454
.64	-.00	.0517
.69	-.00	.0989
.74	.00	.1002
.79	.00	.1106
.84	.00	.1226

X/C	Z/C	CP
0.00	-.01	.1380
.11	.03	-.0742
.20	.05	-.4825
.31	.06	-.7132
.40	.07	-.9364
.51	.06	-.8978
.61	.06	-.5635
.71	.05	-.4016
0.00	-.01	-.3191
.11	-.02	-.0761
.21	-.02	-.0691
.31	-.02	-.0728
.40	-.02	-.0328
.51	-.01	-.0333
.61	-.01	-.0184
.71	-.00	.0018

X/C	Z/C	CP
.11	.01	-1.0581
.21	.00	-.1844
.31	.00	-.9513
.41	.01	-.8538
.51	.01	-.7687
.62	.01	-.5222
.71	.00	-.3621
.11	-.05	.1220
.22	-.04	.0724
.32	-.03	.0496
.42	-.03	.0336
.51	-.02	.0467
.62	-.01	.0778
.72	-.00	.1187

Table III. (concluded)

NASA LANGLEY

7 X 10 HIGH SPEED TUNNEL

TEST 107

RUN 23

TP 17279

MACH .702

Q 25123.2

ALPW

.03

BETA

0.00

P1 72804.13

PT1 101177.85

$$Y/B/2 = .31$$

Y/B/2 = .74

$$Y/B/2 = 1.003$$

Y/B/2 - 1.011

X/C	Z/C	CP
0.00	.03	.5027
.05	.05	-.1387
.10	.06	-.2626
.15	.06	-.3163
.20	.07	-.3519
.25	.07	-.3924
.30	.07	-.4249
.35	.07	-.4468
.40	.07	-.4622
.45	.07	-.4588
.50	.07	-.4397
.55	.06	-.4162
.60	.06	-.3859
.65	.05	-.3526
.70	.05	-.3020
.75	.04	-.2652
.80	.03	-.2257
.85	.03	-.1751
.90	.02	-.1165
0.00	.03	.5982
.05	.01	-.2628
.10	.01	-.2126
.15	.00	-.2023
.20	-.00	-.1983
.25	-.00	-.2019
.30	-.01	-.1993
.35	-.01	-.1995
.40	-.01	-.2009
.45	-.01	-.1978
.50	-.01	-.1991
.55	-.01	-.1835
.60	-.01	-.1565
.65	-.01	-.1282
.70	-.00	-.1036
.75	-.00	-.0744
.80	-.00	-.0401
.85	.00	-.0036
.90	.00	.0452

X/C	Z/C	CP
0.00	.01	.6127
.05	.03	-.1170
.10	.04	-.2805
.15	.05	-.3570
.20	.06	-.4044
.25	.06	-.4473
.30	.07	-.4882
.35	.07	-.5088
.40	.07	-.5319
.45	.07	-.5225
.50	.07	-.4922
.55	.06	-.4618
.60	.06	-.4310
.65	.05	-.4309
.70	.05	-.3438
.75	.04	-.3395
.80	.04	-.2414
.85	.03	-.1877
0.00	.01	.5009
.04	-.00	.0402
.09	-.01	-.2097
.14	-.01	-.1772
.19	-.01	-.1717
.24	-.01	-.1489
.29	-.01	-.1397
.34	-.01	-.1305
.39	-.01	-.1239
.44	-.01	-.1063
.49	-.01	-.0800
.54	-.01	-.0535
.59	-.01	-.0266
.64	-.00	-.0180
.69	-.00	.0354
.74	.00	.0360
.79	.00	.0589
.84	.00	.0725

X/C	Z/C	CP
0.00	-.01	.0986
.11	.03	.0265
.20	.05	-.1866
.31	.06	-.3668
.40	.07	-.5276
.51	.06	-.5692
.61	.06	-.4213
.71	.05	-.3028
0.00	-.01	.0247
.11	-.02	-.2154
.21	-.02	-.1597
.31	-.02	-.1604
.40	-.02	-.1229
.51	-.01	-.1070
.61	-.01	-.0683
.71	-.00	-.0271

X/C	Z/C	CP
.11	.01	-.3475
.21	.00	-.1218
.31	.00	-.6004
.41	.01	-.6126
.51	.01	-.5639
.62	.01	-.4367
.71	.00	-.3034
.11	-.05	-.1465
.22	-.04	-.1203
.32	-.03	-.0966
.42	-.03	-.1041
.51	-.02	-.0456
.62	-.01	.0100
.72	-.00	.0808

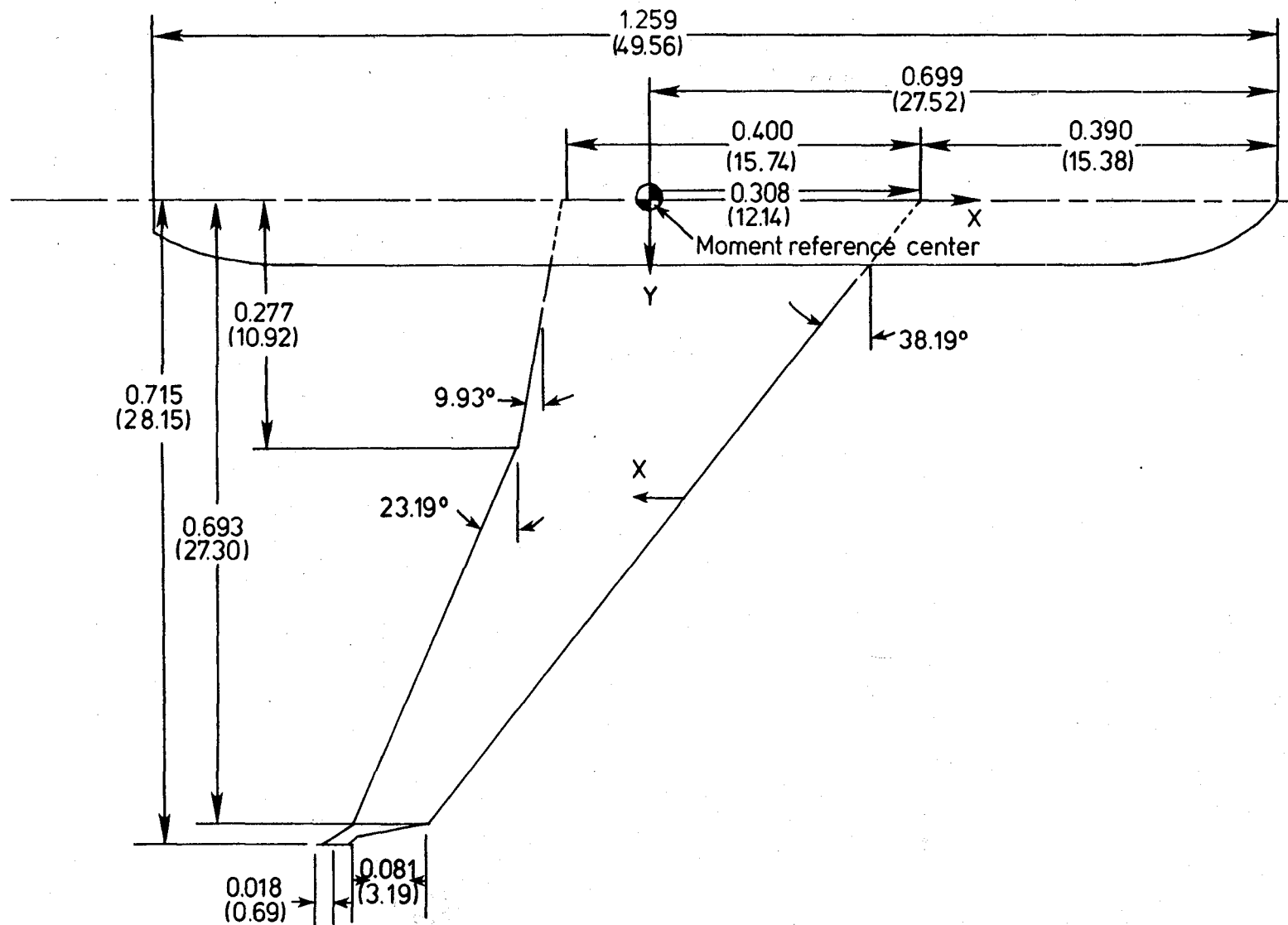


Figure 1. Drawings of the model. Dimensions are in meters (inches). (a) Planview of wing-winglet model and fuselage.

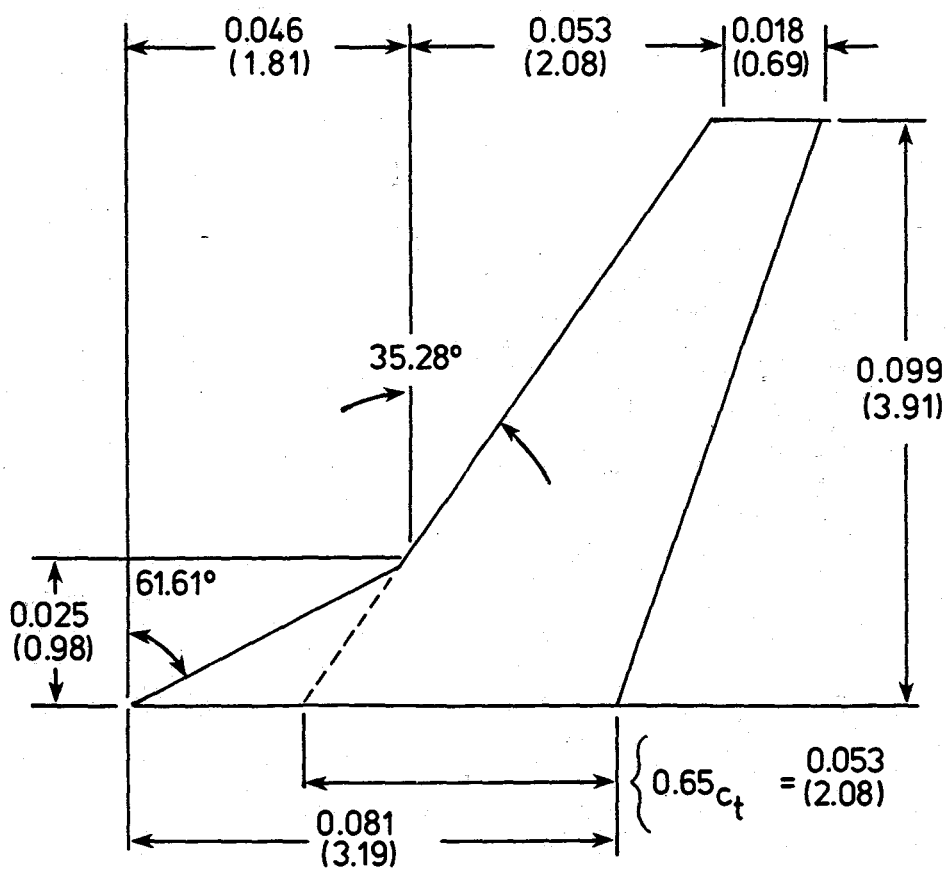


Figure 1(b). Winglet planform.

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L-82-9408

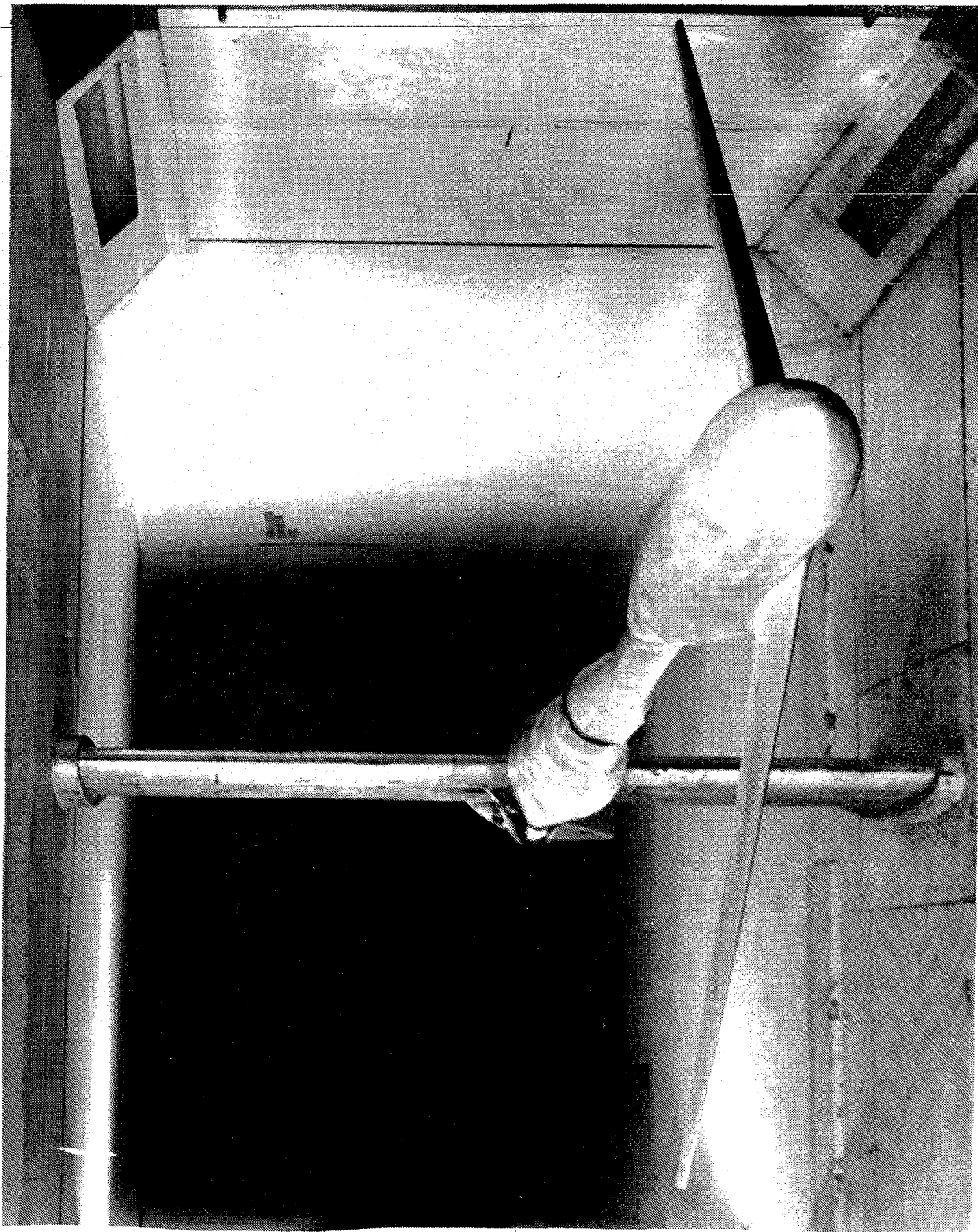
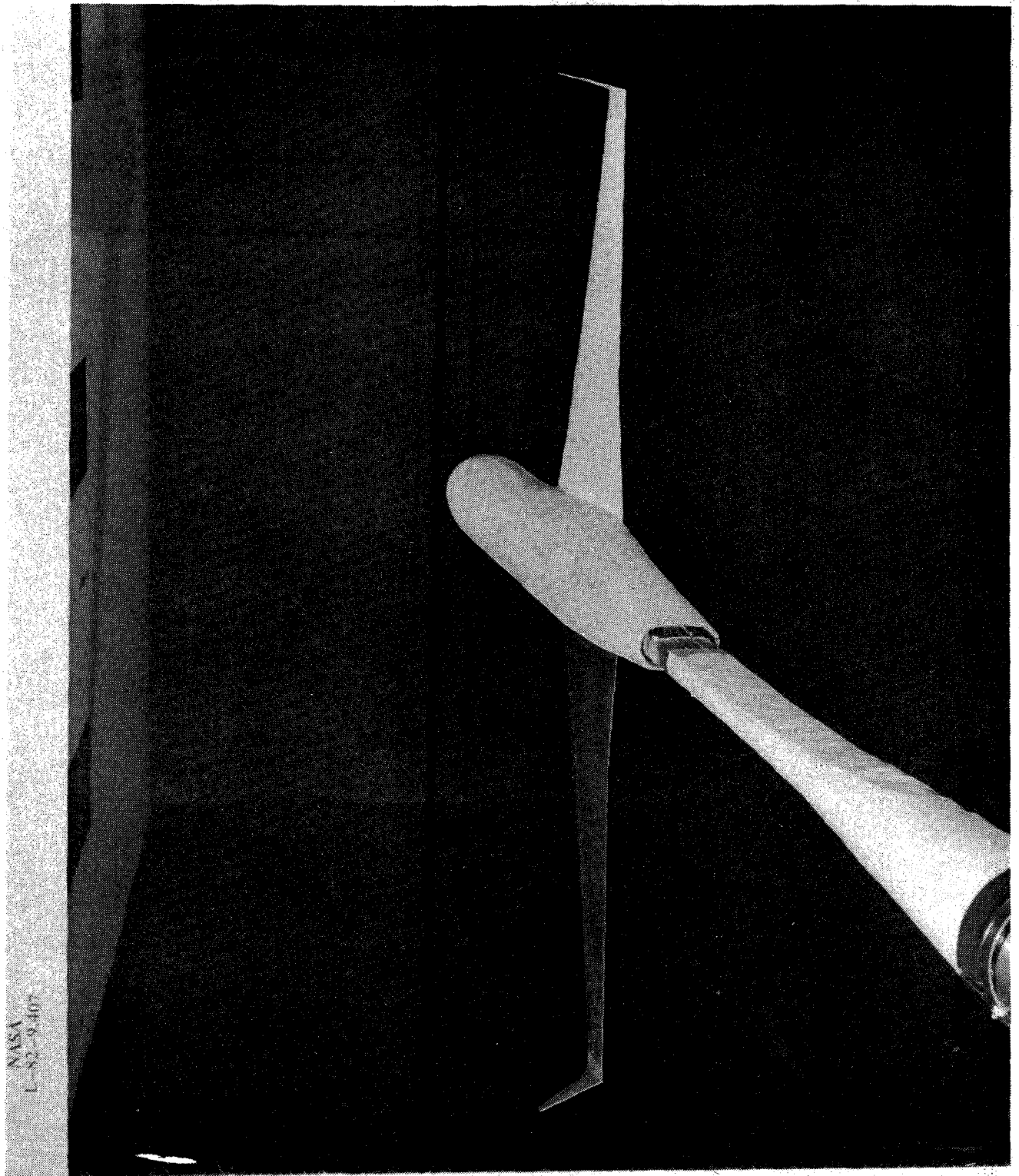


Figure 2. Photographs of the model tested in the NASA/Langley 7 by 10 ft. high speed wind tunnel. (a) Front view. Baseline wing and fuselage.



202 Figure 2(b). Rear view. Wing-winglet configuration.

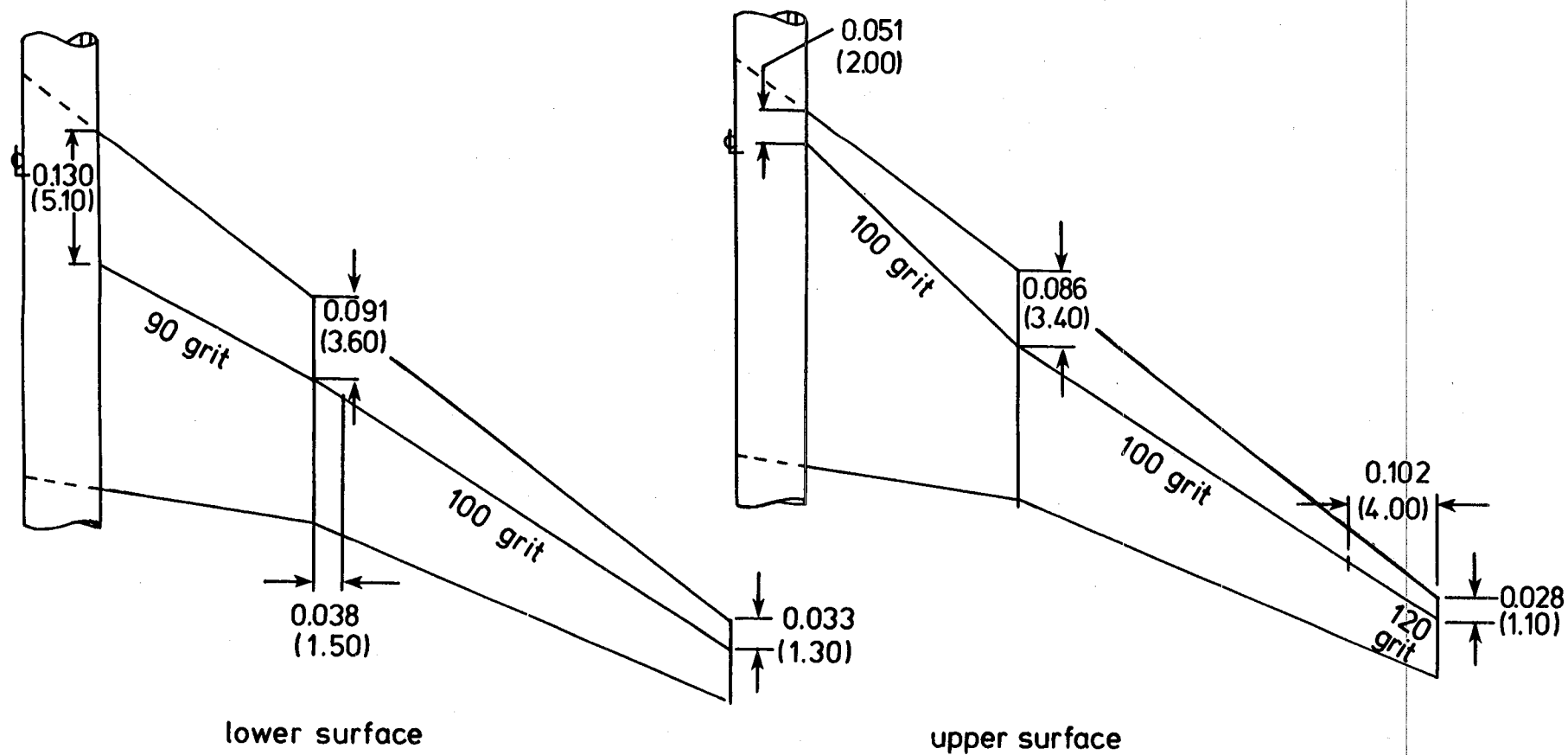


Figure 3. Location and size of transition strips. (a) Wing.

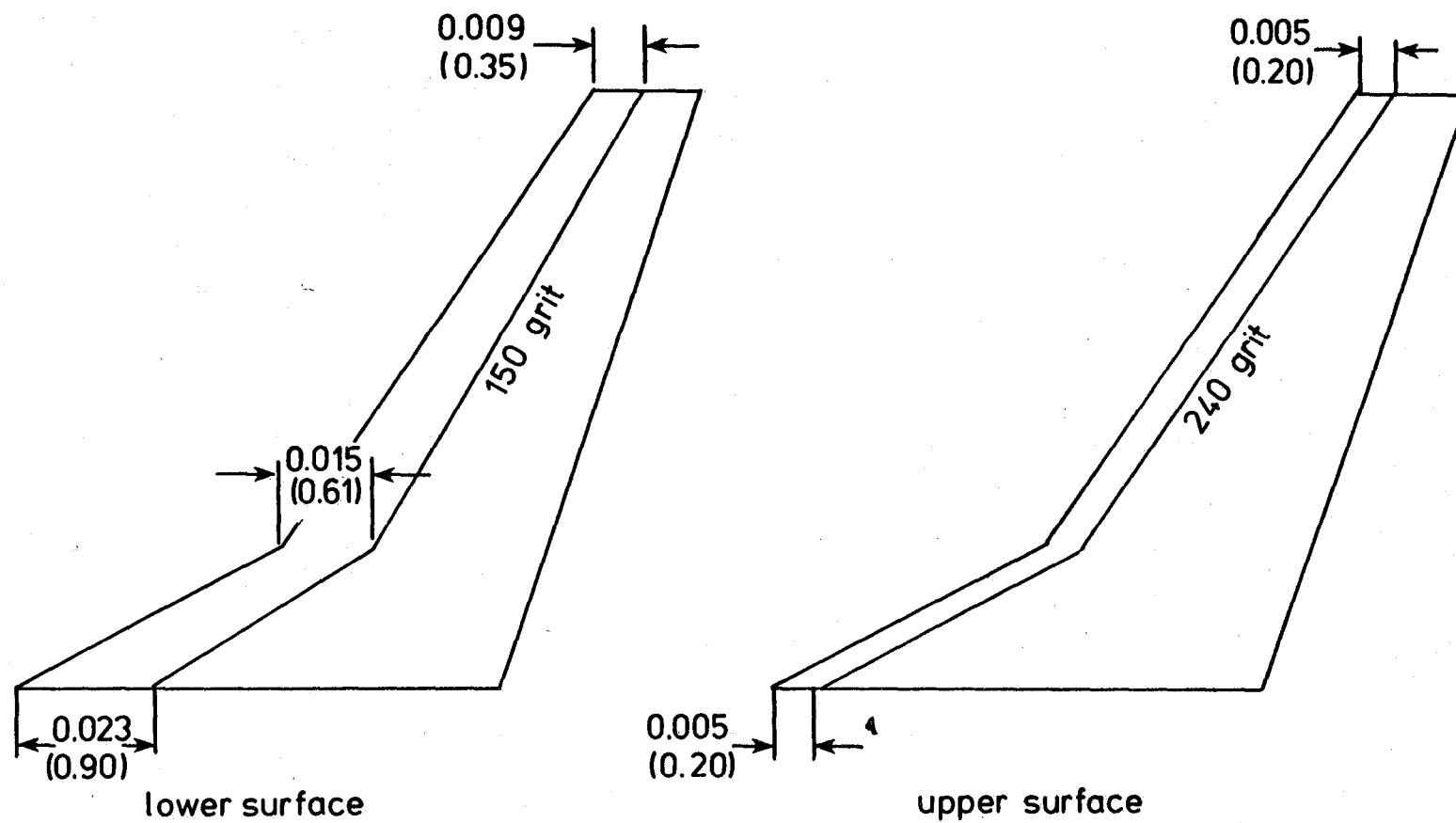


Figure 3 (b). Winglet.

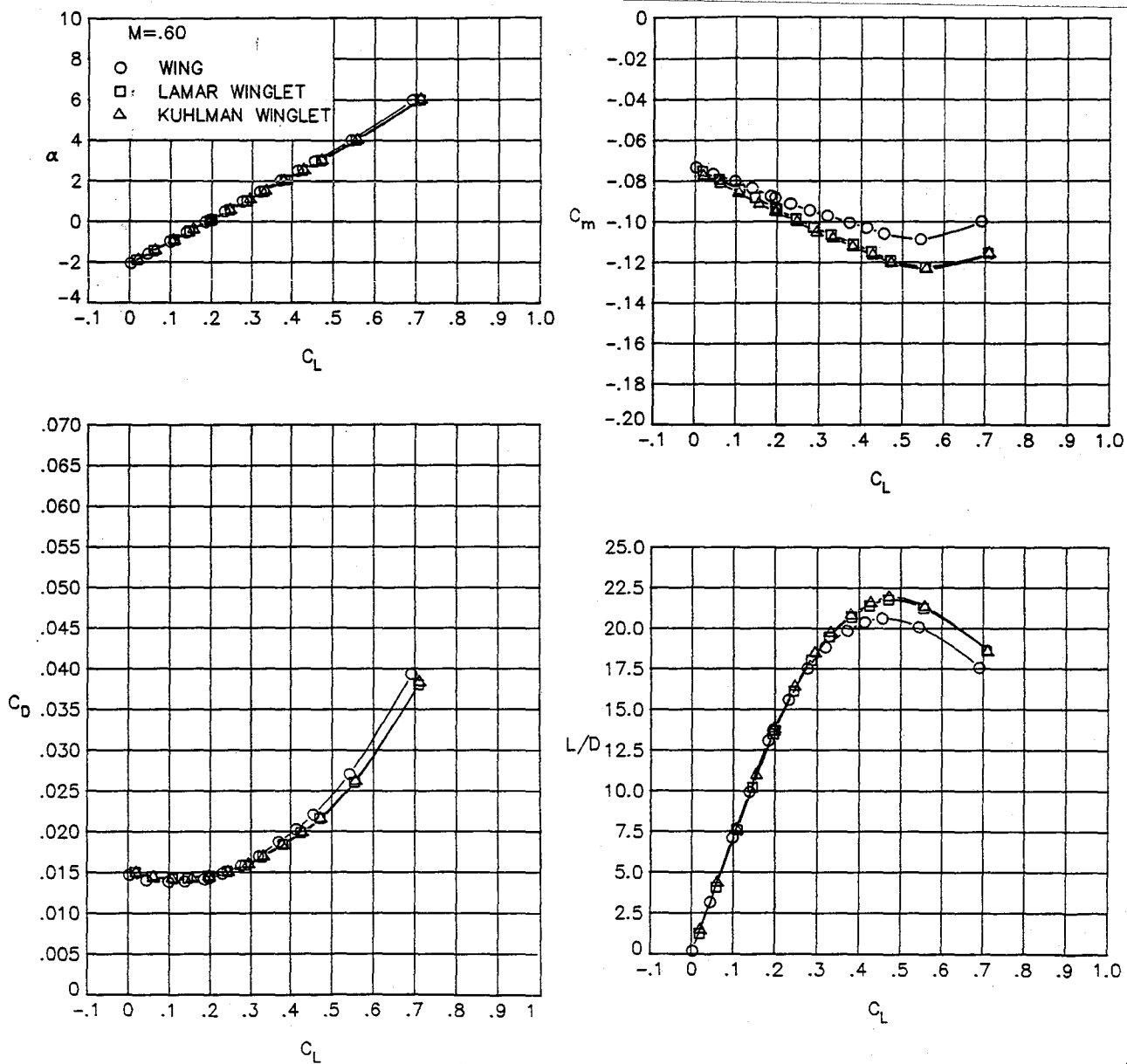


Figure 4. Performance data at $M = 0.60$.

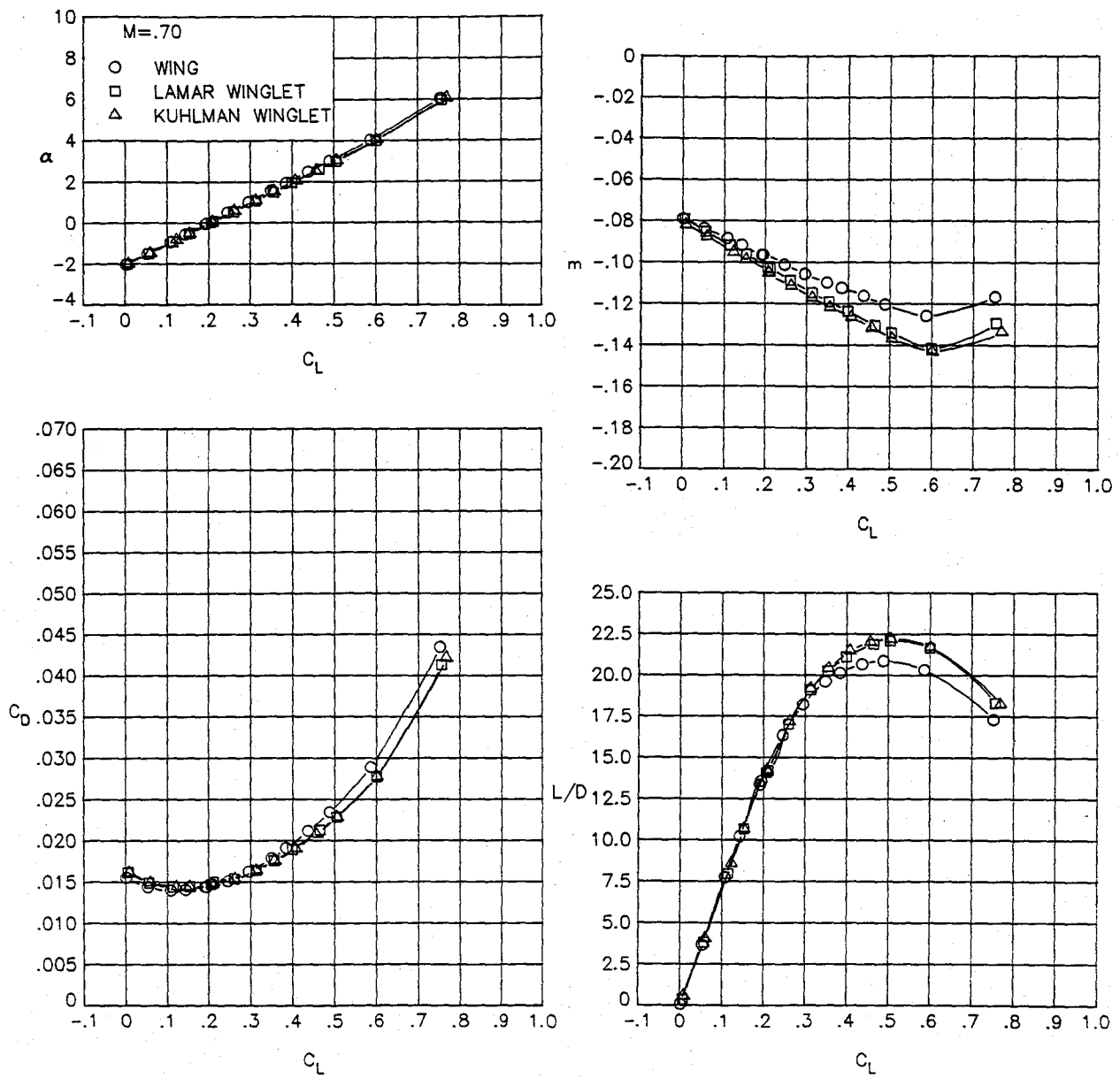


Figure 5. Performance data at $M = 0.70$.

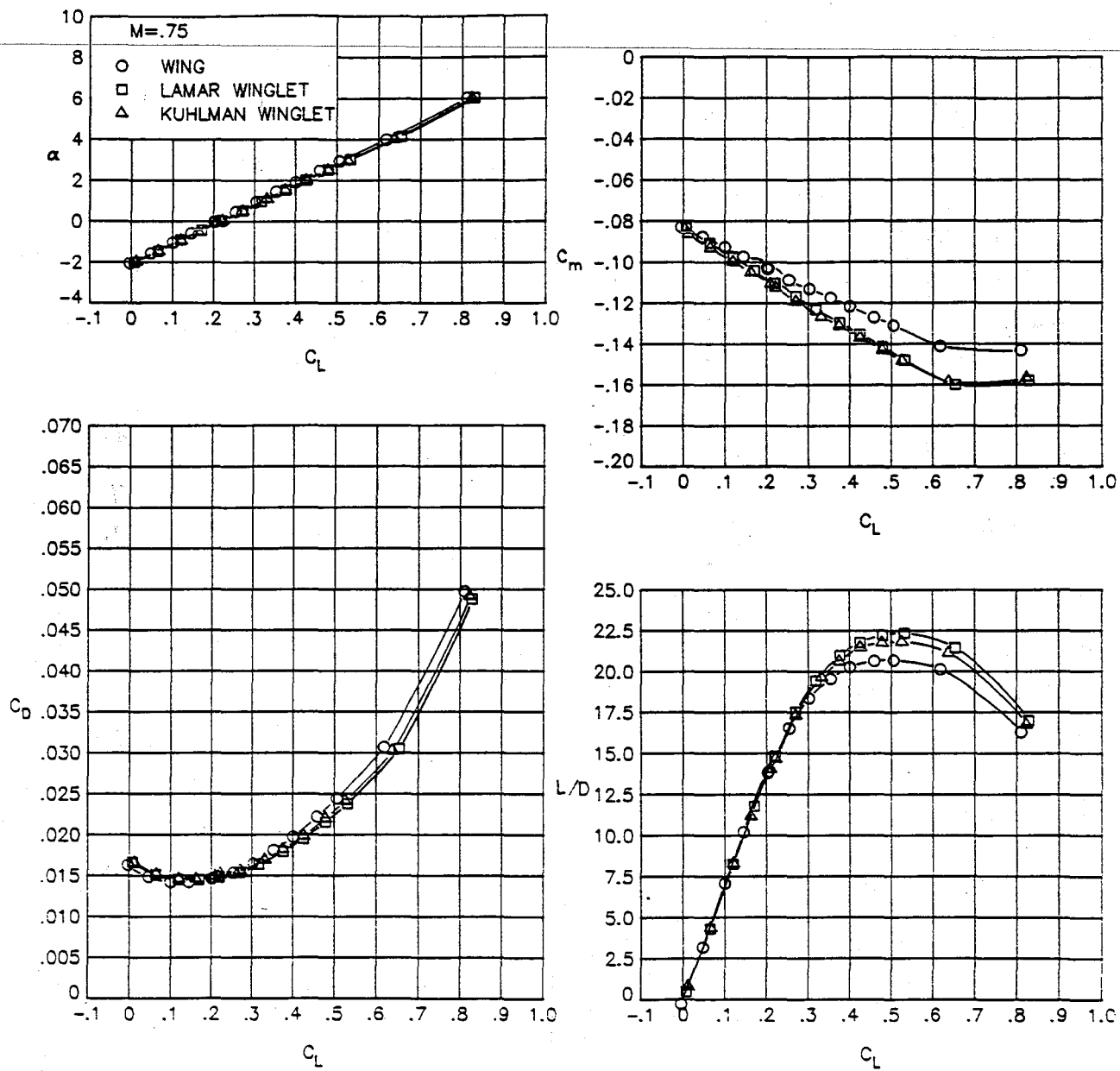


Figure 6. Performance data at $M = 0.75$.

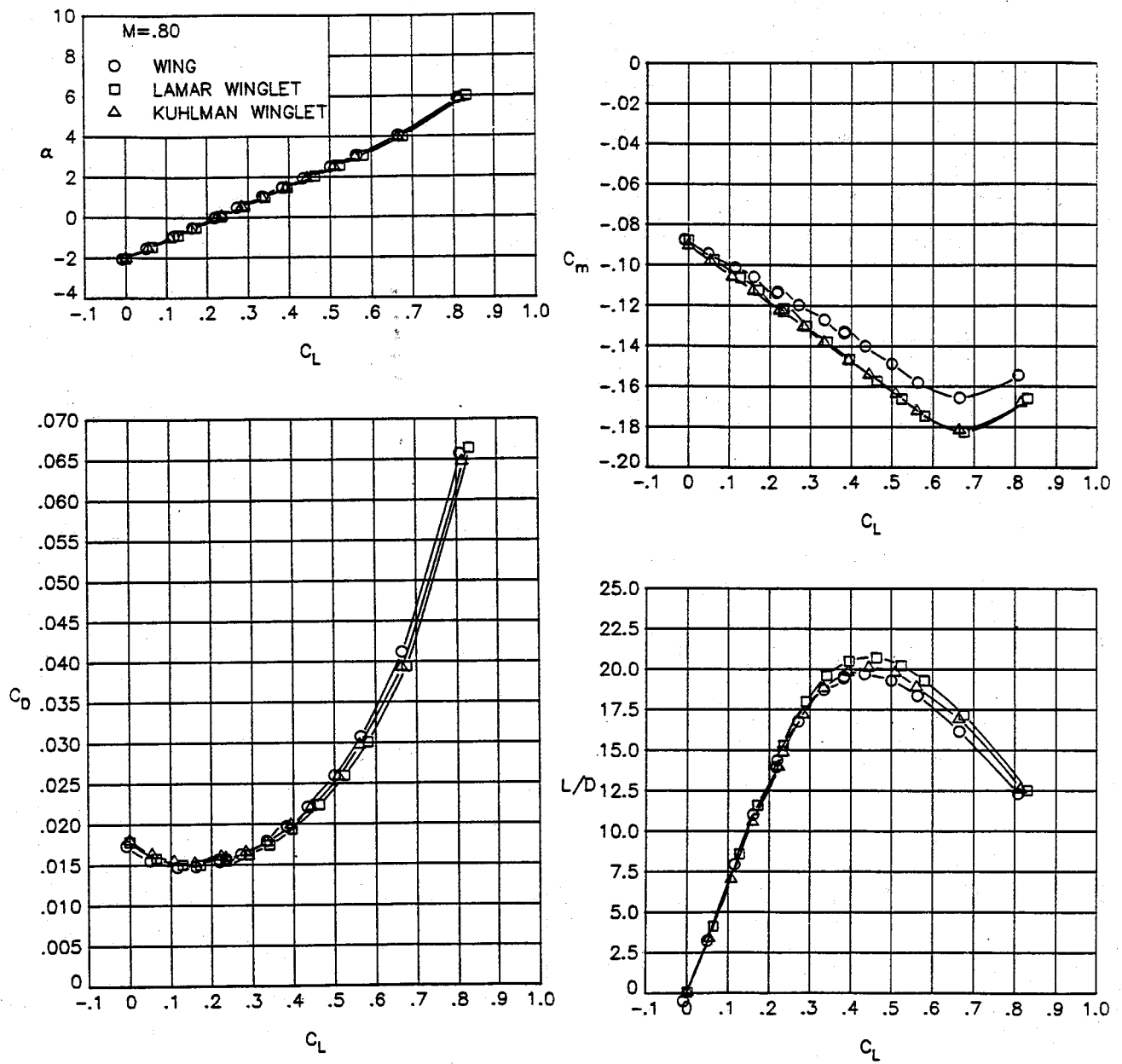


Figure 7. Performance data at $M = 0.80$.

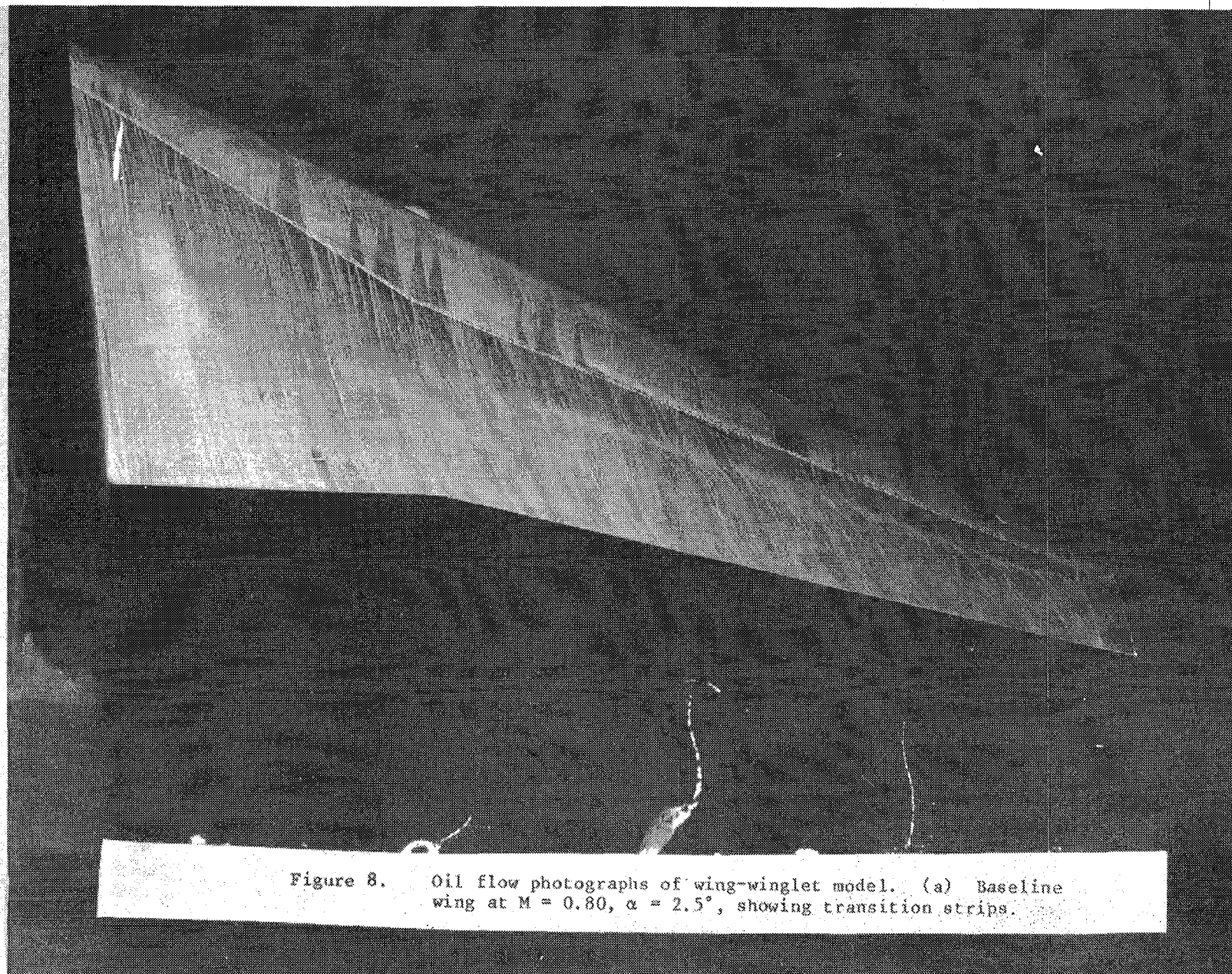
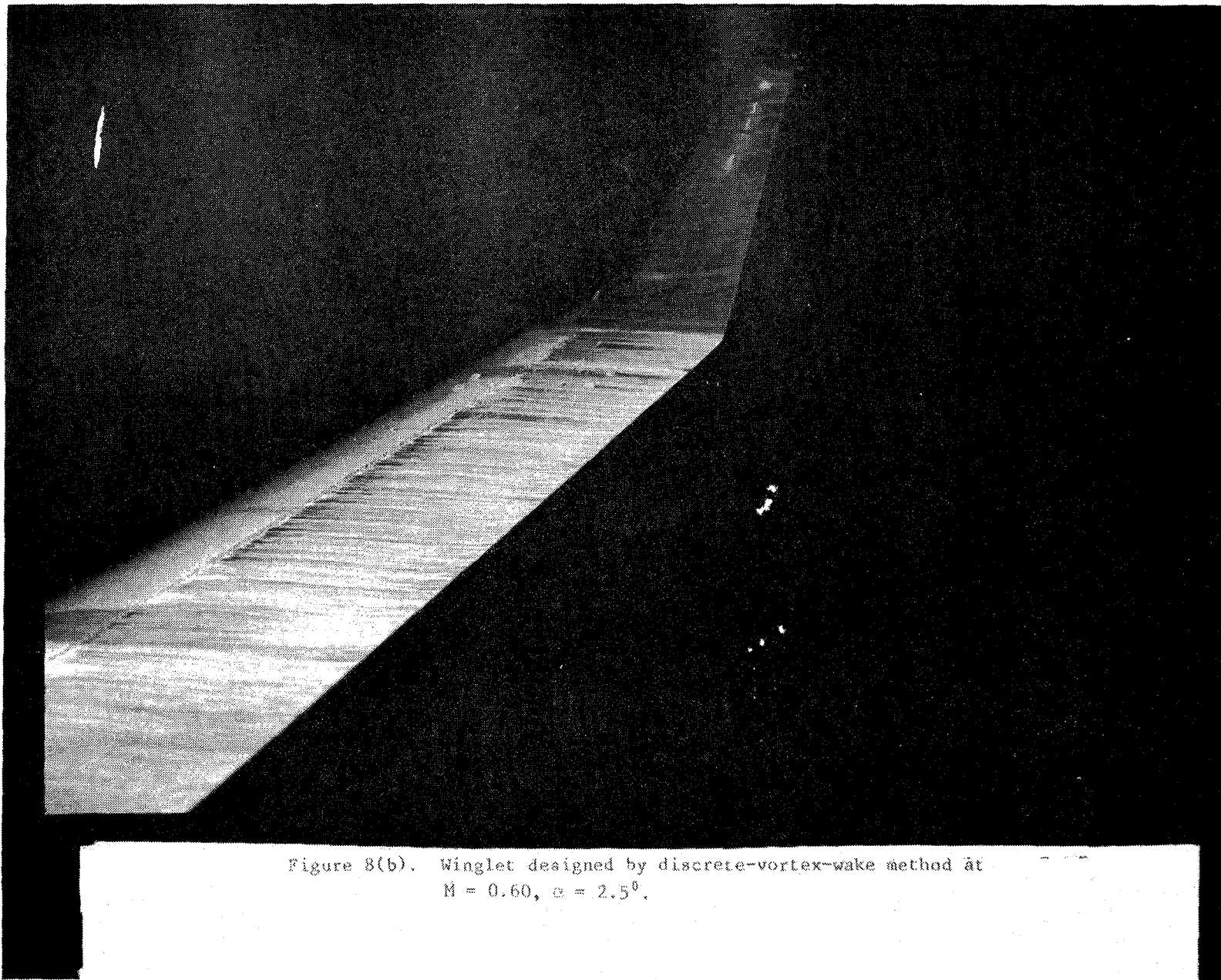


Figure 8. Oil flow photographs of wing-winglet model. (a) Baseline wing at $M = 0.80$, $\alpha = 2.5^\circ$, showing transition strips.



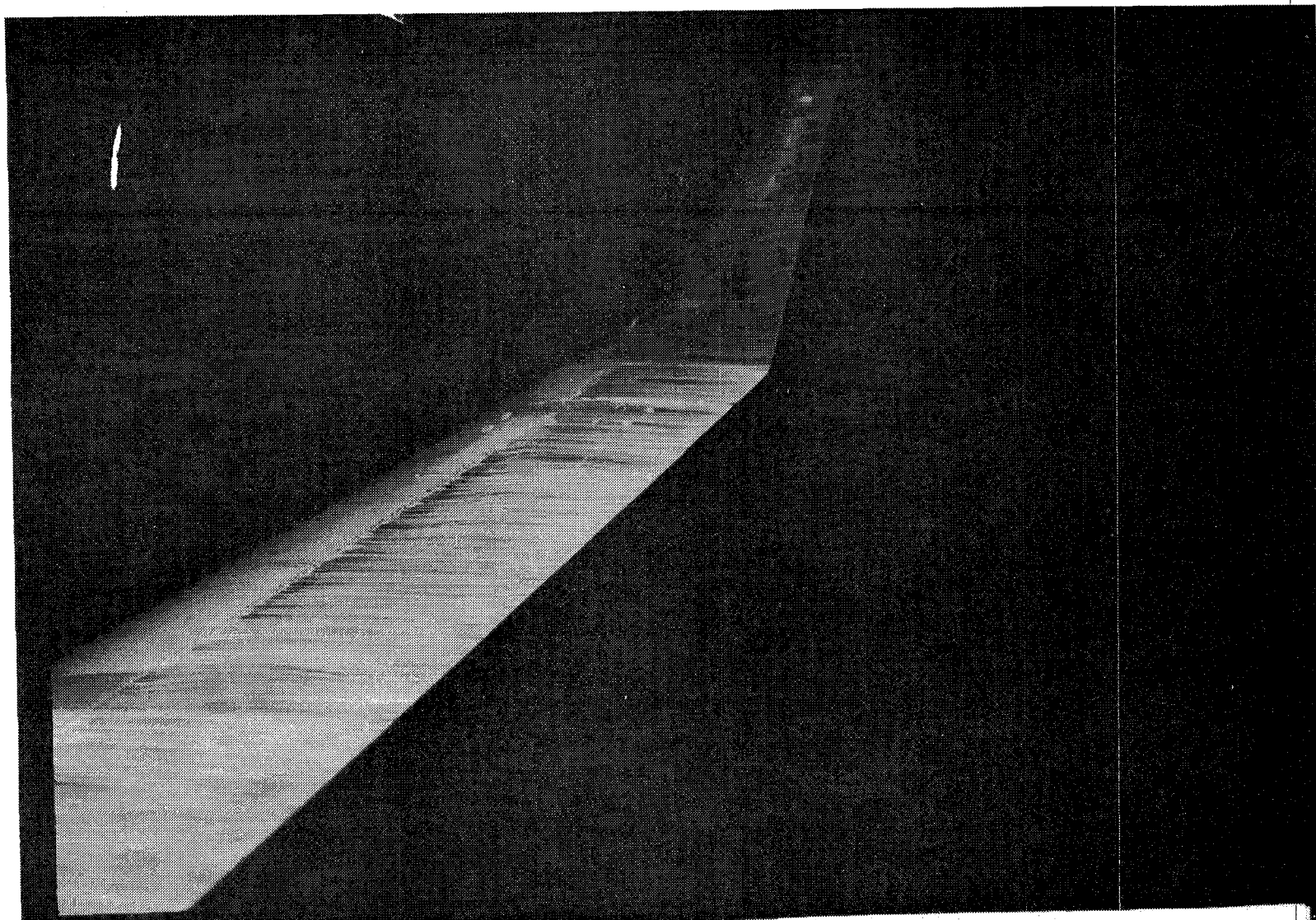


Figure 8(c). Winglet designed by discrete-vortex-wake method at
 $M = 0.60, \alpha = 3^\circ$.

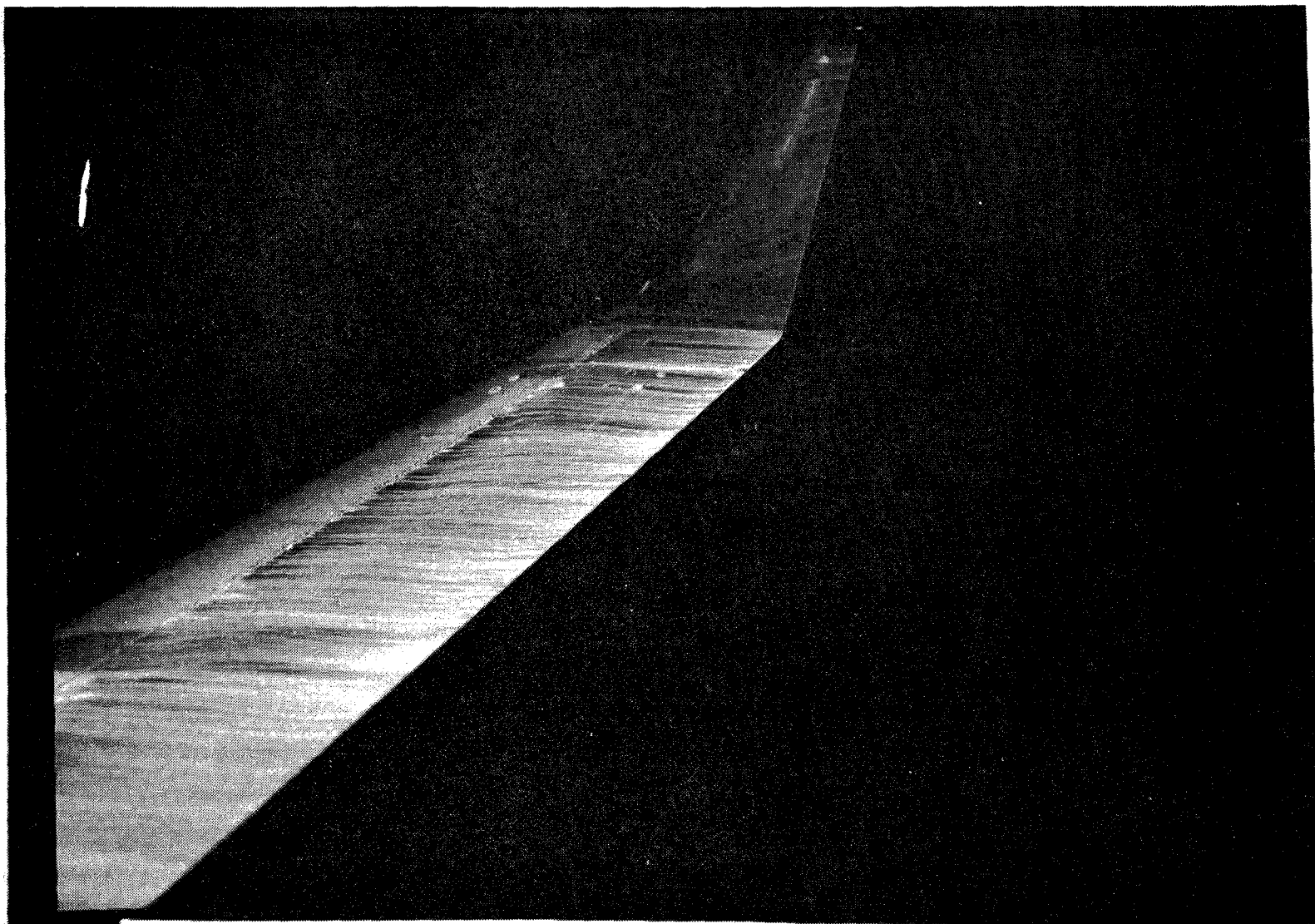


Figure 8(d). Winglet designed by discrete-vortex-wake method at
 $M = 0.60$, $\alpha = 3.5^\circ$.

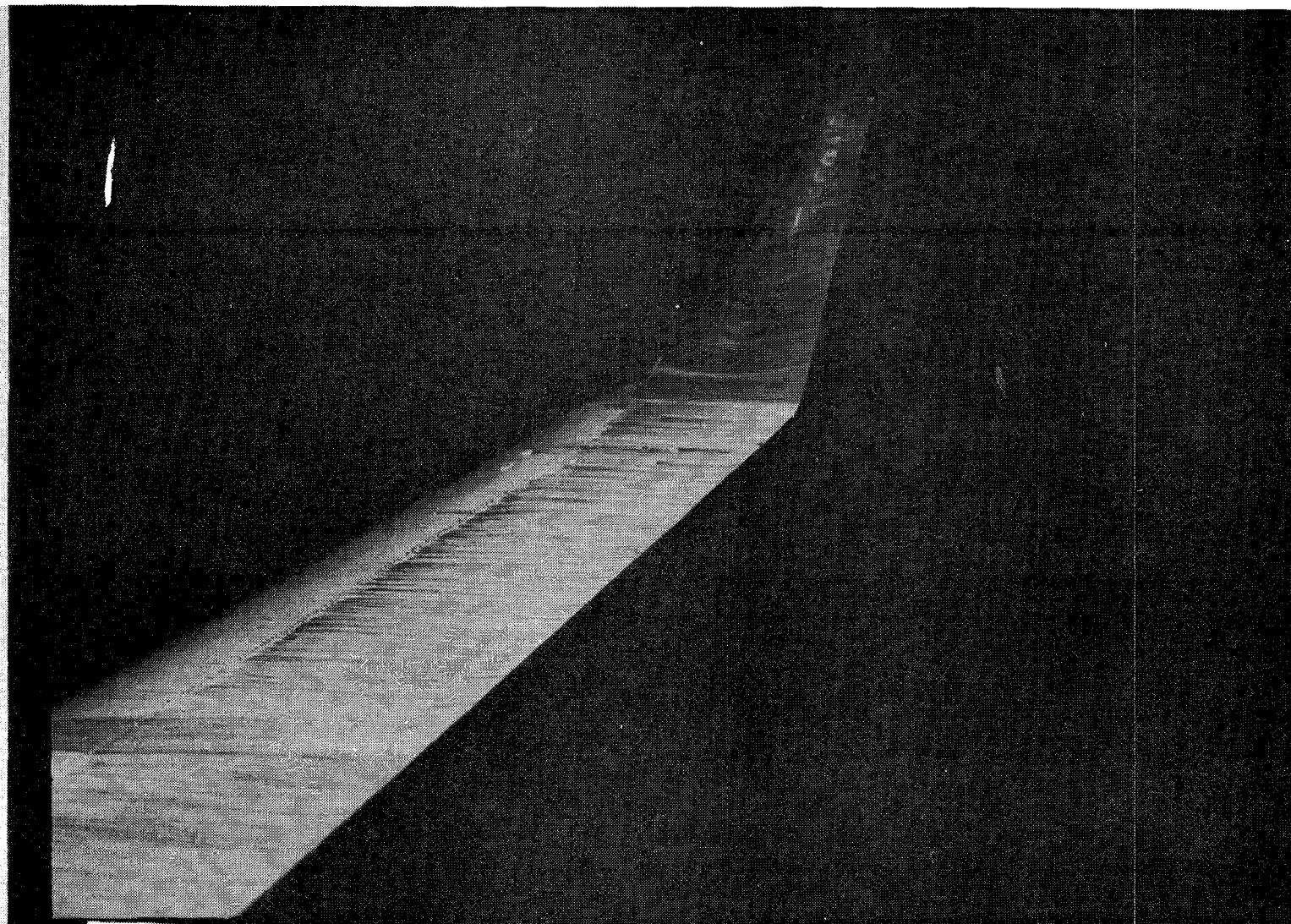


Figure 8(e). Winglet designed by discrete-vortex-wake method at
 $M = 0.70$, $\alpha = 2^\circ$.

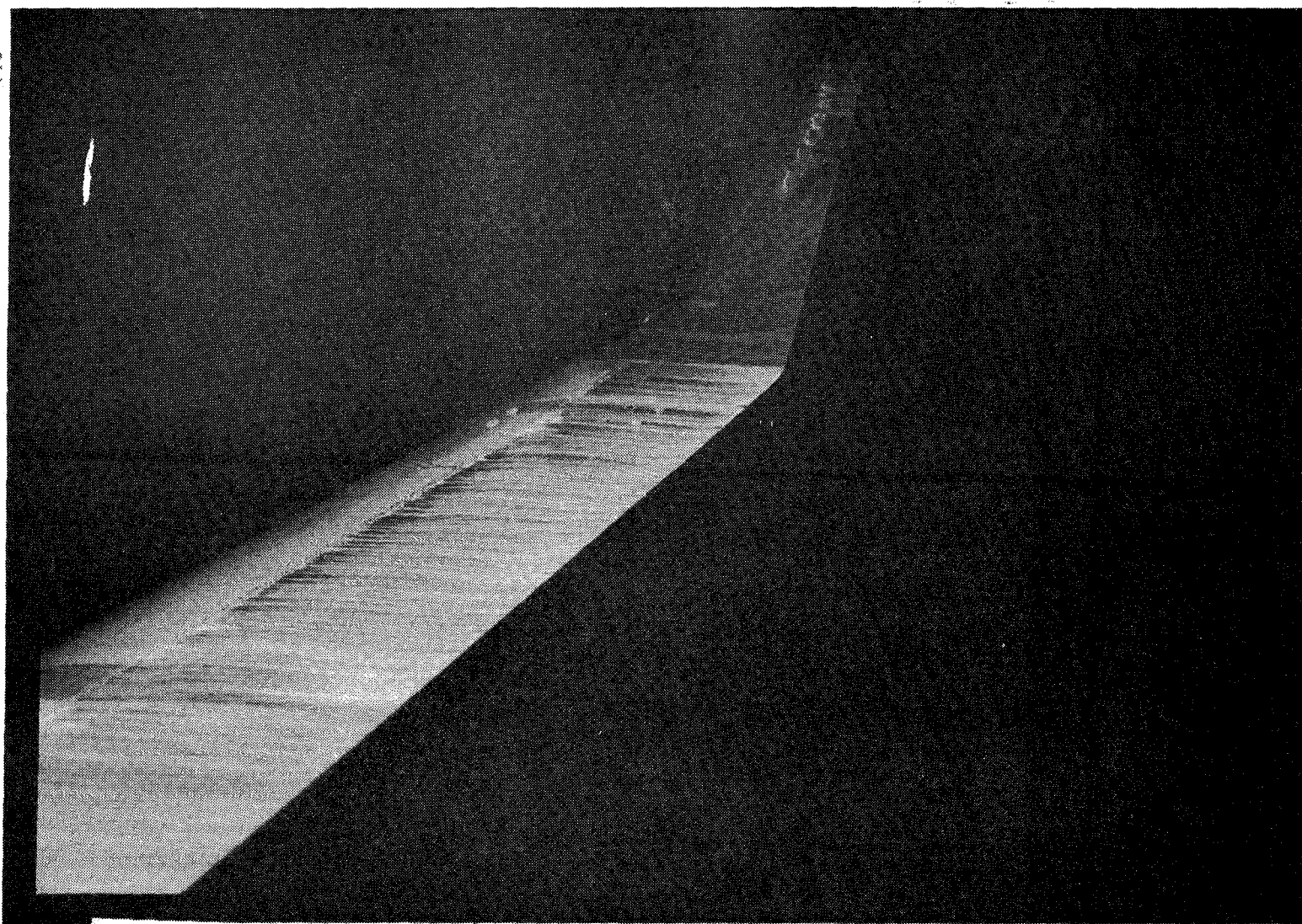


Figure 8(f). Winglet designed by discrete-vortex-wake method at
 $M = 0.70$, $\alpha = 2.5^\circ$.

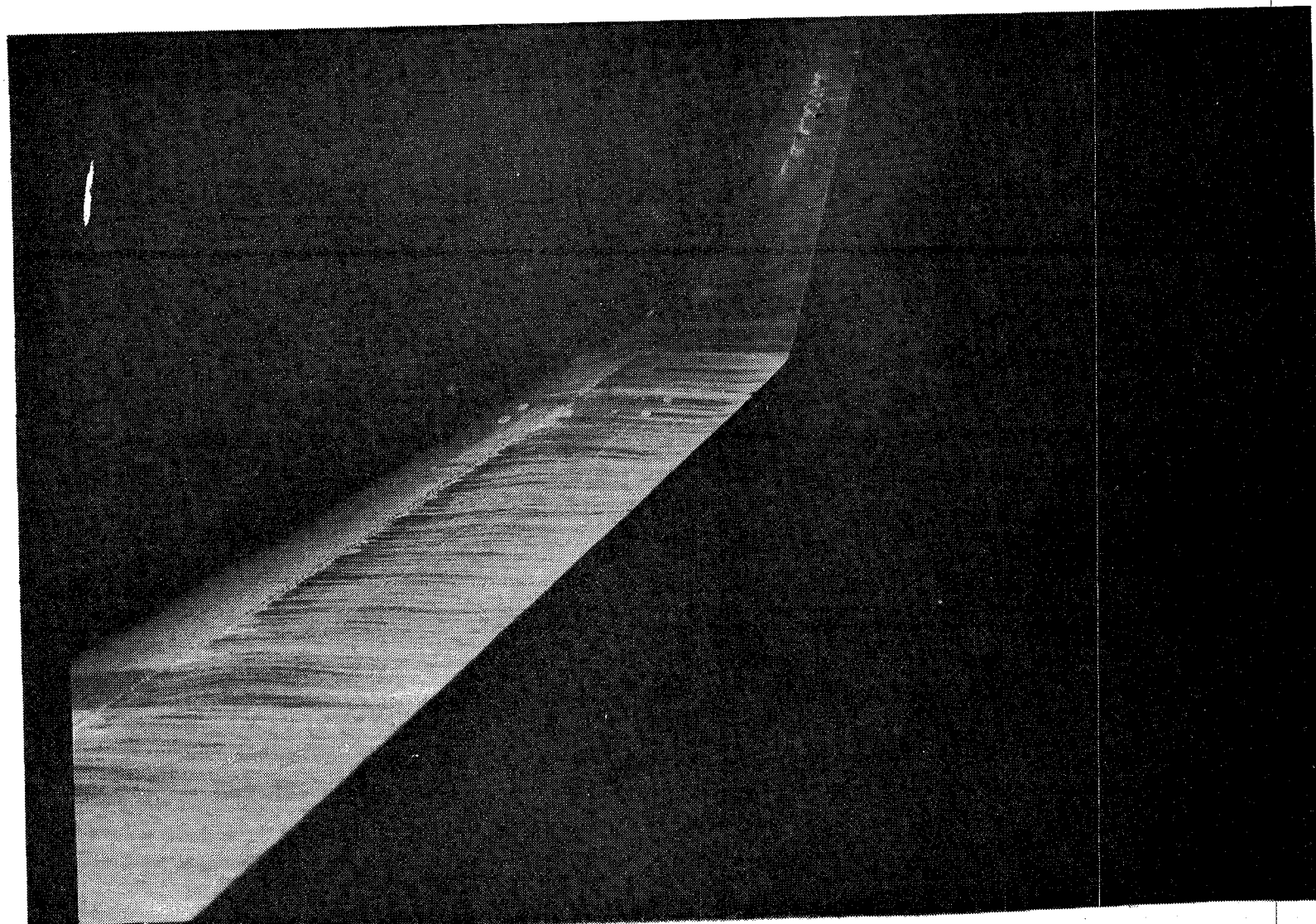


Figure 8(g). Winglet designed by discrete-vortex-wake method at
 $M = 0.70$, $\alpha = 3^\circ$.

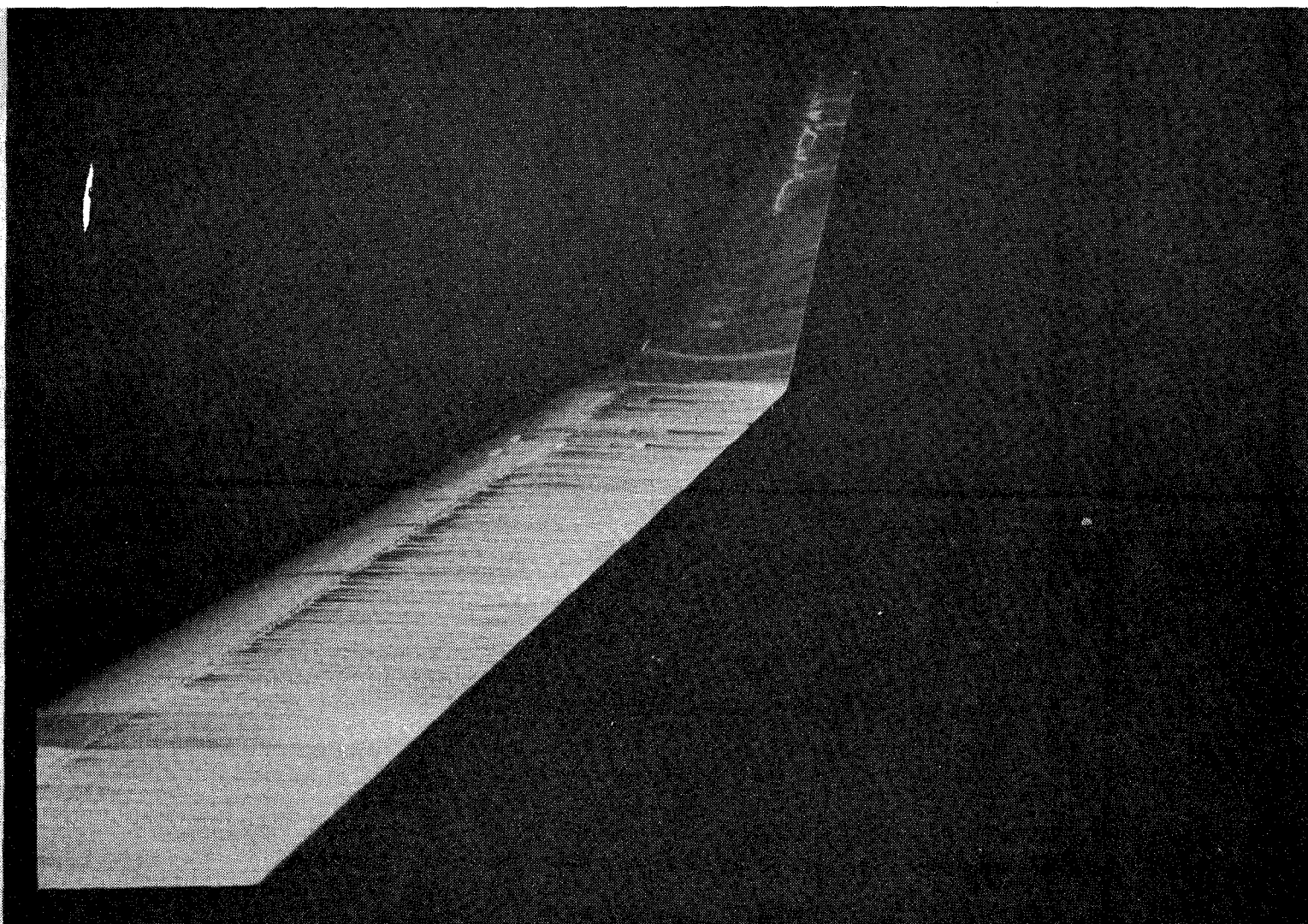


Figure 8(h). Winglet designed by discrete-vortex-wake method at
 $M = 0.75$, $\alpha = 1.5^\circ$.

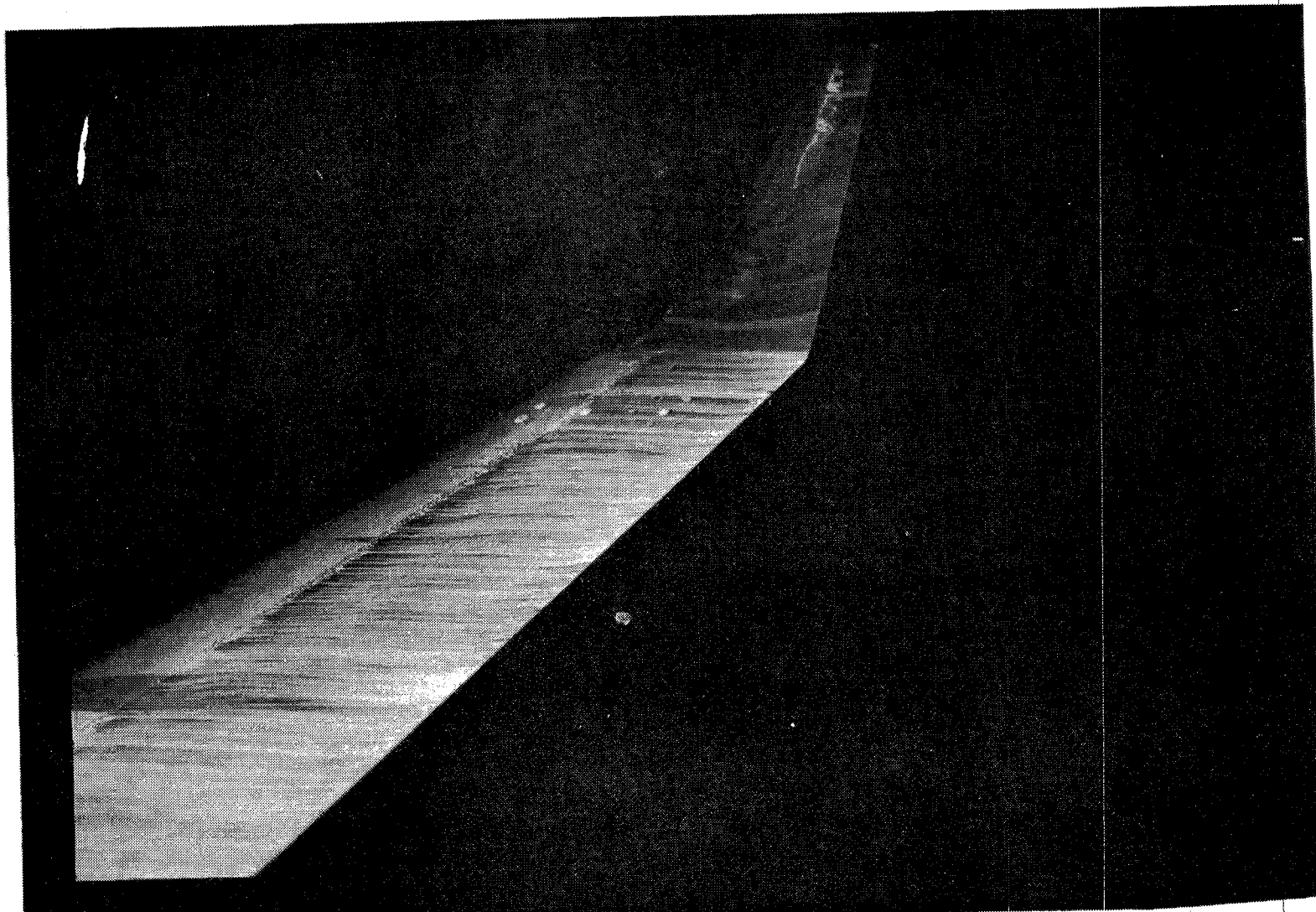


Figure 8(i). Winglet designed by discrete-vortex-wake method at
 $M = 0.75$, $\alpha = 2^\circ$.

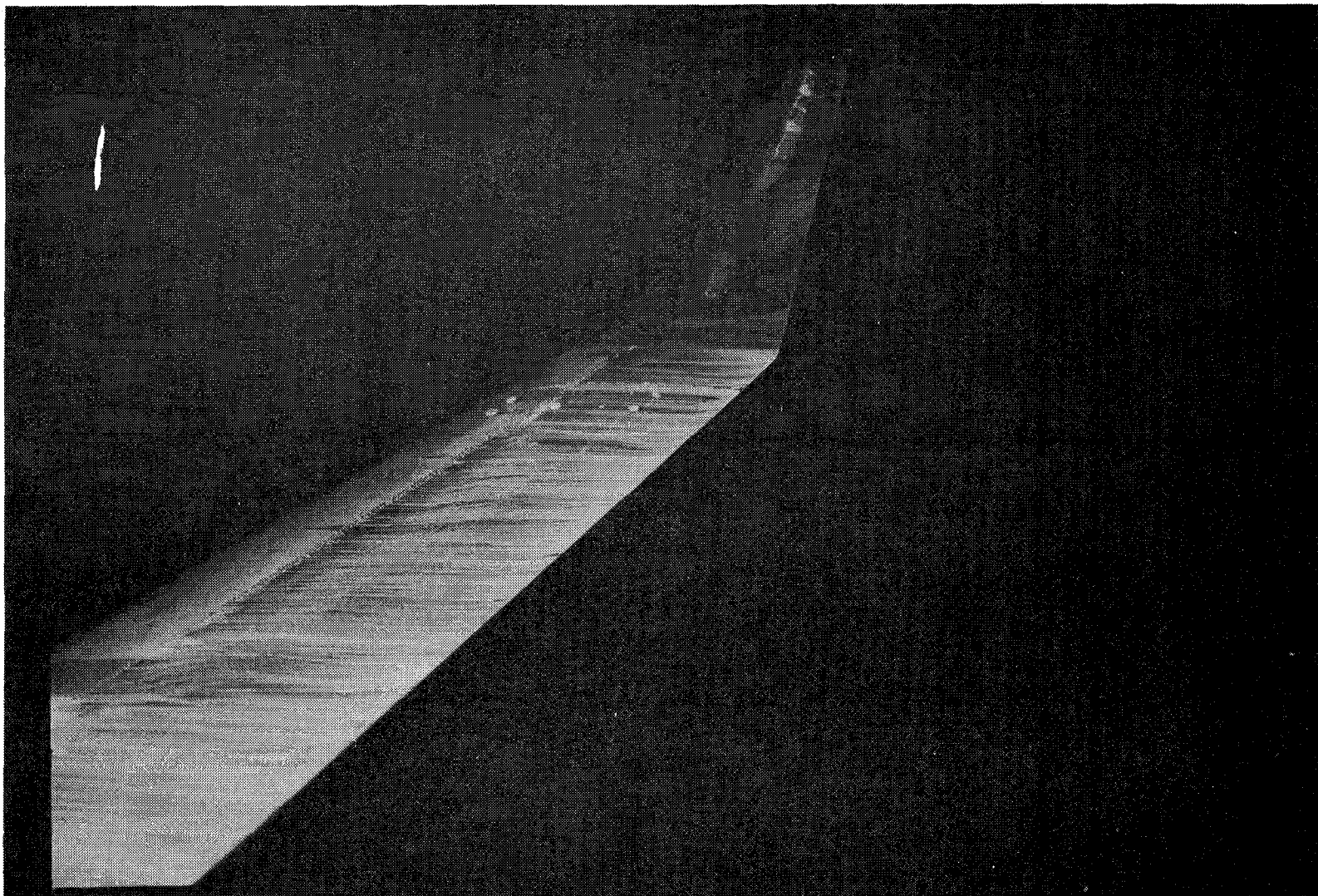


Figure 8(j): Winglet designed by discrete-vortex-wake method at
 $M = 0.75$, $\alpha = 2.5^\circ$.

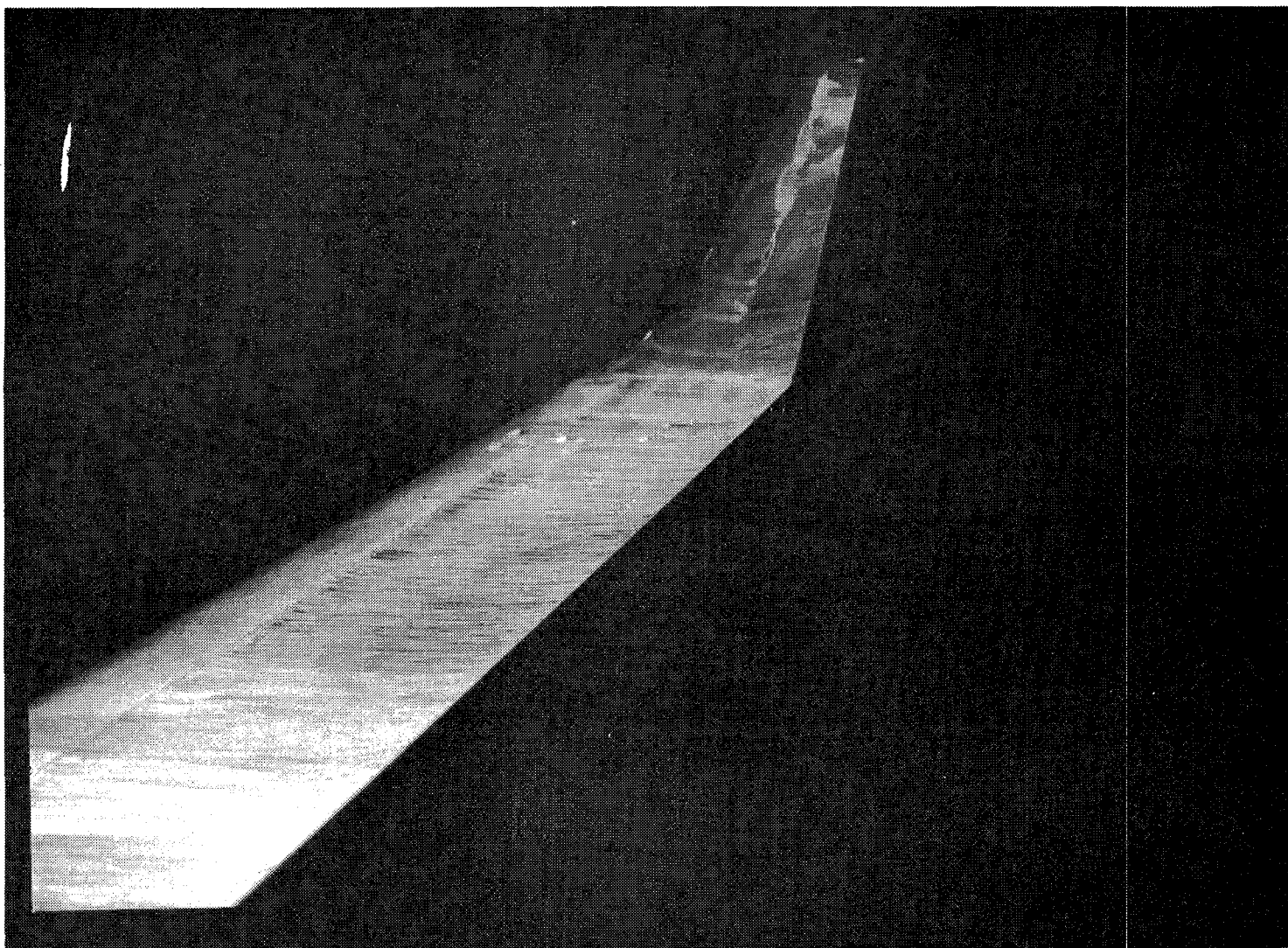


Figure 8(k). Winglet designed by discrete-vortex-wake method at $M = 0.80$, $\alpha = 1.5^\circ$.



Figure 8(1). Winglet designed by discrete-vortex-wake method at
 $M = 0.80$, $\alpha = 2^\circ$.

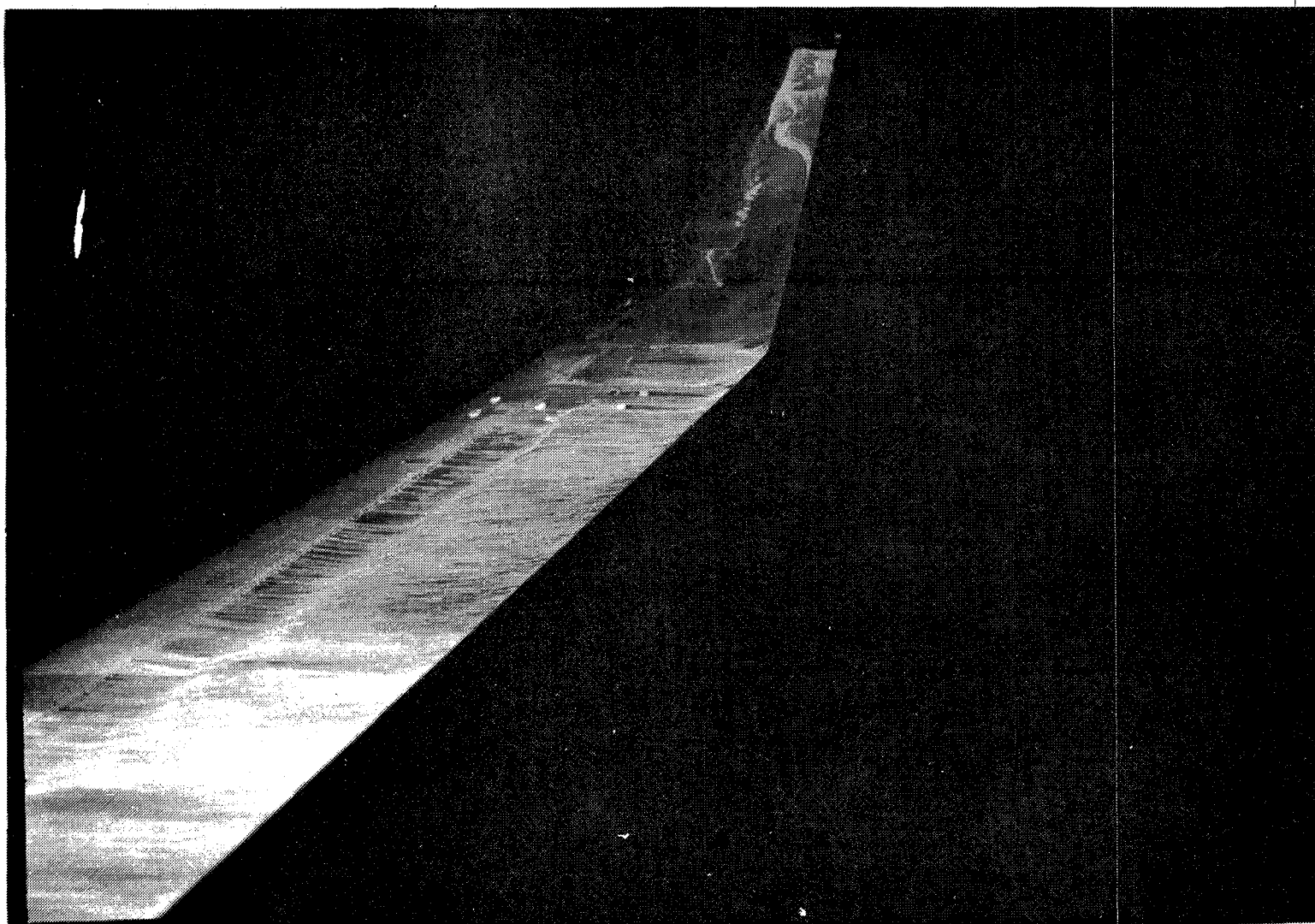


Figure 3(m). Winglet designed by discrete-vortex-wake method at
 $M = 0.80$, $\alpha = 2.5^\circ$.

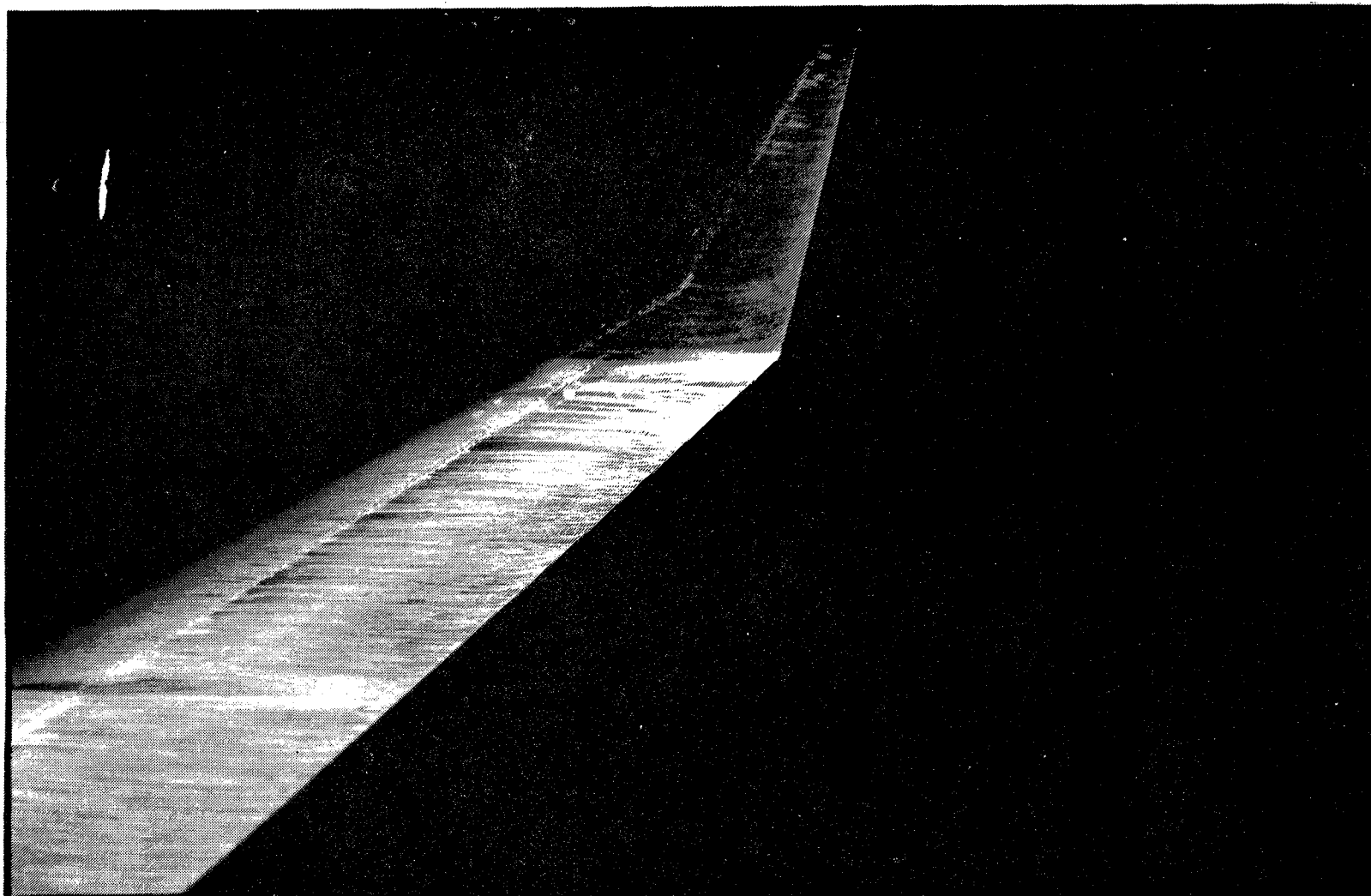


Figure 8(n). Winglet designed by Ribbert order-potential-like method
at $M = 0.60$, $\alpha = 2.5^\circ$.

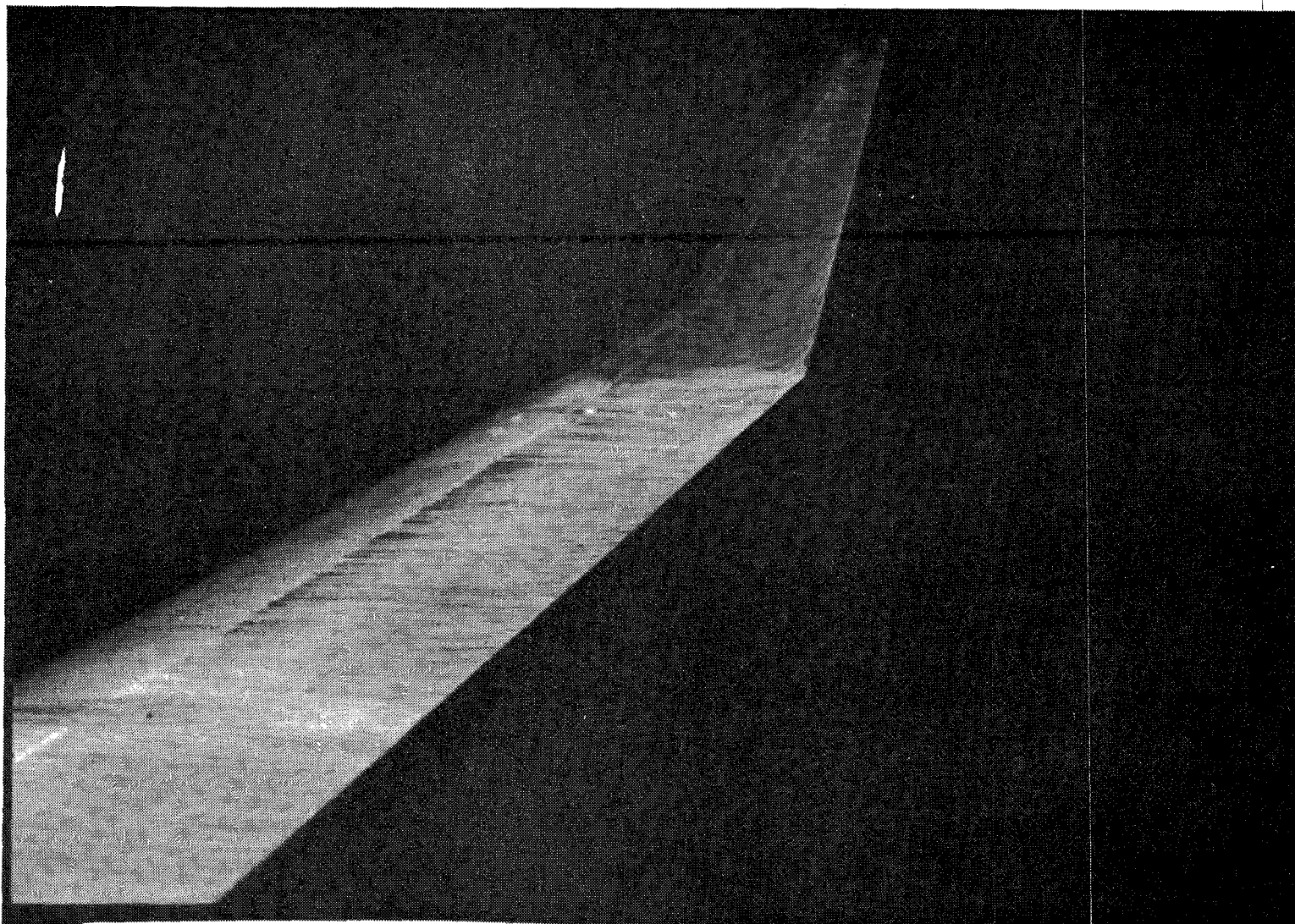


Figure 8(o). Winglet designed by higher-order-panel-wake method
at $M = 0.70$, $\alpha = 2^\circ$.

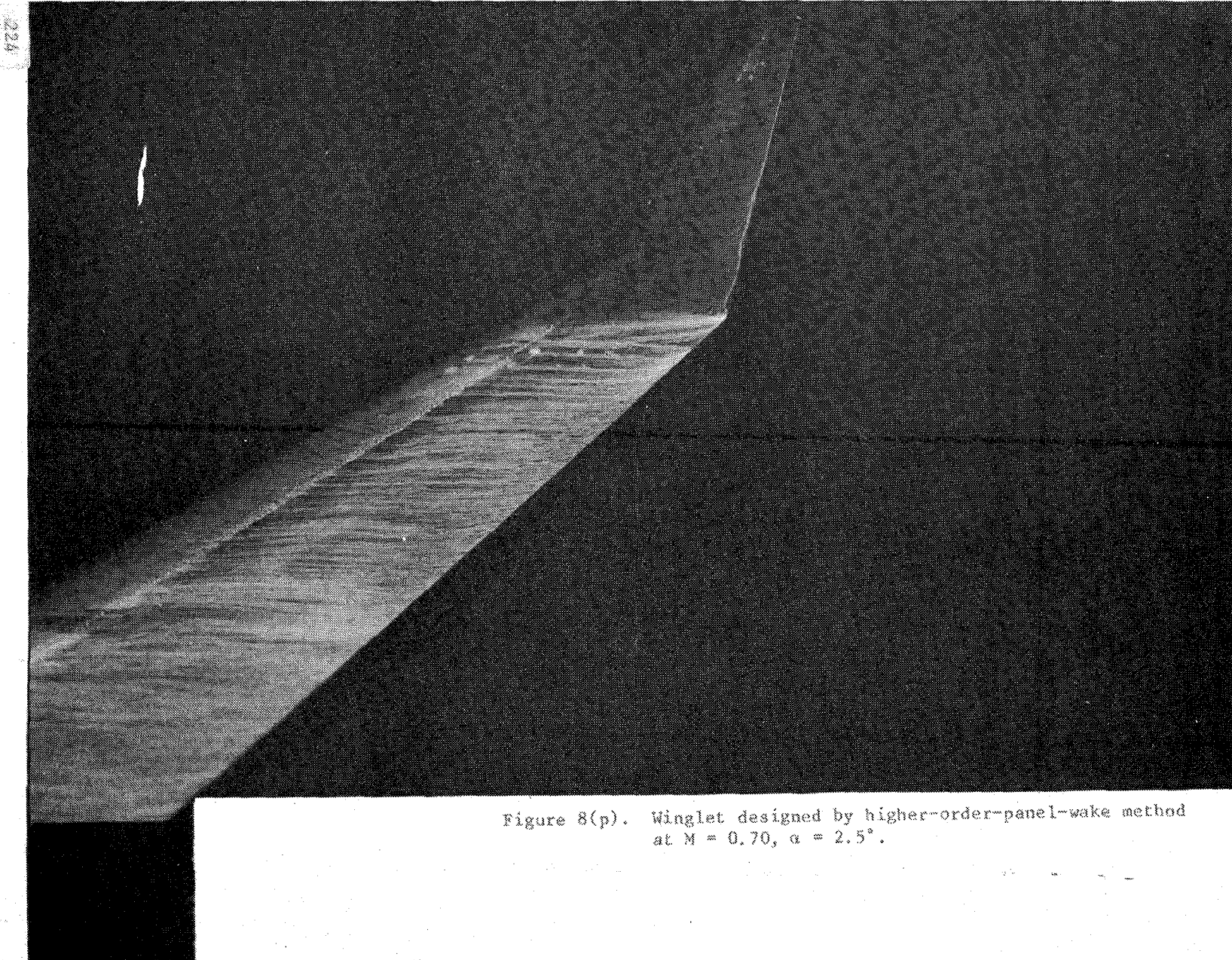


Figure 8(p). Winglet designed by higher-order-panel-wake method
at $M = 0.70$, $\alpha = 2.5^\circ$.

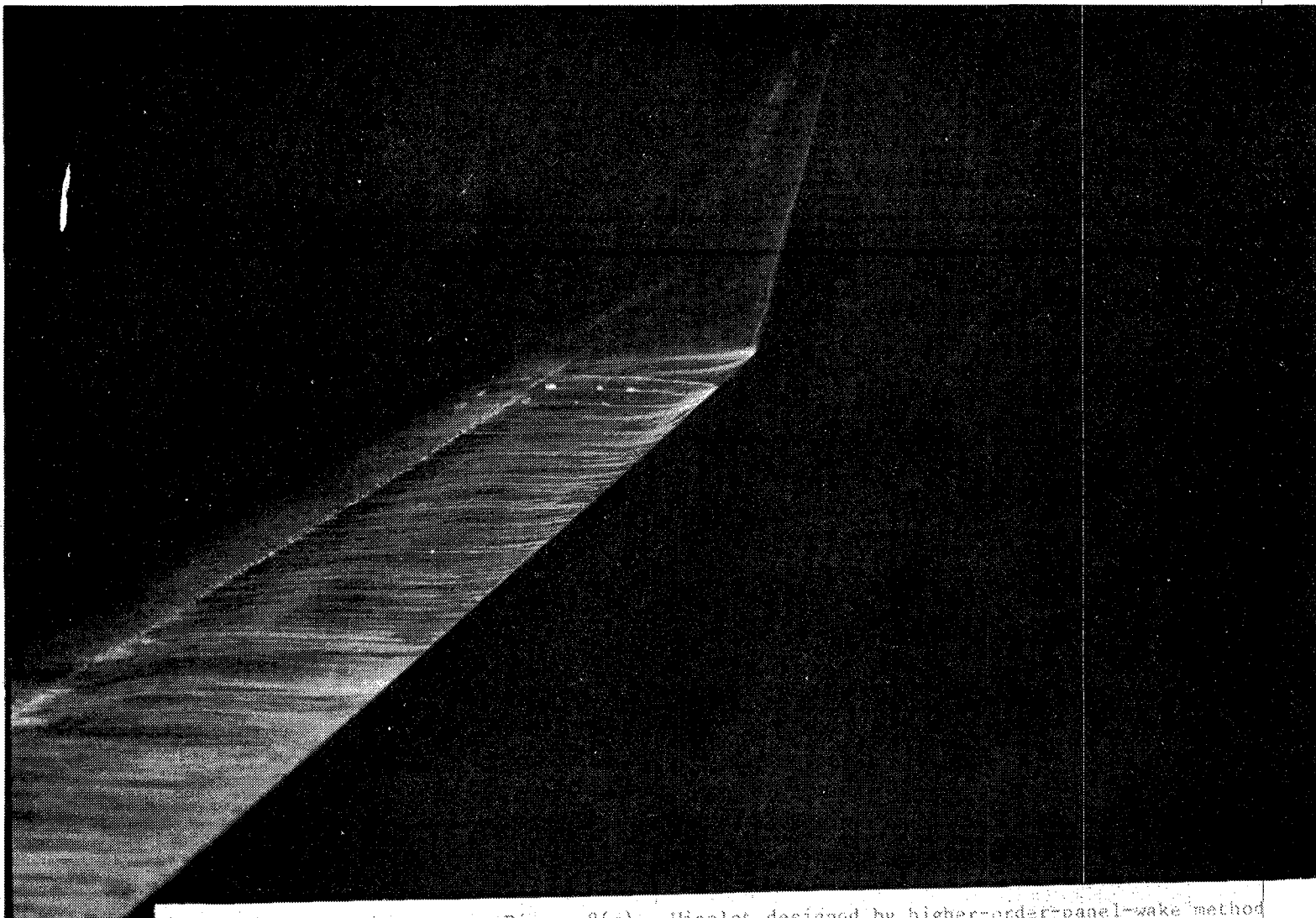


Figure 8(q). Winglet designed by higher-order-panel-wake method
at $M = 0.70$, $\alpha = 3^\circ$.

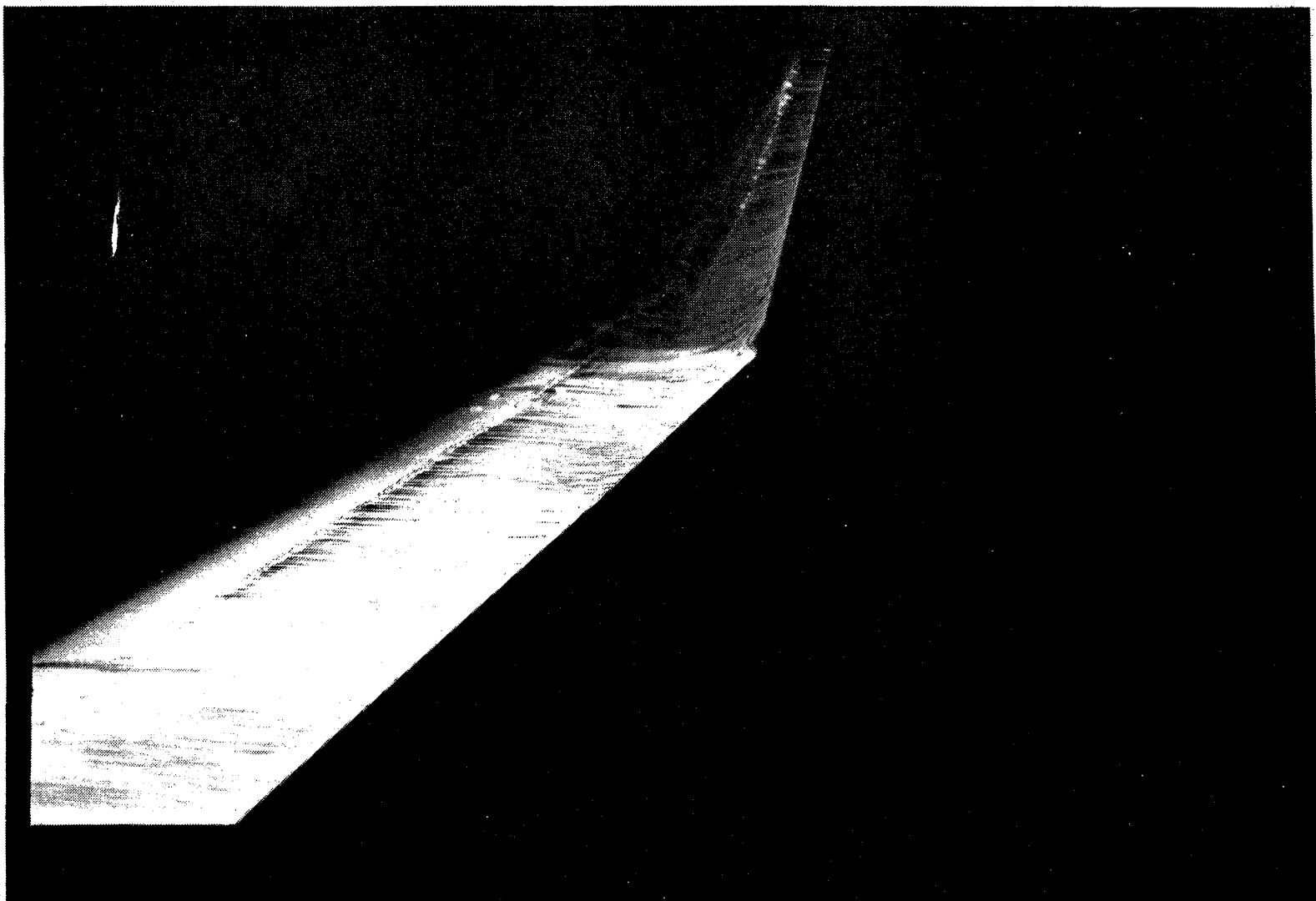


Figure 3(r). Winglet designed by higher-order-panel-wake method
at $M = 0.75$, $\alpha = 1.5^\circ$.

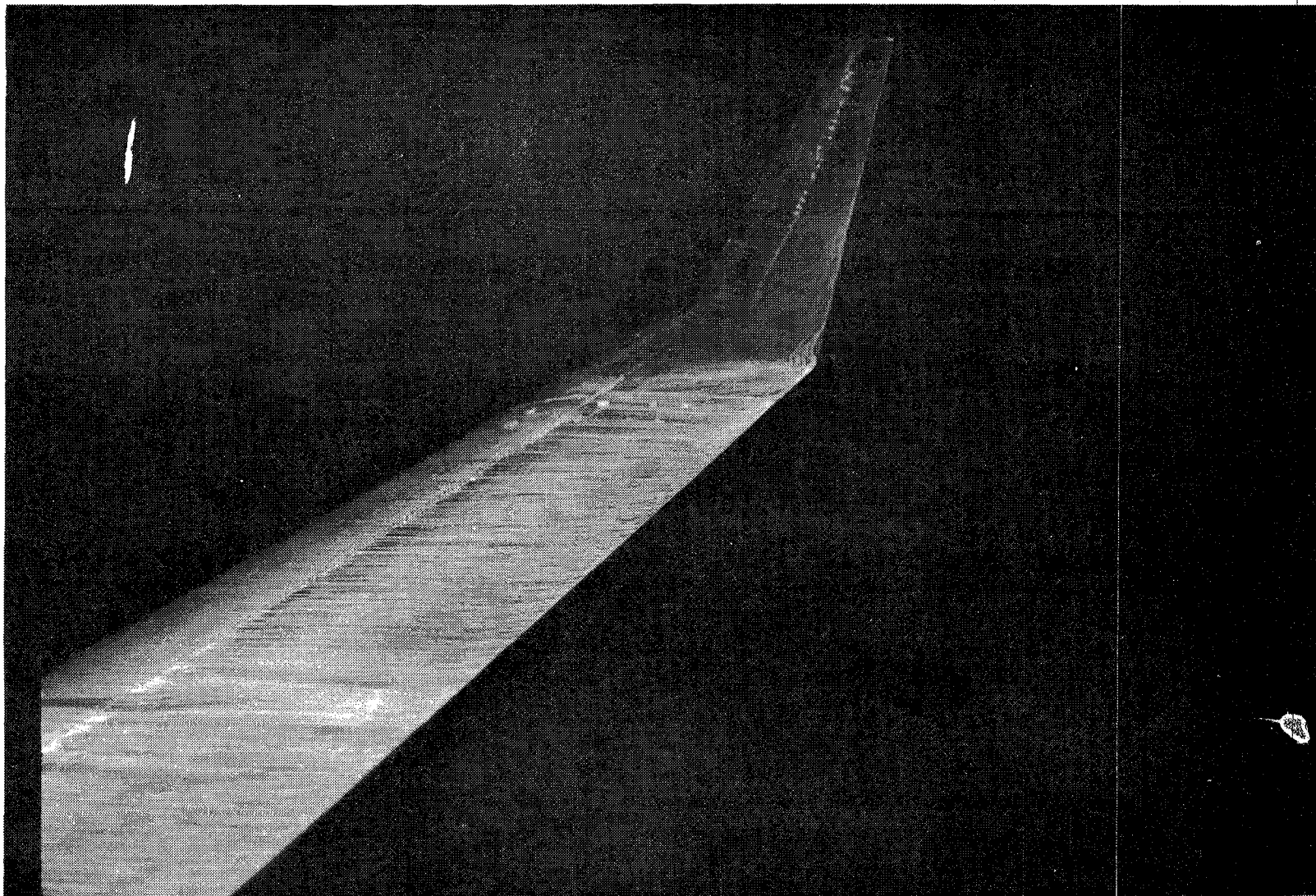


Figure 8(s). Winglet designed by higher-order-panel-wake method
at $M = 0.75$, $\alpha = 2^\circ$.

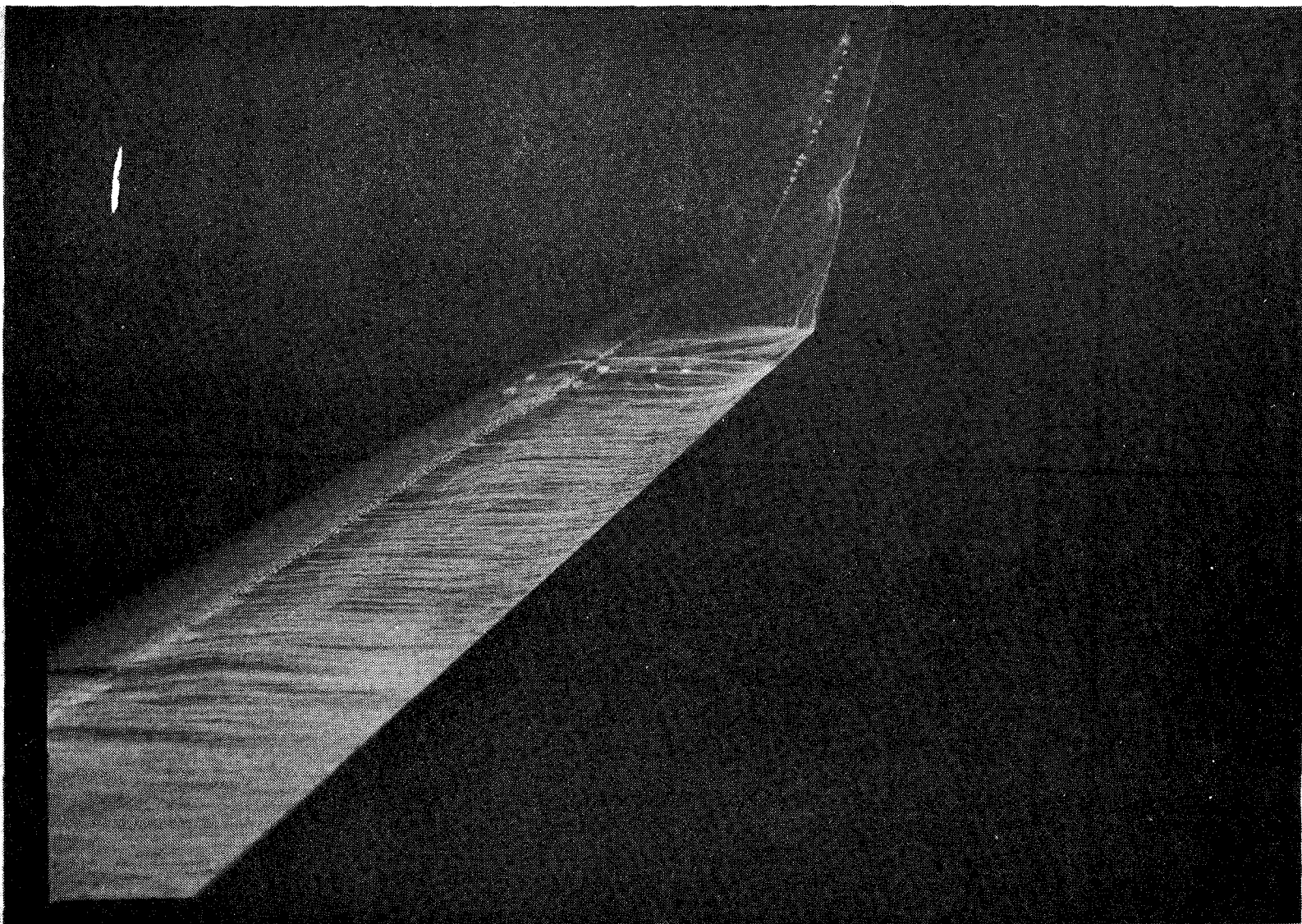


Figure 8(t). Winglet designed by higher-order-panel-wake method
at $M = 0.75$, $\alpha \approx 2.5^\circ$.

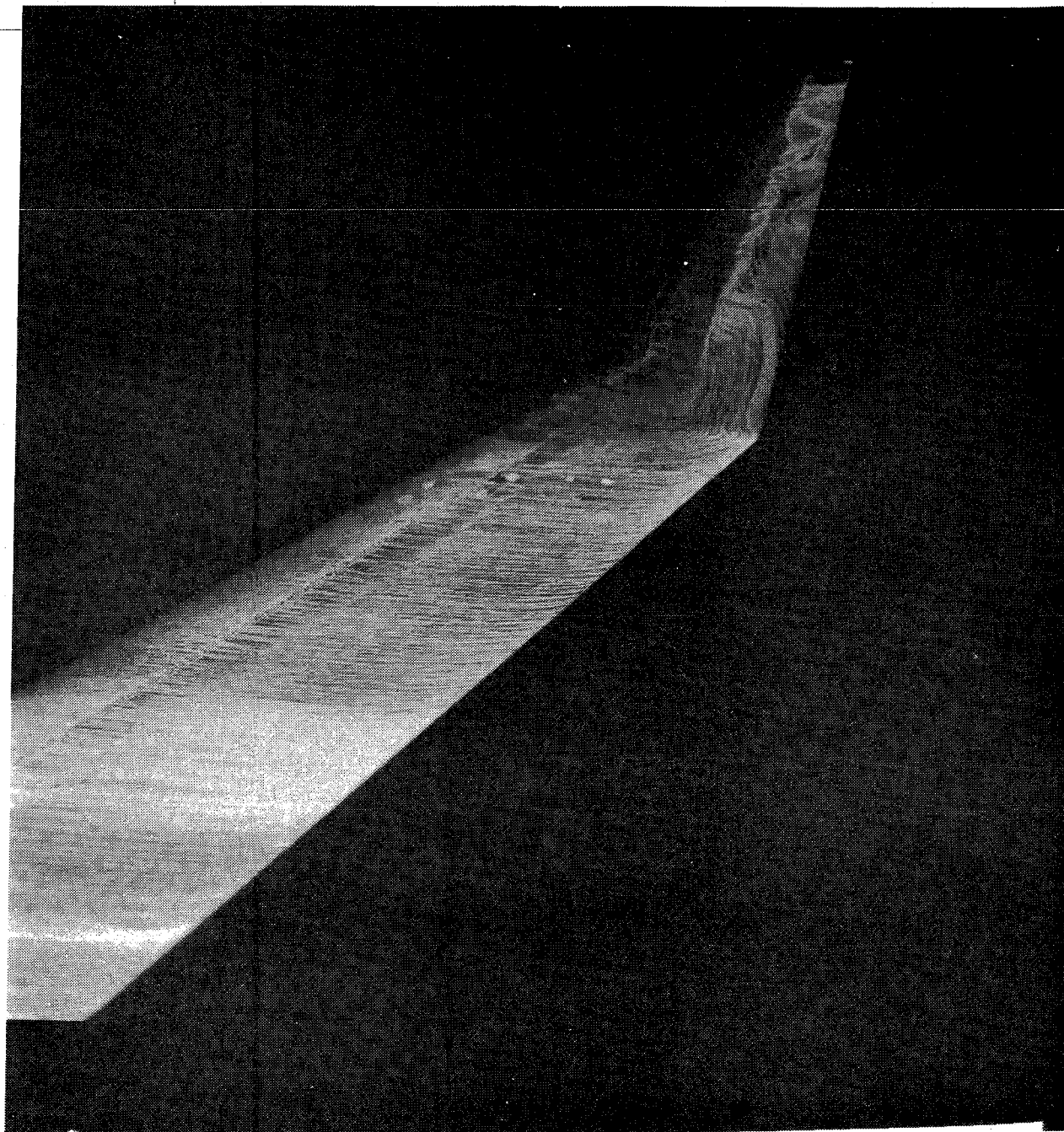


Figure 8(u). Winglet designed by higher-order-panel-wake method
at $M = 0.80$, $\alpha = 1.5^\circ$.

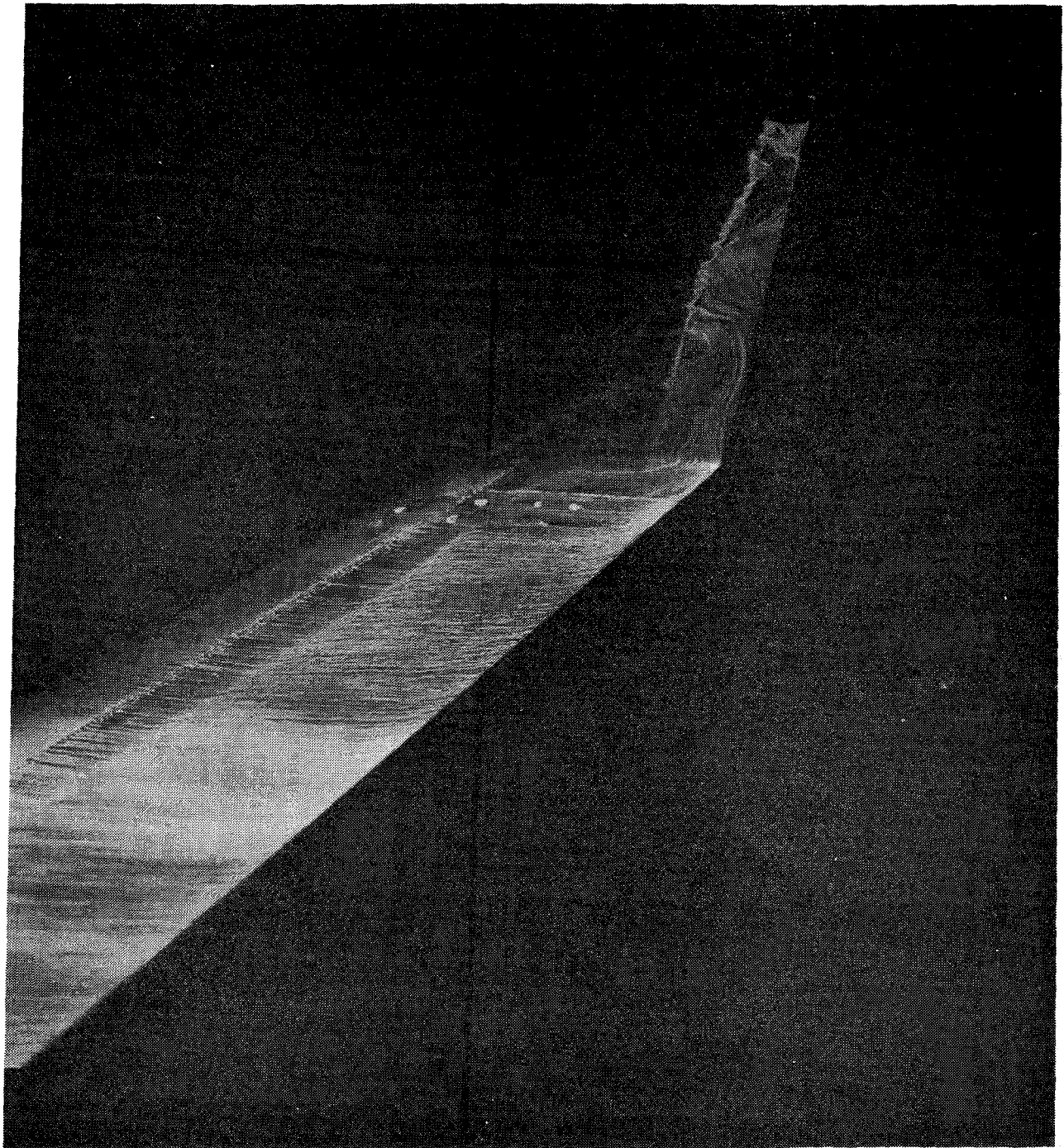


Figure 8(v). Winglet designed by higher-order-panel-wake method
at $M = 0.80$, $\alpha = 2^\circ$.

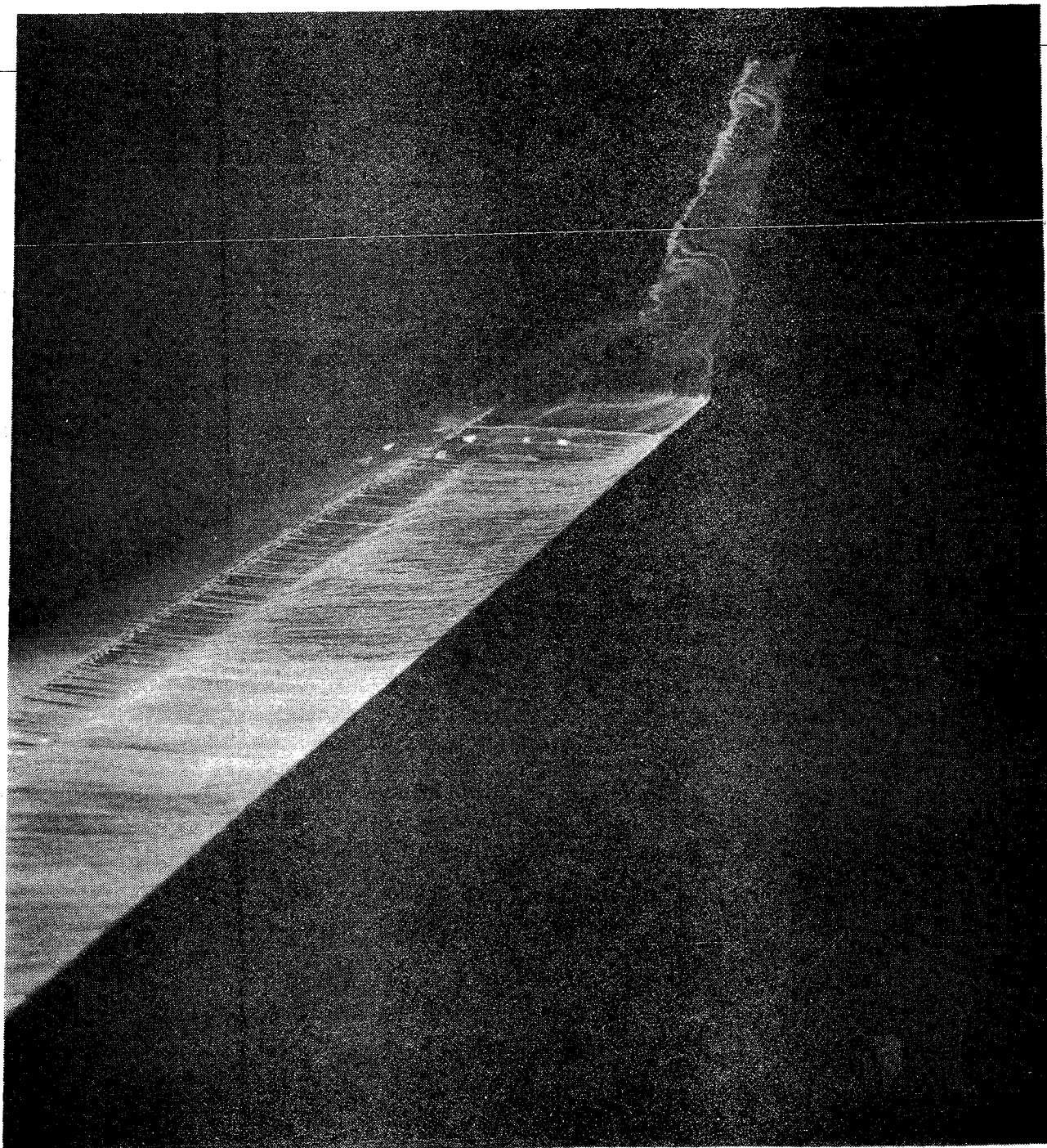


Figure 8(w). Winglet designed by higher-order-panel-wake method
at $M = 0.80$, $\alpha = 2.5^\circ$.

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16. Abstract Wind tunnel test results have been presented herein for a subsonic transport type wing fitted with winglets. Wing planform was chosen to be representative of wings used on current jet transport aircraft, while wing and winglet camber surfaces were designed using two different linear aerodynamic design methods. The purpose of the wind tunnel investigation was to determine the effectiveness of these linear aerodynamic design computer codes in designing a non-planar transport configuration which would cruise efficiently. The design lift coefficient was chosen to be 0.4, at a design Mach number of 0.8. Force and limited pressure data were obtained for the basic wing, and for the wing fitted with the two different winglet designs, at Mach numbers of 0.60, 0.70, 0.75 and 0.80 over an angle of attack range of -2 to +6 degrees, at zero sideslip. The data have been presented without analysis to expedite publication.					
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